

Appendix P: Air Quality

Carbon Monoxide Traffic Air Quality Analysis – Preferred Alternative

Quantitative MSAT Analysis Technical Report – Preferred Alternative

Carbon Monoxide Traffic Air Quality Analysis – as Published in the DEIS, January 5,
2023

Carbon Monoxide Traffic Air Quality Analysis – Preferred Alternative



Carbon Monoxide Traffic Air Quality Analysis

I-35 Capital Express Central Project

Travis County, Texas
Austin District
CSJ: 0015-13-388

July 2023

The environmental review, consultation, and other actions required by applicable Federal environmental laws for this project are being, or have been, carried out by TxDOT pursuant to 23 U.S.C. 327 and a Memorandum of Understanding dated December 9, 2019, and executed by FHWA and TxDOT.

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1.0 Introduction

The Texas Department of Transportation (TxDOT) Austin District is proposing improvements to Interstate Highway 35 (I-35) from US Highway 290 East (US 290E) to State Highway 71 (SH 71)/Ben White Boulevard (CSJ: 0015-13-388). See **Appendix A** for a Project Location Map.

Modeled Scenarios

For the carbon monoxide (CO) analysis, both the No Build Alternative and the Modified Alternative 3 (Mod Alt 3) were modeled for the estimated time of completion (ETC) year (2032) and design year (2050), in accordance with TxDOT's *Environmental Guide: Volume 2 Activity Instructions (March 2023)*.

2.0 Background Information

CO is a primary pollutant from motor vehicles that is largely emitted from a vehicle's exhaust system; thus, there is a federal requirement to model localized CO concentrations for proposed highway projects. Projects that are adding capacity may result in an increase of CO emissions; therefore, TxDOT requires the completion of a project-level CO analysis for added capacity projects that exceed an annual average daily traffic (AADT) volume of 140,000 vehicles per day (vpd).

Since the project would add capacity and the design year traffic volume is above 140,000 vpd (see **Table 1** below), a CO traffic air quality analysis (TAQA) is required to assess whether the project would adversely affect local air quality by contributing to CO levels that exceed the 1-hour or 8-hour CO National Ambient Air Quality Standard (NAAQS).

3.0 Analysis Methodology

The CAL3QHC dispersion model was used to calculate CO concentrations for the modeled scenarios. The supplied traffic data includes 24-hour AADT volumes for the years of 2030 and 2050 (see **Table 1** below). See **Appendix B** for the complete traffic data provided by TxDOT Austin District.

Table 1: Projected AADT and DHV

| I-35 Sections: Mainlanes | AADT | | DHV | |
|--|---------|---------|--------|--------|
| | 2030 | 2050 | 2030 | 2050 |
| Section 1: William Cannon Dr. to MLK Blvd. | 203,000 | 251,450 | 12,180 | 15,087 |
| Section 2: MLK Blvd. to St. Johns Ave | 234,700 | 293,200 | 14,082 | 17,592 |
| I-35 Sections: Frontage Roads | AADT | | DHV | |
| | 2030 | 2050 | 2030 | 2050 |
| Section 2: Ben White Blvd/SH 71 to Oltorf Street | 48,600 | 59,250 | 2,916 | 3,555 |
| Section 3: Oltorf Street to MLK Blvd | 113,700 | 143,450 | 6,822 | 8,607 |
| Section 4: MLK Blvd to 38 1/2th Street | 47,300 | 60,750 | 2,838 | 3,645 |
| Section 5: 38 1/2th Street to US 290 | 132,050 | 166,000 | 7,923 | 9,960 |
| Section 6: US 290 to St. Johns Ave | 74,050 | 91,600 | 4,443 | 5,496 |

DHV – Design Hourly Volume

A growth rate per traffic section was applied to the 2030 traffic volumes to utilize volumes for the ETC year of 2032 in the CO analysis.

The CO analysis includes modeled free-flow areas, as well as select intersections. The free-flow segments (segments 1 through 4) modeled in the CO analysis were chosen based on the areas of the project with the highest AADT and narrowest ROW. Each of the segments were modeled for both alternatives in both the ETC and design year. See **Appendix C** for the mapped modeled segment locations. The modeled segment limits and their respective traffic sections are as follows:

- Segment 1: South of 51st St to N of Airport Blvd (within Traffic Section 2 (Mainlanes) and Section 5 (Frontage Roads))
- Segment 2: North of Dean Keeton to Manor Rd (within Traffic Section 2 (Mainlanes) and Section 4 (Frontage Roads))
- Segment 3: Holly St to north of Lake Austin Dr (within Traffic Section 1 (Mainlanes) and Section 3 (Frontage Roads))
- Segment 4: Woodward St to south of Oltorf St (within Traffic Section 1 (Mainlanes) and Section 2 (Frontage Roads))

Intersection segments (segments 5 through 6) were modeled and chosen based on their Level of Service (LOS) rating (either D, E, or F, with F being the worst LOS). LOS for all the intersections within the Mod Alt 3 area were identified for the ETC and design year, as well as AM and PM peak periods. From this, the two intersections with the most prevalent “F” rated LOS across the peak periods and analyzed years were chosen as the segments for this CO analysis.

- Segment 5: 7th St Intersection (within Traffic Section 1 (Mainlanes) and Section 3 (Frontage Roads).
- Segment 6: Riverside Dr Intersection (within Traffic Section 1 (Mainlanes) and Section 3 (Frontage Roads)

Background CO concentrations of 1.6 parts per million (ppm) (1-hour) and 1.3 ppm (8-hour) were used for the model in accordance with Appendix B of TxDOT’s *Environmental Guide: Volume 2 Activity Instructions (March 2023)*.

Variable emission rates were used in the analysis based on worst-case peak speeds. Worst-case peak traffic speeds range from 3 to 67 mph for both free-flow and intersection scenarios. The rates were derived from the MOVES3 model, gathered from the TxDOT CO TAQA Running and Idling Emission Rates Lookup Tables (ERLT) for TAQA (*TxDOT Air Quality Toolkit, January 2023*).

The following adverse meteorological conditions are the worst-case assumptions and input parameters used in the analysis, in accordance with Appendix D of TxDOT’s *Environmental Guide: Volume 2 Activity Instructions (March 2023)*:

- Averaging time of 60 minutes
- Atmospheric Stability Class of 4 (stable)
- Mixing height of 1,000 meters
- Wind speed of 1 meter per second
- Winds blowing parallel to the roadway
- Surface roughness coefficient of 108 cm
- Source height ranging from -32 feet to +25 feet
- Background CO Concentration for Austin: 1.6 and 1.3 ppm (1-Hour and 8-Hour, respectively)

The following input parameters were used in the intersection analysis, in accordance with *User’s Guide to CAL3QHC Version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections (Revised)*:

- Average total signal cycle length
- Average red total signal cycle length
- Clearance lost time
- Approach volume on queue link
- Idle emission factor
- Saturation flow rate
- Signal type
- Arrival rate

4.0 Receptor Locations

Free-flow receptors were modeled on the future ROW line for each modeled segment. Intersection receptors were modeled at least 10 feet away from the nearest travel lane and on public use features, such as a sidewalk, and placed at each quadrant of the intersection. A standard height of 5.9 feet was given to the receptors for all models to simulate the average height of a person. **Table 2** and **Table 3** depict the associated ROW, LOS, and traffic at each of the modeled receptors. Aerial maps depicting the receptor locations along the project ROW are found in **Appendix C**.

Table 2: Free-flow Receptor Descriptions

| Name | Segment | Distance from Roadway | ROW Width | 2032 Total DHV | 2050 Total DHV | 2032 Total AADT | 2050 Total AADT | Traffic Speeds |
|-----------------|-----------|-----------------------|-----------|----------------|----------------|-----------------|-----------------|----------------|
| Receptor 1 (R1) | Segment 1 | 103 ft | 487 ft | 22,502 | 27,552 | 375,041 | 459,200 | 3-56 mph |
| Receptor 2 (R2) | Segment 1 | 85 ft | 487 ft | 22,502 | 27,552 | 375,041 | 459,200 | 3-56 mph |
| Receptor 3 (R3) | Segment 2 | 15 ft | 205 ft | 17,307 | 21,237 | 288,443 | 353,950 | 3-55 mph |
| Receptor 4 (R4) | Segment 2 | 13 ft | 205 ft | 17,307 | 21,237 | 288,443 | 353,950 | 3-55 mph |
| Receptor 5 (R5) | Segment 3 | 25 ft | 353 ft | 19,424 | 23,694 | 323,726 | 394,900 | 3-67 mph |
| Receptor 6 (R6) | Segment 3 | 46 ft | 353 ft | 19,424 | 23,694 | 323,726 | 394,900 | 3-67 mph |
| Receptor 7 (R7) | Segment 4 | 33 ft | 350 ft | 15,416 | 18,642 | 256,936 | 310,700 | 3-66 mph |
| Receptor 8 (R8) | Segment 4 | 25 ft | 350 ft | 15,416 | 18,642 | 256,936 | 310,700 | 3-66 mph |

Table 3: Intersection Receptor Descriptions

| Name | Segment | Distance from Roadway | LOS | 2032 Total DHV | 2050 Total DHV | 2032 Total AADT | 2050 Total AADT | Traffic Speeds |
|-----------------------------|-----------|-----------------------|-----|----------------|----------------|-----------------|-----------------|----------------|
| 7 th St (7th SE) | Segment 5 | 15 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-57 mph |
| 7 th St (7th NE) | Segment 5 | 21 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-57 mph |
| 7 th St (7th NW) | Segment 5 | 10 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-57 mph |
| 7 th St (7th SW) | Segment 5 | 21 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-57 mph |
| Riverside Dr (RS SE) | Segment 6 | 109 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-44 mph |
| Riverside Dr (RS NE) | Segment 6 | 12 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-44 mph |
| Riverside Dr (RS SW) | Segment 6 | 10 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-44 mph |
| Riverside Dr (RS NW) | Segment 6 | 8 ft | F | 19,423 | 23,694 | 323,726 | 394,900 | 3-44 mph |

5.0 Analysis Results

The 1-hour CO NAAQS is 35 ppm, while the 8-hour NAAQS is 9 ppm, which are not to be exceeded more than once in a year. Modeling results indicate that local concentrations of CO are not expected to exceed national standards at any time along any segment of the project. While emission rates are expected to decrease over time, some model results show a slight increase in CO concentrations from 2032 to 2050. These increases can be explained with the worsening traffic speeds predicted for 2050.

The highest CO concentration result and percent of the 1-hour and 8-hour NAAQS along the I-35 project for all scenarios and intersections are recorded in **Tables 4 through 7**. The highest modeled CO concentrations mostly occur in Segment 2, from north of Dean Keaton to Manor Road, and represents the worst-case results for the project. Even though the AADT for Segment 2 isn't the highest, it has the lowest peak period speeds and narrowest ROW by 145 feet with the associated receptors being in close proximity to frontage roads with high emission rates. Segment 3 CO concentrations see similar results to a lesser degree than Segment 2 for the same reason. In contrast, the lowest modeled CO concentrations occur in Segments 1 and 4, which have wider ROW.

The projected CO concentrations are relatively consistent between the 7th St and Riverside intersections, with the highest CO concentration result occurring at 7th Street in the Mod Alt 3 2050 scenario. Both intersections fall within traffic sections Mainlane Section 1 and Frontage Road Section 3, meaning that roadway design and speeds are the primary deciding factors in their CO concentrations.

Among all modeled segments, receptor proximity to roadway section tends to be a standout determining factor for CO concentrations. Peak speed limit is a key contributing factor for any variance in expected CO concentrations between ETC and Design scenarios since they vary with year while AADT between the scenarios grow in tandem.

The associated input and output CAL3QHC files have been submitted with this technical report for inclusion in the project files.

Table 4: Free-flow No Build and Mod Alt 3 1-Hour and 8-Hour CO Concentrations (ETC Year)

| ETC Year: 2032 | | | | | | | |
|--|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| No Build | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 2 (NB) | Segment 1 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 3 (SB) | Segment 2 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 4 (NB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 5 (SB) | Segment 3 | 2.4 | 1.6 | 1.3 | 1.9 | 6.9% | 21.1% |
| Receptor 6 (NB) | Segment 3 | 2.4 | 1.6 | 1.3 | 1.9 | 6.9% | 21.1% |
| Receptor 7 (SB) | Segment 4 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 8 (NB) | Segment 4 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Mod Alt 3 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 2 (NB) | Segment 1 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 3 (SB) | Segment 2 | 3.4 | 1.6 | 1.3 | 2.6 | 9.7% | 28.9% |
| Receptor 4 (NB) | Segment 2 | 4.9 | 1.6 | 1.3 | 3.6 | 14.0% | 40.0% |
| Receptor 5 (SB) | Segment 3 | 2.4 | 1.6 | 1.3 | 1.9 | 6.9% | 21.1% |
| Receptor 6 (NB) | Segment 3 | 2.2 | 1.6 | 1.3 | 1.7 | 6.3% | 18.9% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Note: 8-Hour CO Concentrations have been rounded to the nearest tenth decimal. | | | | | | | |

Table 5: Free-flow No Build and Mod Alt 3 1-Hour and 8-Hour CO Concentrations (Design Year)

| Design Year: 2050 | | | | | | | |
|--|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| No Build | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 2 (NB) | Segment 1 | 2.5 | 1.6 | 1.3 | 1.9 | 7.1% | 21.1% |
| Receptor 3 (SB) | Segment 2 | 2.5 | 1.6 | 1.3 | 1.9 | 7.1% | 21.1% |
| Receptor 4 (NB) | Segment 2 | 2.4 | 1.6 | 1.3 | 1.9 | 6.9% | 21.1% |
| Receptor 5 (SB) | Segment 3 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 6 (NB) | Segment 3 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 7 (SB) | Segment 4 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 8 (NB) | Segment 4 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Mod Alt 3 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 2 (NB) | Segment 1 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 3 (SB) | Segment 2 | 3.1 | 1.6 | 1.3 | 2.4 | 8.9% | 26.7% |
| Receptor 4 (NB) | Segment 2 | 5.7 | 1.6 | 1.3 | 4.2 | 16.3% | 46.7% |
| Receptor 5 (SB) | Segment 3 | 2.7 | 1.6 | 1.3 | 2.1 | 7.7% | 23.3% |
| Receptor 6 (NB) | Segment 3 | 2.5 | 1.6 | 1.3 | 1.9 | 7.1% | 21.1% |
| Receptor 7 (SB) | Segment 4 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 8 (NB) | Segment 4 | 2.2 | 1.6 | 1.3 | 1.7 | 6.3% | 18.9% |
| Note: 8-Hour CO Concentrations have been rounded to the nearest tenth decimal. | | | | | | | |

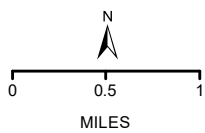
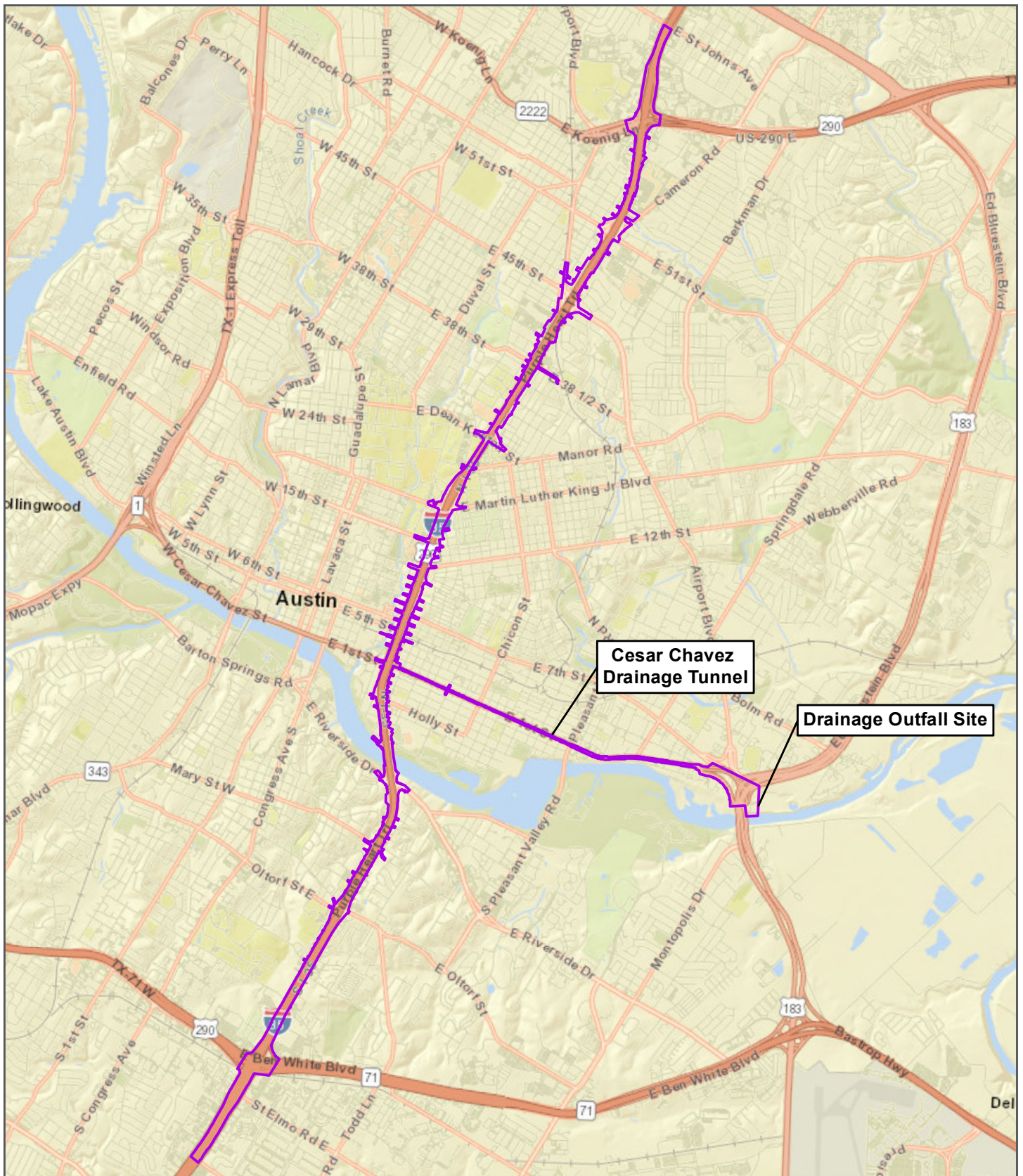
Table 6: Mod Alt 3 Intersection 1-Hour and 8-Hour CO Concentrations (ETC Year)

| 2032 | | | | | | | |
|--------------------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7 th SE | Segment 5 | 2.7 | 1.6 | 1.3 | 2.1 | 7.7% | 23.3% |
| 7 th NE | Segment 5 | 2.6 | 1.6 | 1.3 | 2.0 | 7.4% | 22.2% |
| 7 th NW | Segment 5 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| 7 th SW | Segment 5 | 2.2 | 1.6 | 1.3 | 1.7 | 6.3% | 18.9% |
| RS SE | Segment 6 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| RS NE | Segment 6 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| RS SW | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS NW | Segment 6 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |


Table 7: Mod Alt 3 Intersection 1-Hour and 8-Hour CO Concentrations (Design Year)

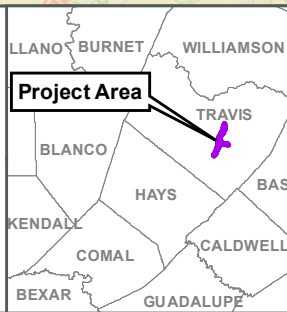
| 2050 | | | | | | | |
|--------------------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7 th SE | Segment 5 | 2.9 | 1.6 | 1.3 | 2.2 | 8.3% | 24.4% |
| 7 th NE | Segment 5 | 2.8 | 1.6 | 1.3 | 2.1 | 8.0% | 23.3% |
| 7 th NW | Segment 5 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| 7 th SW | Segment 5 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| RS SE | Segment 6 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| RS NE | Segment 6 | 2.5 | 1.6 | 1.3 | 1.9 | 7.1% | 21.1% |
| RS SW | Segment 6 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| RS NW | Segment 6 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |

APPENDIX A
Project Location Map



Legend

 MODIFIED ALTERNATIVE 3 - PREFERRED ALTERNATIVE



PROJECT LOCATION MAP

I-35 CAPITAL EXPRESS
CENTRAL PROJECT

TRAVIS COUNTY, TX

APRIL 2023

FIGURE 1



APPENDIX B

Traffic Data

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 91.2 | | 96.0 | | | | | | | | | |
| Medium Duty | 2.3 | | 1.0 | | | | | | | | | |
| Heavy Duty | 6.5 | | 3.0 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Mainlanes) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From William Cannon Dr. To US 183 | 245,200 | 305,900 | 51 - 49 | 6.0 | 8.8 | 4.0 | 13,700 | 20 | 86,456,000 | 3 | 121,376,000 | 8" |
| Travis County | | | | | | | | | | | | |
| I-35 (No Build Mainlanes) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From William Cannon Dr. To US 183 | 245,200 | 326,200 | 51 - 49 | 6.0 | 8.8 | 4.0 | 13,700 | 20 | 134,461,000 | 3 | 188,770,500 | 8" |
| Travis County | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | |
|--|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|-------------|---|-------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Mainlanes)</u></p> <p align="center"><u>Section 3</u></p> <p>From US 183 To SH 45 N</p> <p>Travis County</p> | | | | | | | | | | | | | 81,221,500 | 3 | 114,057,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | |
| Light Duty | 90.4 | | 95.7 | | | | | | | | | | | | | |
| Medium Duty | 2.6 | | 1.2 | | | | | | | | | | | | | |
| Heavy Duty | 7.0 | | 3.1 | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Mainlanes)</u></p> <p align="center"><u>Section 3</u></p> <p>From US 183 To SH 45 N</p> <p>Travis County</p> | | | | | | | | | | | | | 125,926,000 | 3 | 176,834,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From SH 45 South To Slaughter Creek Travis County | 9,300 | 12,150 | 52 - 48 | 7.0 | 4.3 | 3.2 | 10,800 | 40 | 1,151,000 | 3 | 1,419,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| | Light Duty | 95.7 | 96.8 | | | | | | | | | |
| Medium Duty | 2.6 | | 2.0 | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.2 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From SH 45 South To Slaughter Creek Travis County | 9,300 | 12,850 | 52 - 48 | 7.0 | 4.3 | 3.2 | 10,800 | 40 | 1,783,500 | 3 | 2,199,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From Slaughter Creek To Slaughter Lane | 54,250 | 71,100 | 52 - 48 | 7.0 | 3.9 | 2.9 | 11,900 | 30 | 6,116,000 | 3 | 7,534,500 | 8" |
| Travis County | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | |
| | Light Duty | 96.1 | 97.1 | | | | | | | | | |
| Medium Duty | 2.3 | 1.7 | | | | | | | | | | |
| Heavy Duty | 1.6 | 1.2 | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From Slaughter Creek To Slaughter Lane | 54,250 | 75,500 | 52 - 48 | 7.0 | 3.9 | 2.9 | 12,000 | 30 | 9,496,000 | 3 | 11,699,000 | 8" |
| Travis County | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | |
| Light Duty | 96.8 | | 97.6 | | | | | | | | | | |
| Medium Duty | 1.9 | | 1.4 | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From Slaughter Lane To William Cannon Dr. Travis County | 79,000 | 103,550 | 52 - 48 | 7.0 | 3.2 | 2.4 | 12,000 | 30 | 7,345,500 | 3 | 9,028,500 | 8" | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From Slaughter Lane To William Cannon Dr. Travis County | 79,000 | 109,650 | 52 - 48 | 7.0 | 3.2 | 2.4 | 12,000 | 30 | 11,386,500 | 3 | 13,995,000 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|--------|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 4 | | | | | | | | | | | | | |
| From William Cannon Dr. To Lady Bird Lake | | | | | | | | | | | | | |
| Travis County | | | | | | | | | | | | | |
| 71,050 | 89,450 | 52 - 48 | 7.0 | 3.4 | 2.6 | 12,000 | 30 | 6,850,500 | 3 | 8,426,500 | 8" | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | | |
| Base Year | | | | | | | | | | | | | |
| % of ADT | | | | | | | | | | | | | |
| % of DHV | | | | | | | | | | | | | |
| Light Duty | | | | | | | | | | | | | |
| 96.6 | | | | | | | | | | | | | |
| 97.4 | | | | | | | | | | | | | |
| Medium Duty | | | | | | | | | | | | | |
| 2.0 | | | | | | | | | | | | | |
| 1.5 | | | | | | | | | | | | | |
| Heavy Duty | | | | | | | | | | | | | |
| 1.4 | | | | | | | | | | | | | |
| 1.1 | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 4 | | | | | | | | | | | | | |
| From William Cannon Dr. To Lady Bird Lake | | | | | | | | | | | | | |
| Travis County | | | | | | | | | | | | | |
| 71,050 | 95,500 | 52 - 48 | 7.0 | 3.4 | 2.6 | 12,000 | 30 | 10,663,000 | 3 | 13,116,000 | 8" | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | |
| Light Duty | 95.9 | 96.9 | | | | | | | | | | |
| Medium Duty | 2.4 | 1.8 | | | | | | | | | | |
| Heavy Duty | 1.7 | 1.3 | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 5 | | | | | | | | | | | | |
| From Lady Bird Lake To 38 1/2th Street | 48,400 | 64,350 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 8,665,000 | 3 | 10,681,000 | 8" |
| Travis County | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | |
|--|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From 38 1/2th Street To 51st Street</p> <p>Travis County</p> | | | | | | | | | | 84,400 | 105,100 | 51 - 49 | 6.0 | 3.2 | 2.4 | 12,000 | 30 | 7,625,000 | 3 | 9,372,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.8 | | 97.6 | | | | | | | | | | | | | | | | | | |
| Medium Duty | 1.9 | | 1.4 | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From 38 1/2th Street To 51st Street</p> <p>Travis County</p> | | | | | | | | | | 84,400 | 112,000 | 51 - 49 | 6.0 | 3.2 | 2.4 | 12,100 | 30 | 11,854,500 | 3 | 14,570,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | |
|---|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|-----------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 7</u></p> <p>From 51st Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | | 6,150,500 | 3 | 7,572,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | |
| | Light Duty | | 96.3 | | 97.2 | | | | | | | | | | | |
| | Medium Duty | | 2.2 | | 1.7 | | | | | | | | | | | |
| | Heavy Duty | | 1.5 | | 1.1 | | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 7</u></p> <p>From 51st Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | | 9,562,500 | 3 | 11,774,000 | 8" |

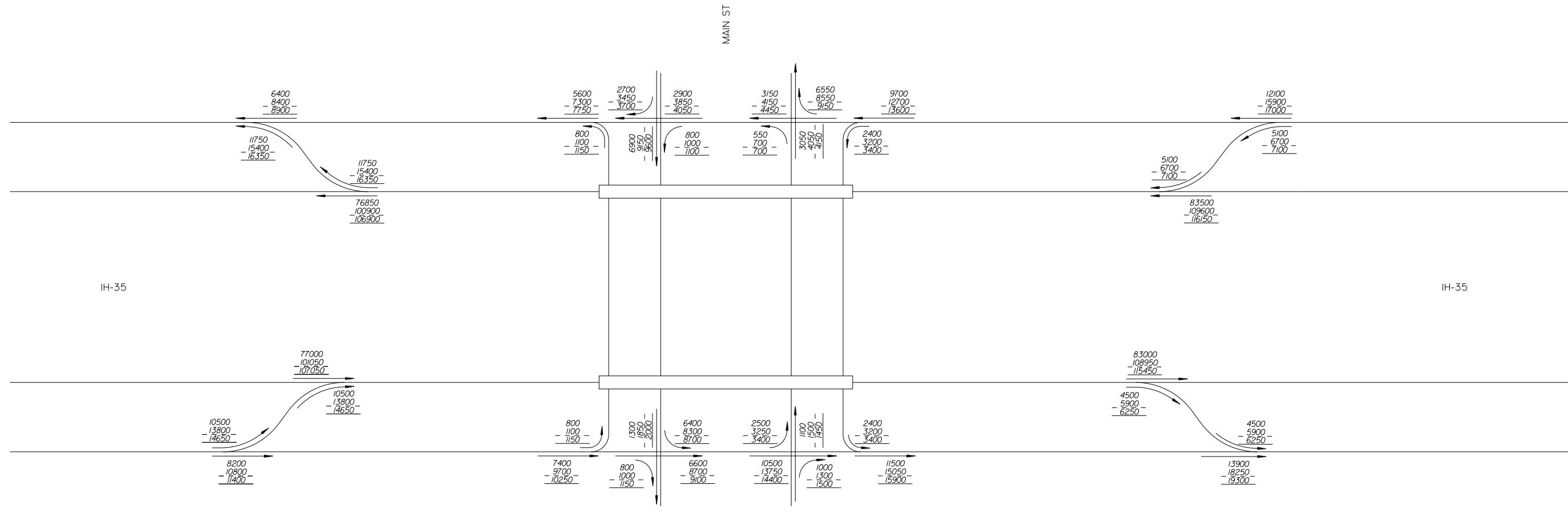
TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | | | |
|--|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--------|---------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 8</u></p> <p>From US 290 To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 74,450 | 95,450 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 7,044,000 | 3 | 8,661,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.7 | | 97.5 | | | | | | | | | | | | | | | | | | | | | |
| Medium Duty | 2.0 | | 1.5 | | | | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 8</u></p> <p>From US 290 To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 74,450 | 101,750 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 10,958,000 | 3 | 13,473,500 | 8" |

NO-BUILD CONFIGURATION



... \2018.0011 *LineDiagrams*TPP*NB.dgn

Houston

11:12:01 AM



1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

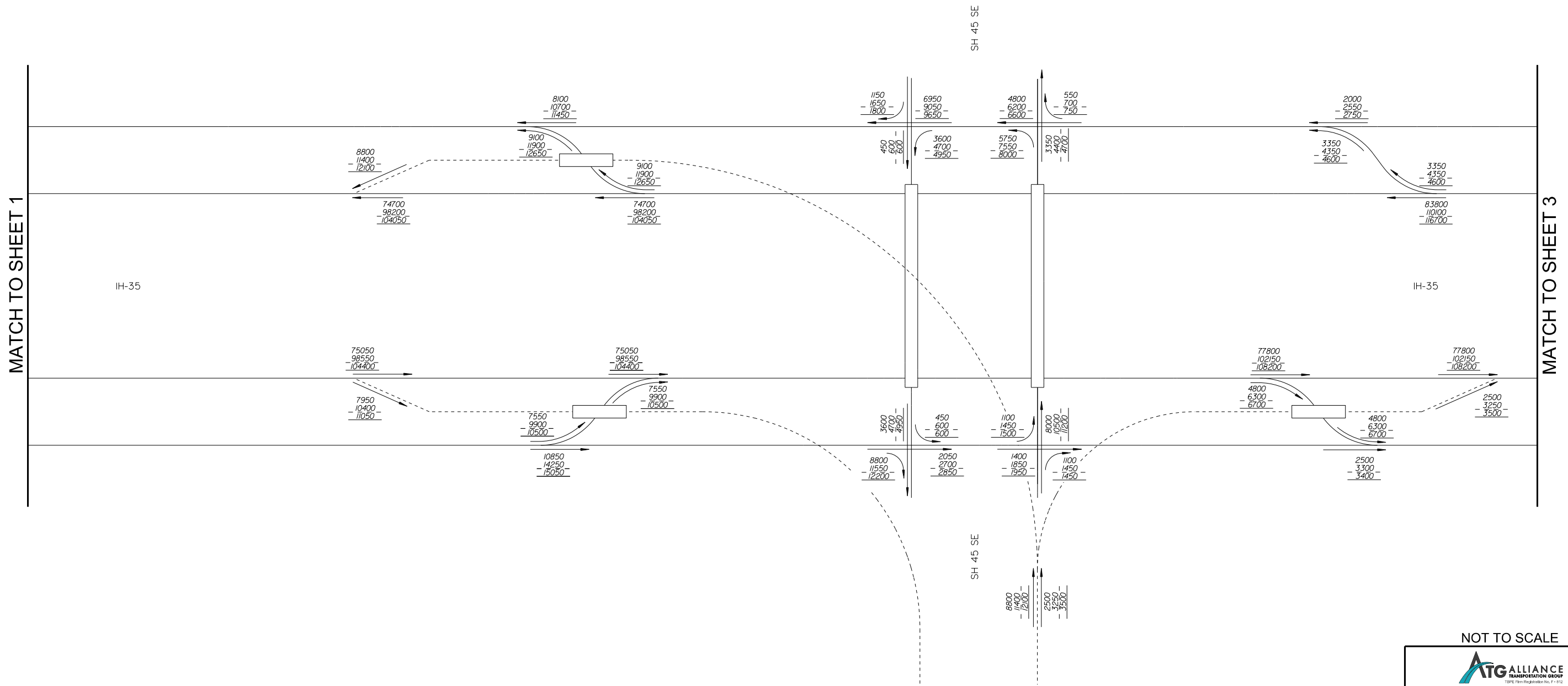
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 1 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | HAYS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 1 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

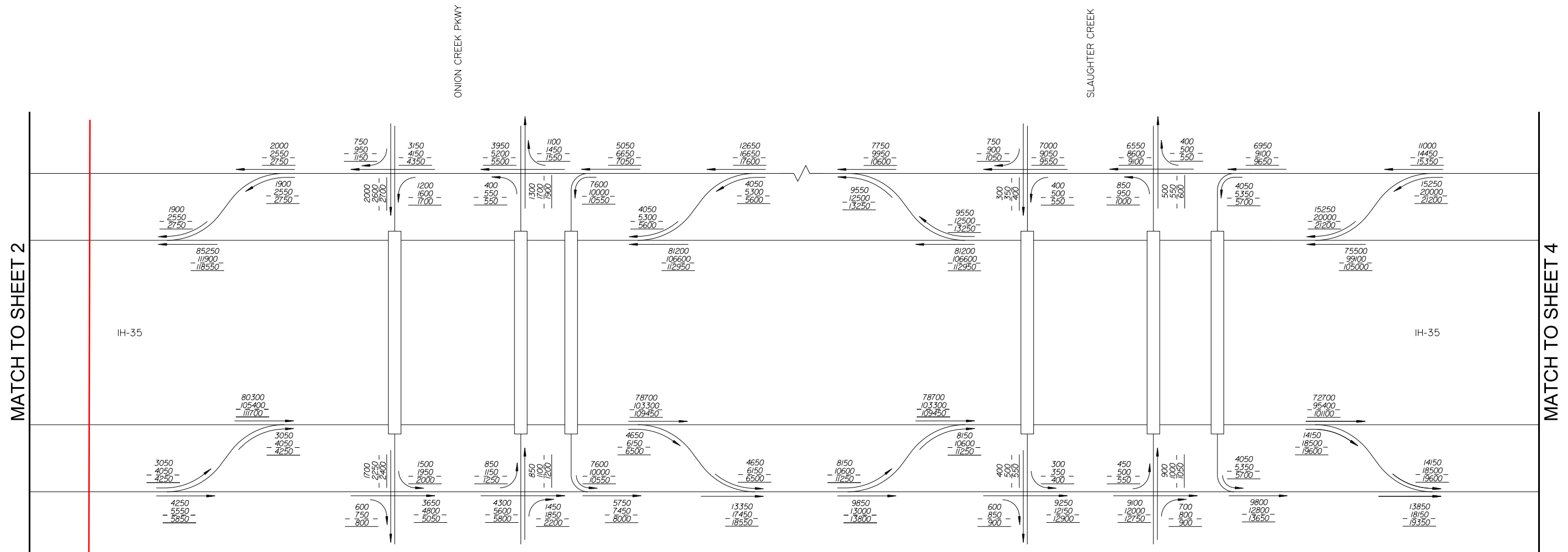
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 2 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 2 |

NO-BUILD CONFIGURATION



MATCH TO SHEET 2

MATCH TO SHEET 4

IH-35

IH-35

Frontage Road
Section 1

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

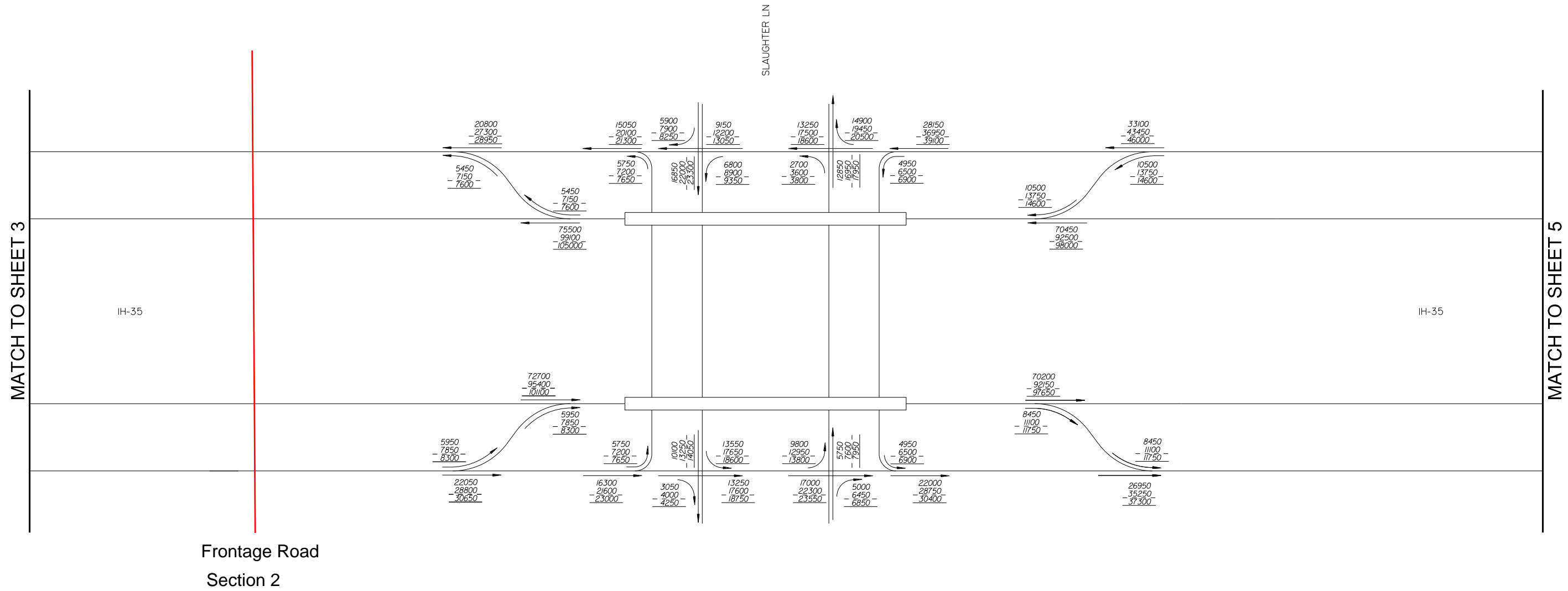
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 3 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 3 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

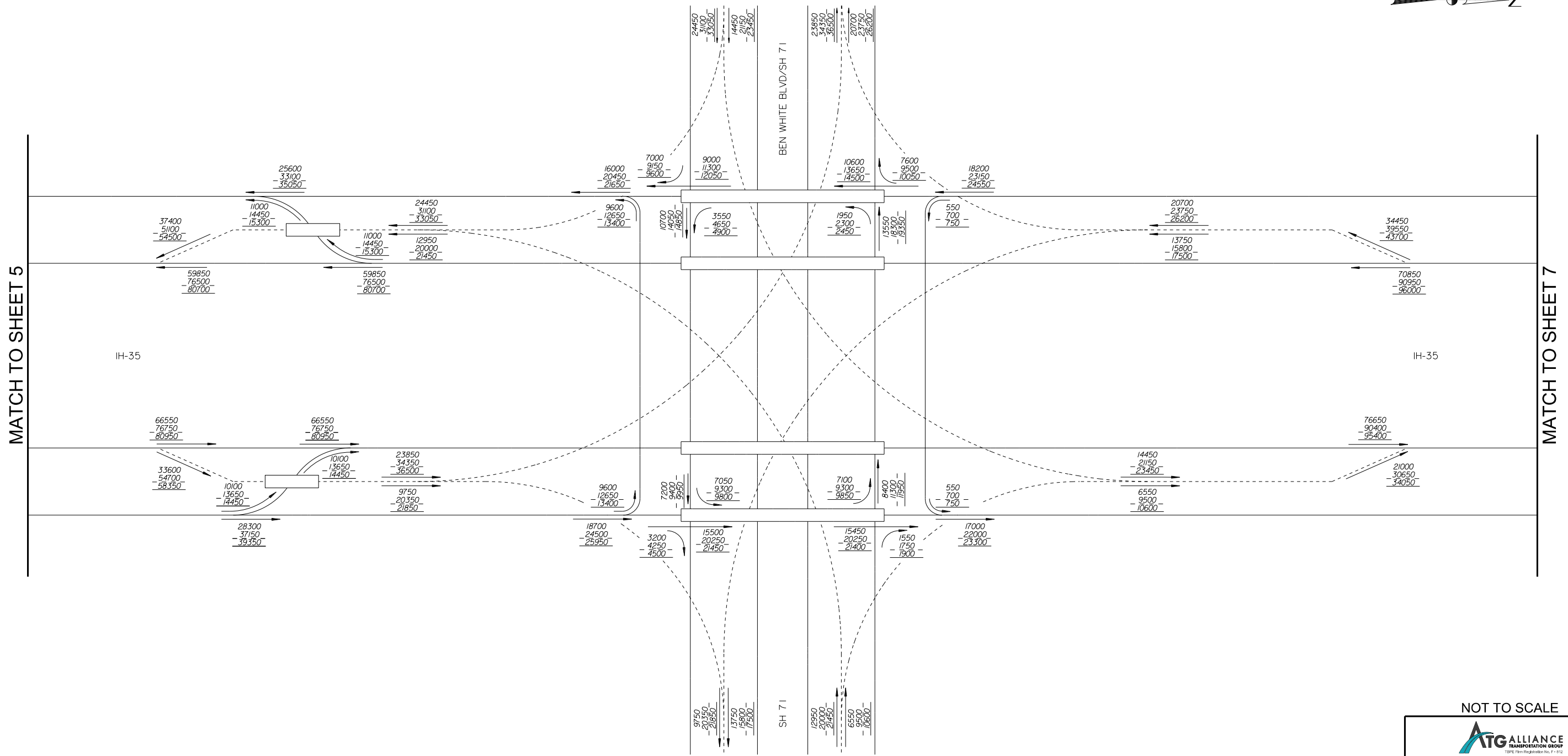


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 4 OF 28)

| | | | | |
|------------------|----------------|-------------------|-------------|-----------|
| SCALE : N. T. S. | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 4 |

NO-BUILD CONFIGURATION




MATCH TO SHEET 5

MATCH TO SHEET 7


2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



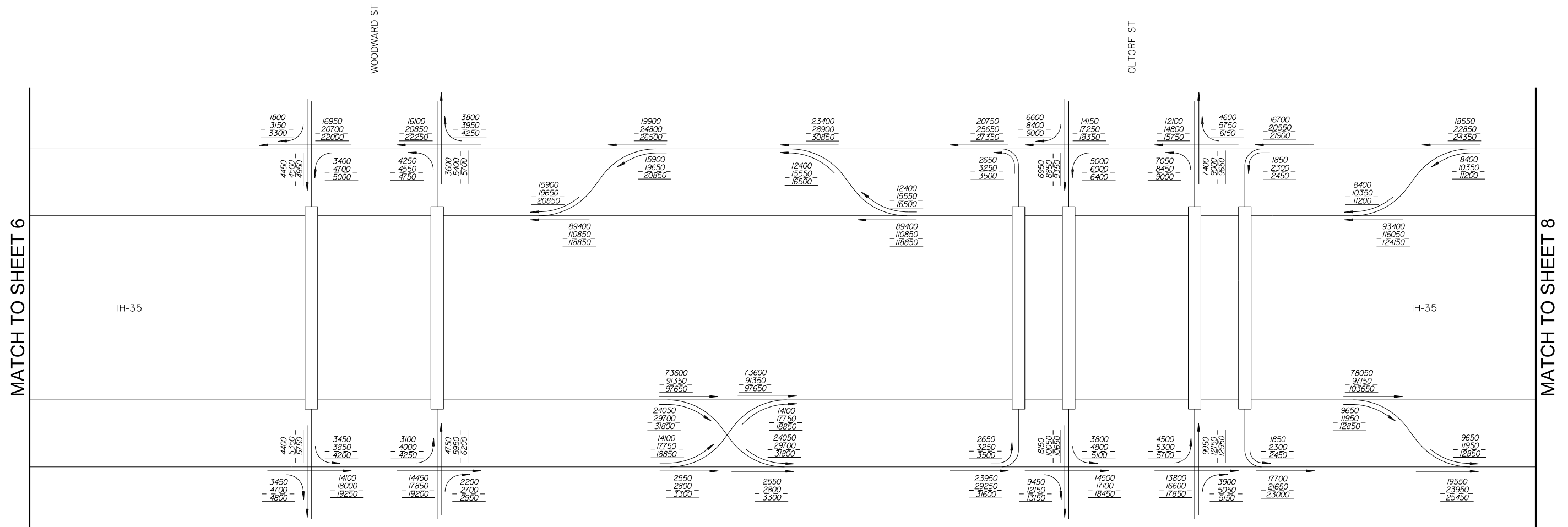
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 6 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 6 |

NO-BUILD CONFIGURATION



MATCH TO SHEET 6


MATCH TO SHEET 8

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



ATG ALLIANCE
TRANSPORTATION GROUP



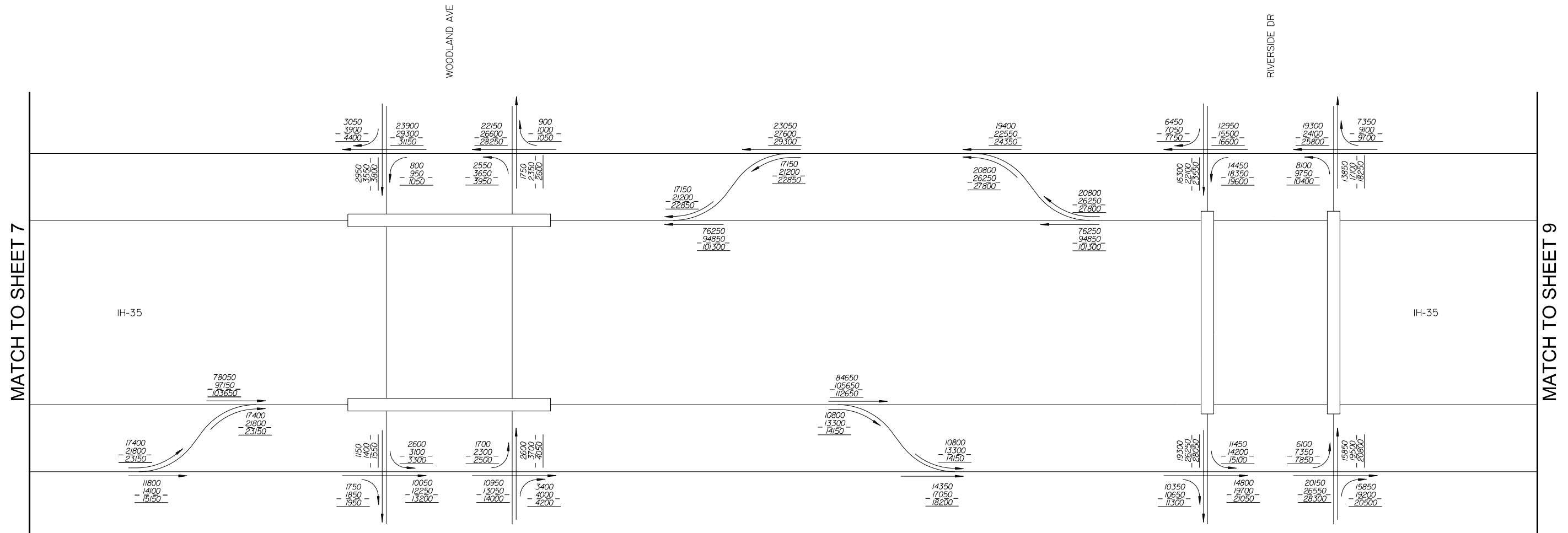
TEXAS DEPARTMENT OF TRANSPORTATION

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 7 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 7 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

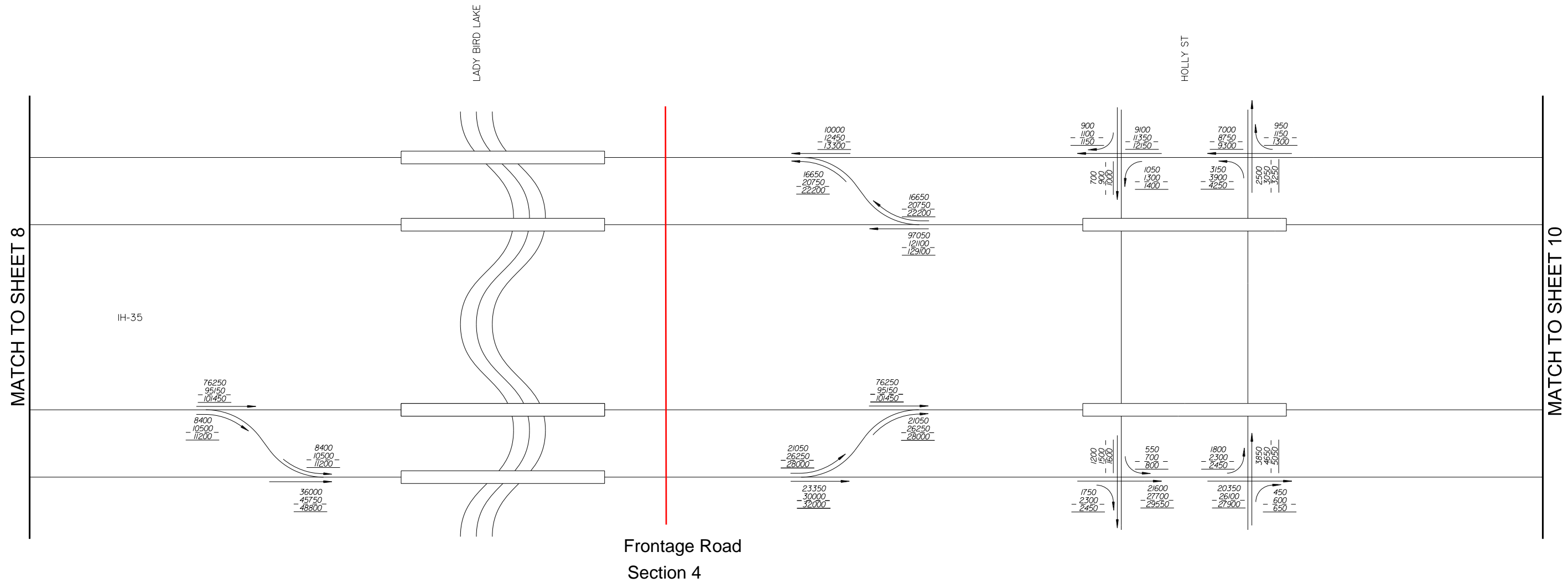


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 8 OF 28)

| | | | | | |
|------------------|----------------|-------------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 8 | |

NO-BUILD CONFIGURATION



Frontage Road
Section 4

MATCH TO SHEET 8

MATCH TO SHEET 10

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

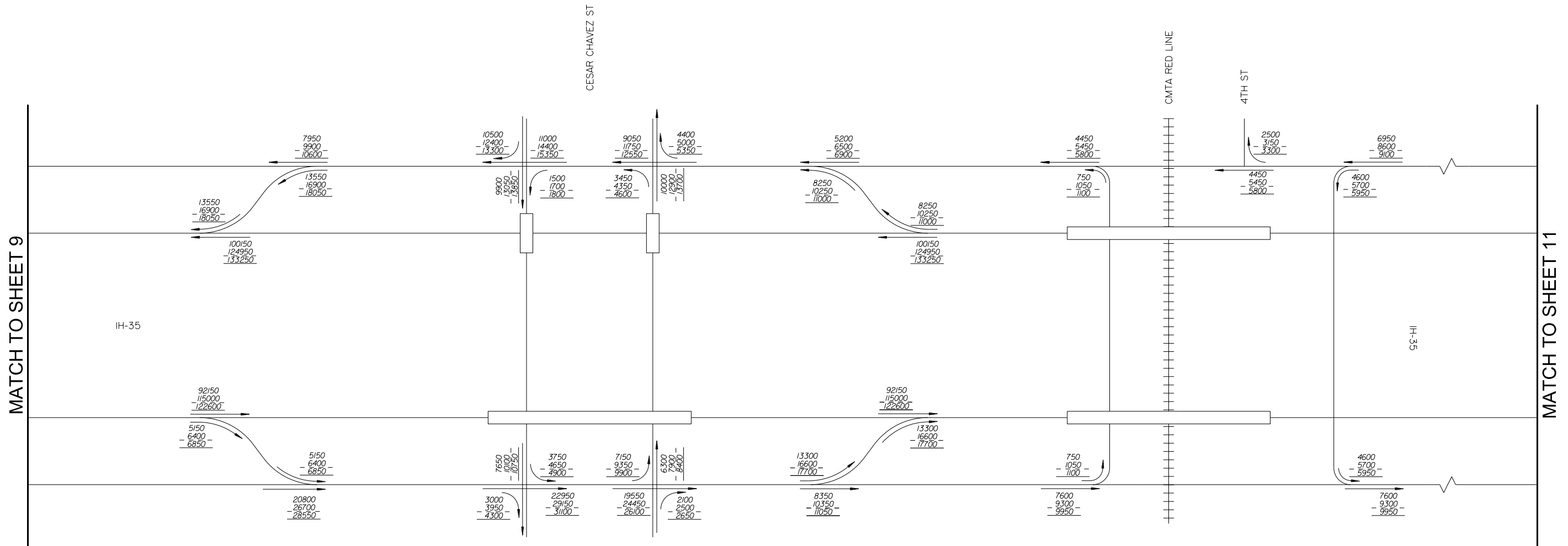
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 9 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 9 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

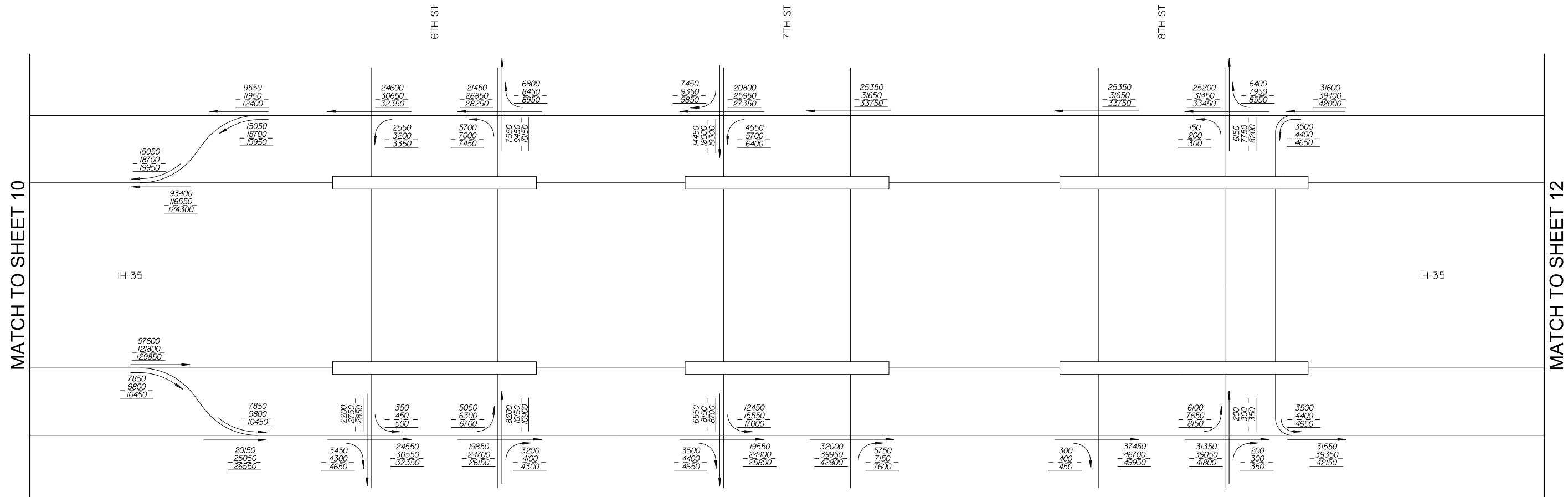
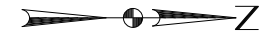
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NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 10 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 10 |

NO-BUILD CONFIGURATION



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



TRANSPORTATION GROUP



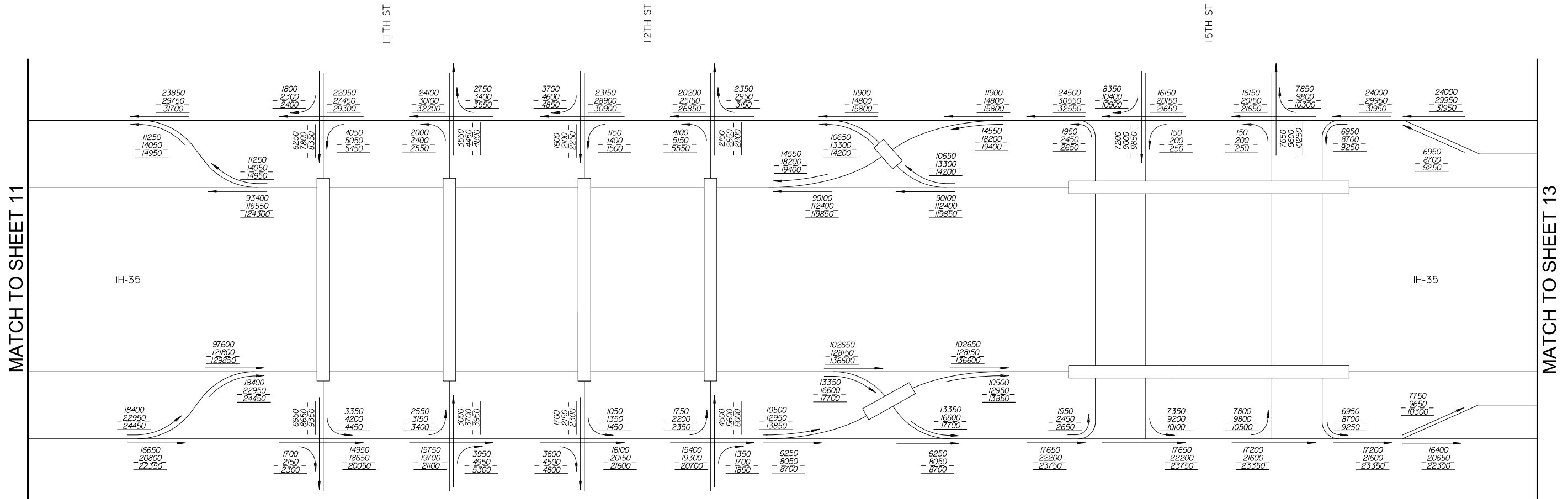
Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 11 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 11 |

NO-BUILD CONFIGURATION



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Houston

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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

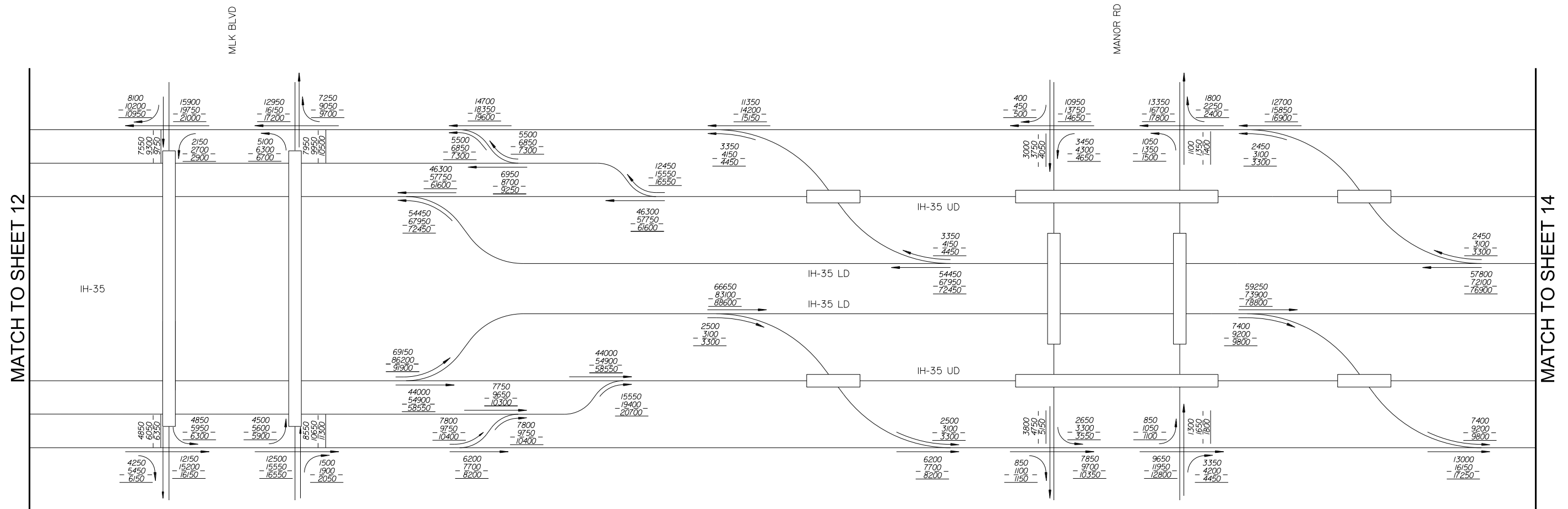
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 12 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 12 |

NO-BUILD CONFIGURATION



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Houston

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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



TRANSPORTATION GROUP



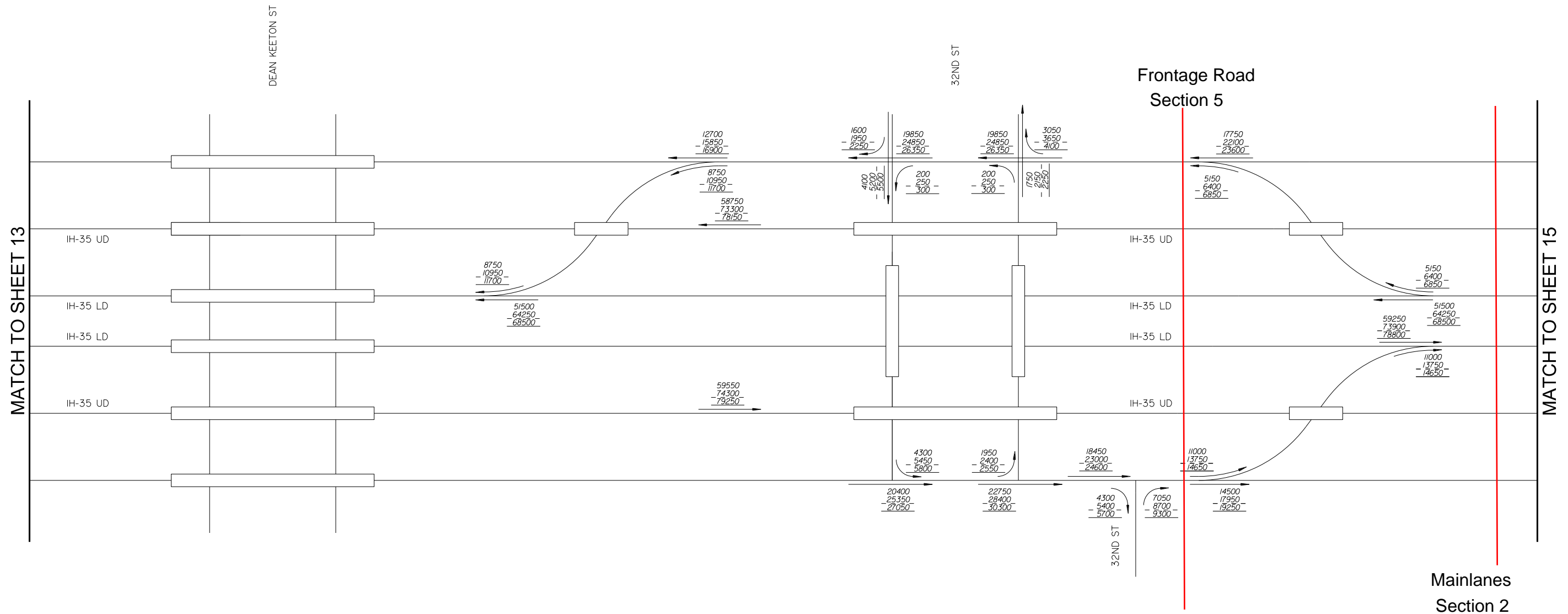
Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 13 OF 28)

| | | | |
|------------------|---------|-------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE | FED. RD. DISTRICT |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 13 |



NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

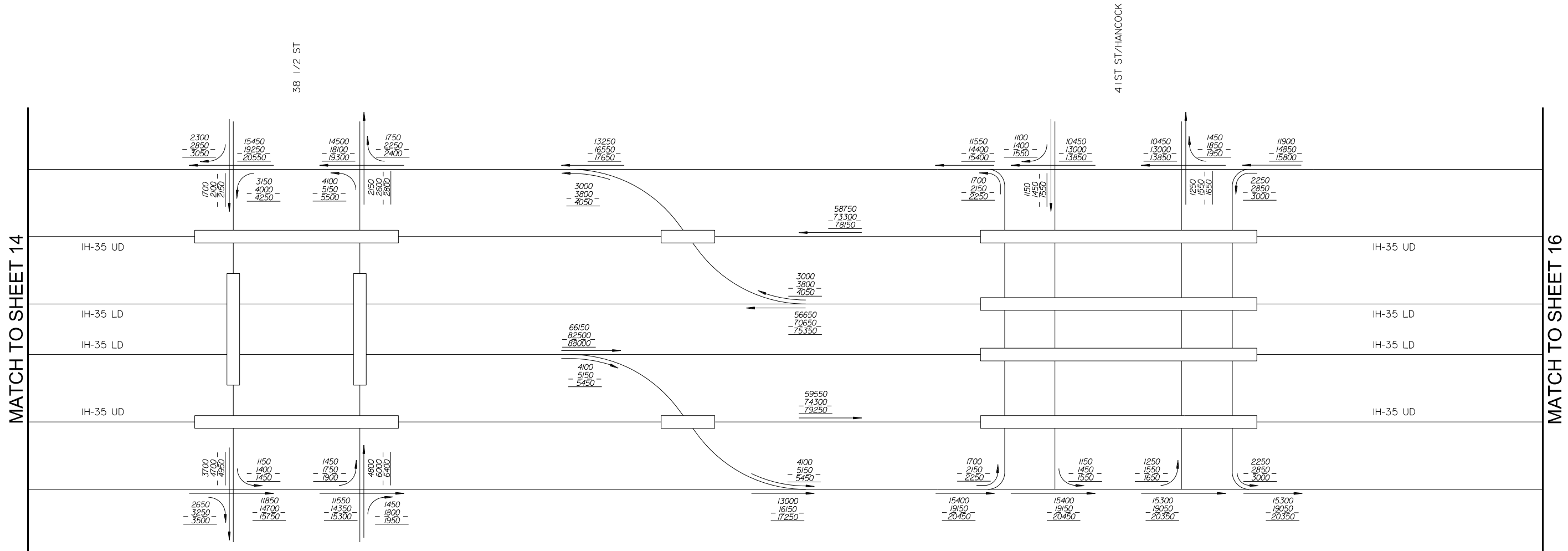
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 14 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 14 |



NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

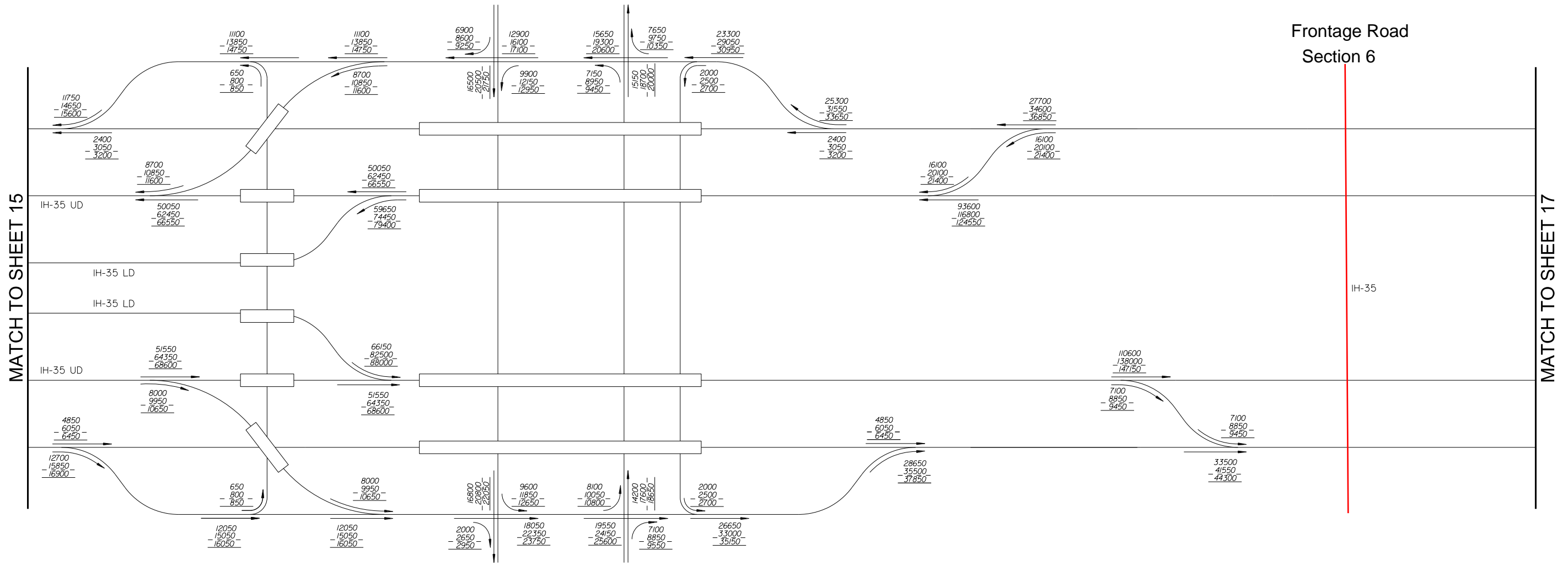
CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 15 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 15 |

NO-BUILD CONFIGURATION



Frontage Road Section 6



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

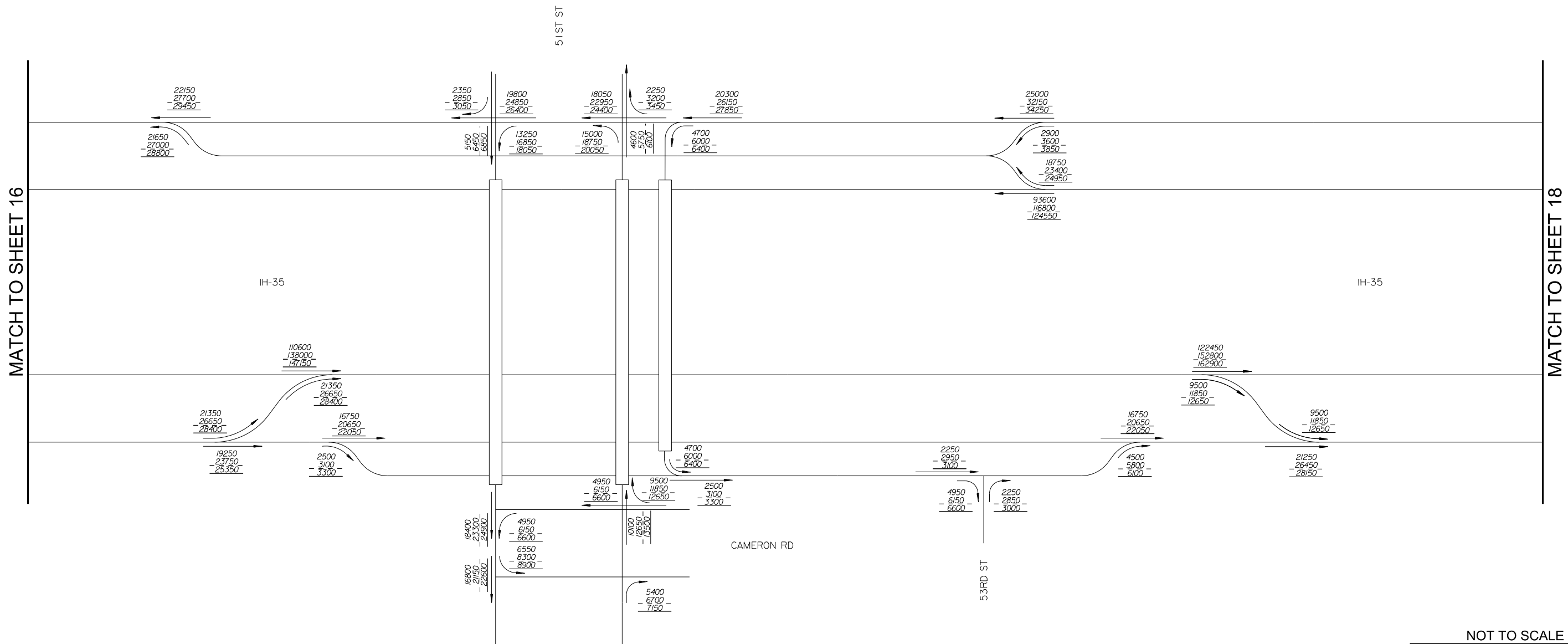


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 16 OF 28)

| | | | | |
|------------------|----------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 16 |

NO-BUILD CONFIGURATION



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



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TRANSPORTATION GROUP



TEXAS DEPARTMENT OF TRANSPORTATION

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 17 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 17 |

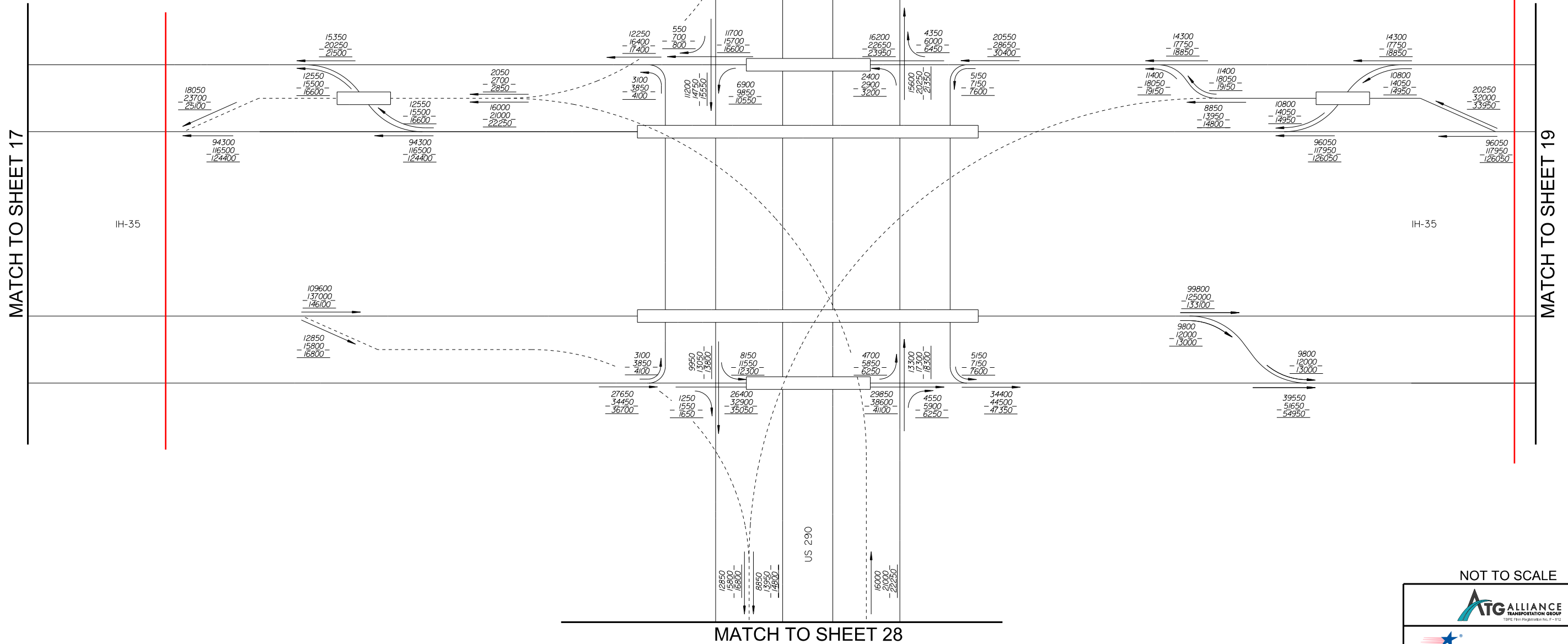
NO-BUILD CONFIGURATION

MATCH TO SHEET 27



Frontage Road
Section 7

Frontage Road
Section 8



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

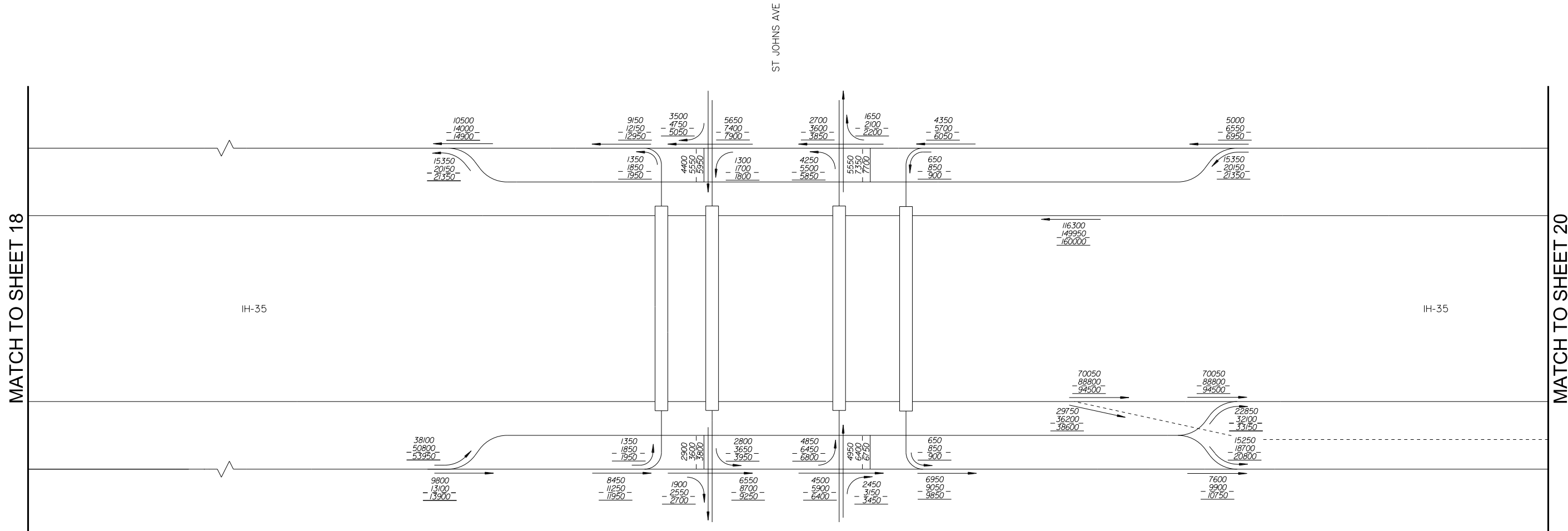
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 18 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |

NO-BUILD CONFIGURATION





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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
 LD - LOWER DECK
 UD - UPPER DECK
 → TRAVEL DIRECTION

NOT TO SCALE

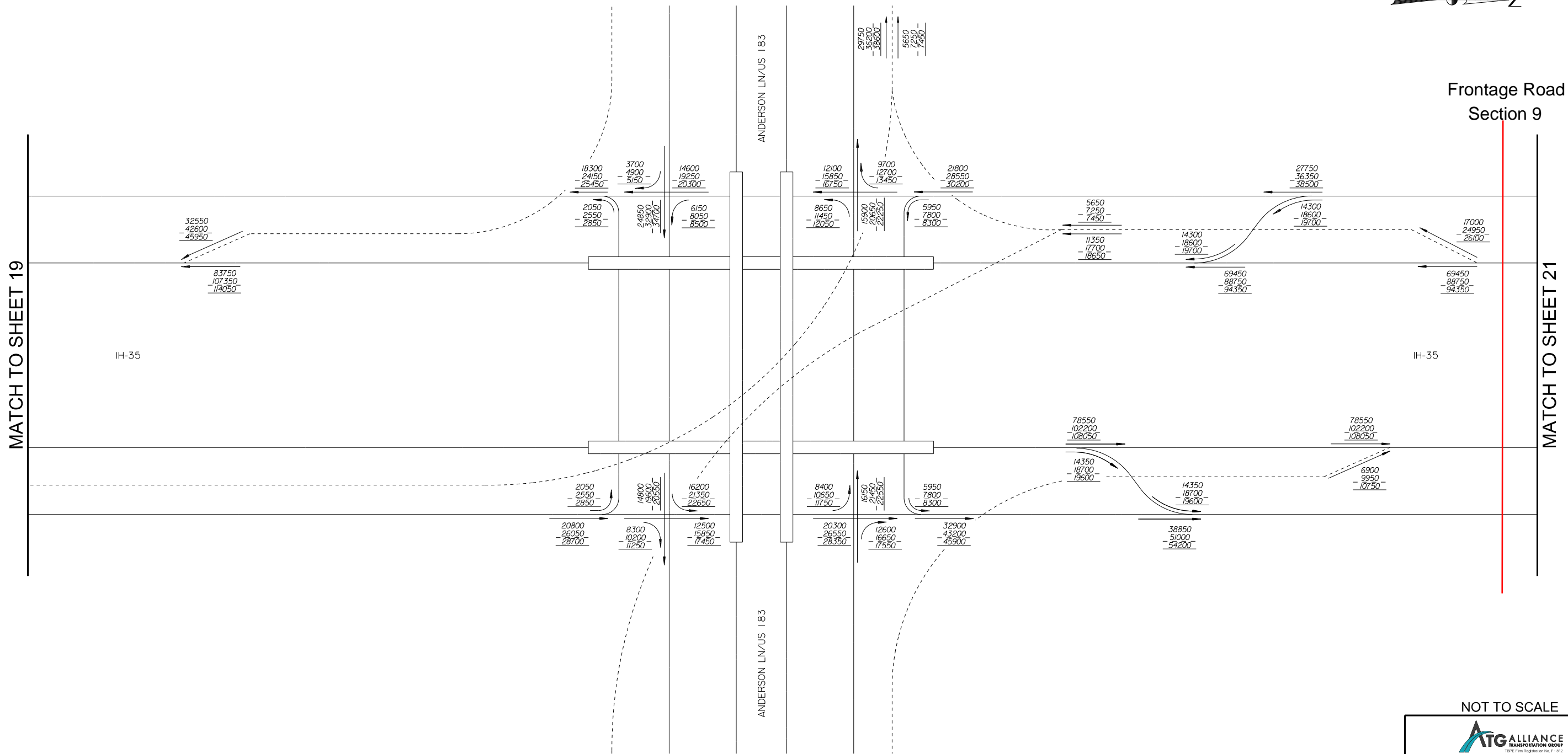
CAPITAL EXPRESS
 NO-BUILD CONFIGURATION
 24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 19 |

NO-BUILD CONFIGURATION



Frontage Road
Section 9




2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



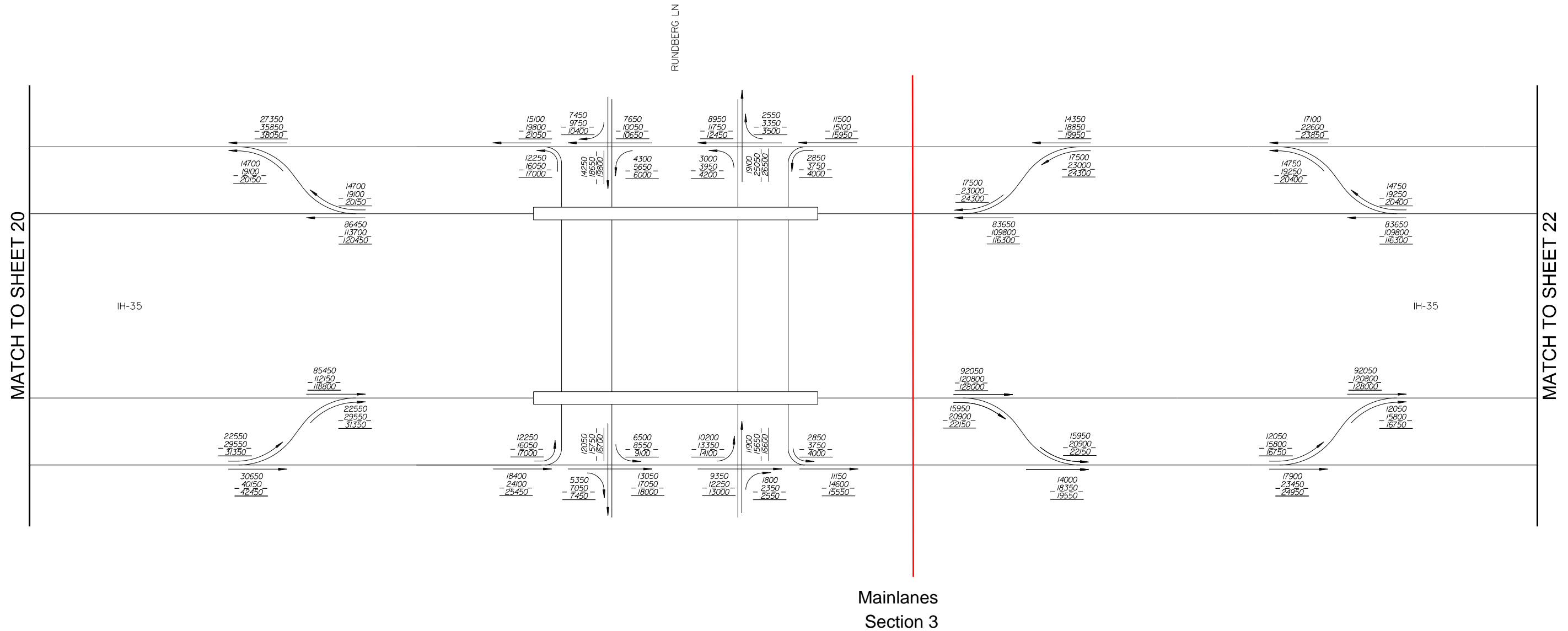
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 20 OF 28)

| | | | |
|------------------|----------------|---------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 20 |

NO-BUILD CONFIGURATION



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

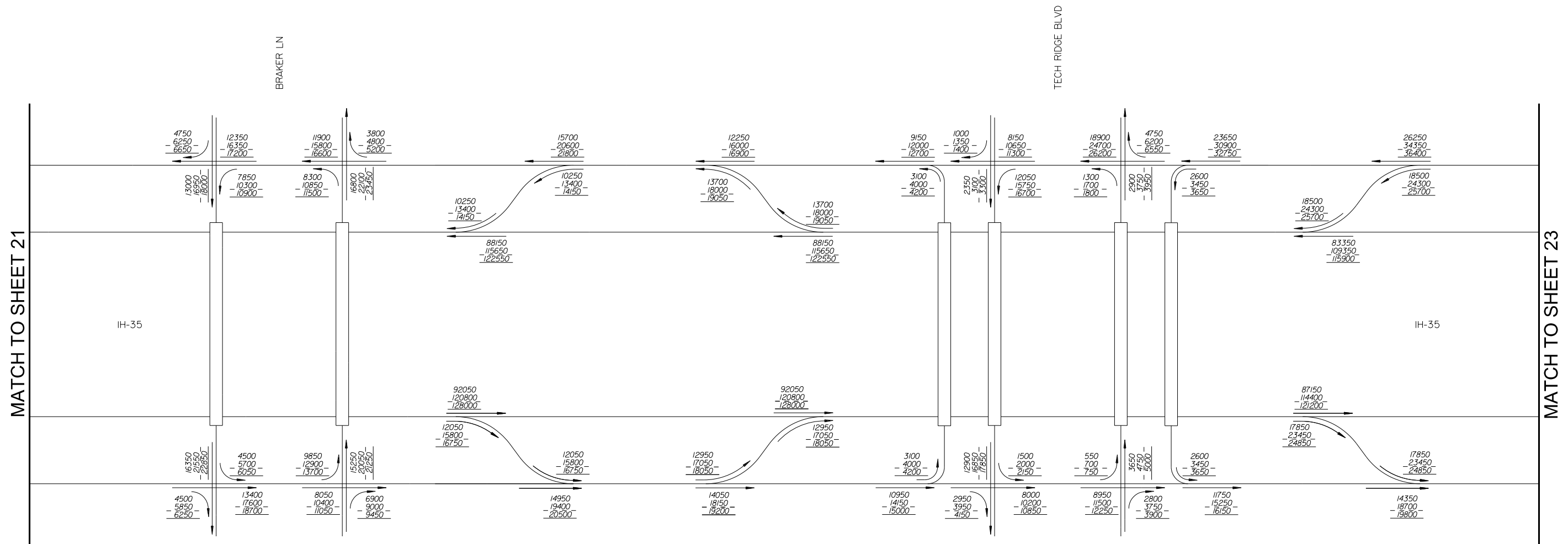


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 21 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 21 |

NO-BUILD CONFIGURATION



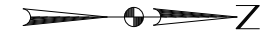
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- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

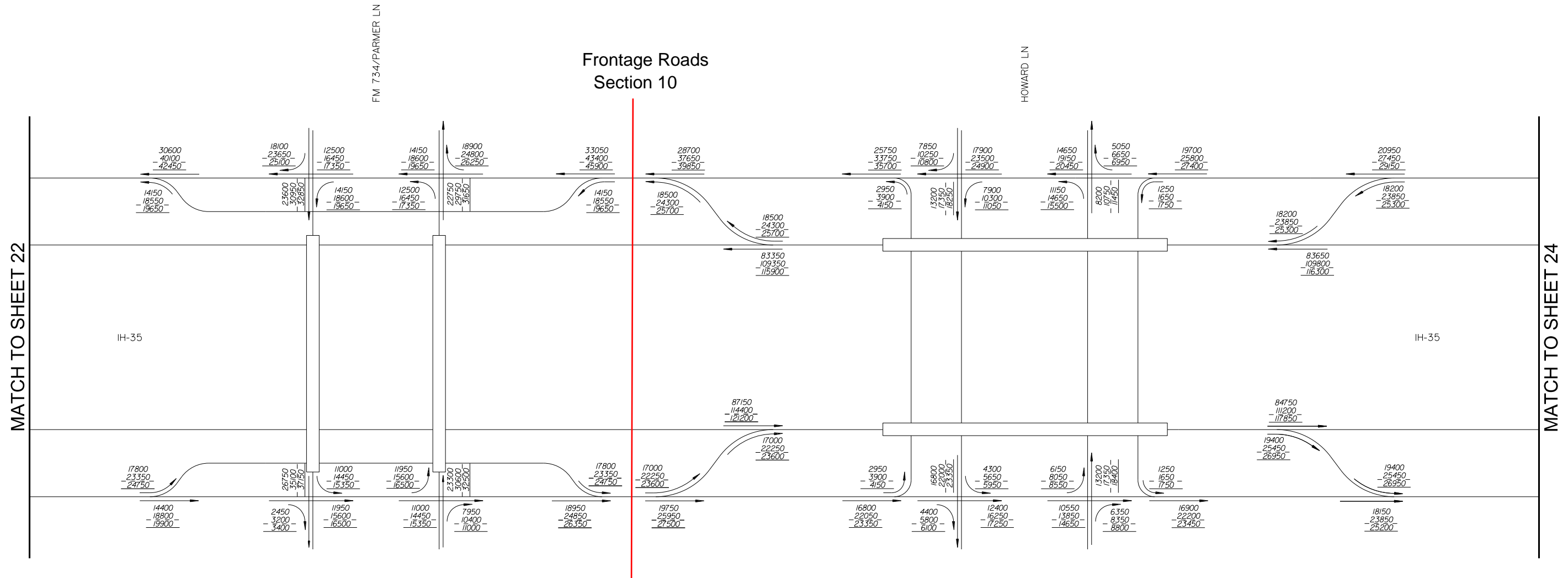
NOT TO SCALE

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| | | | | |
| | | | | |
| CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 22 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 22 |

NO-BUILD CONFIGURATION



Frontage Roads Section 10



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

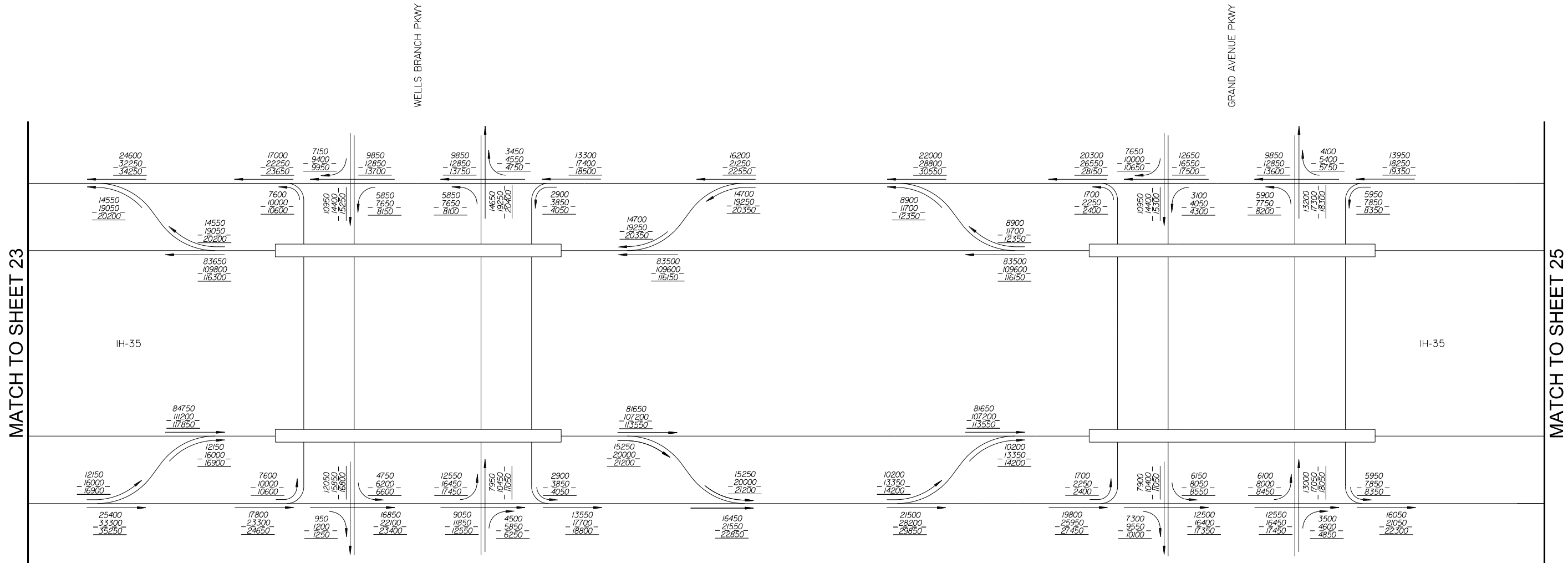


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 23 OF 28)

| | | | | |
|------------------|----------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 23 |

NO-BUILD CONFIGURATION





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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 LD - LOWER DECK
 UD - UPPER DECK
 → TRAVEL DIRECTION

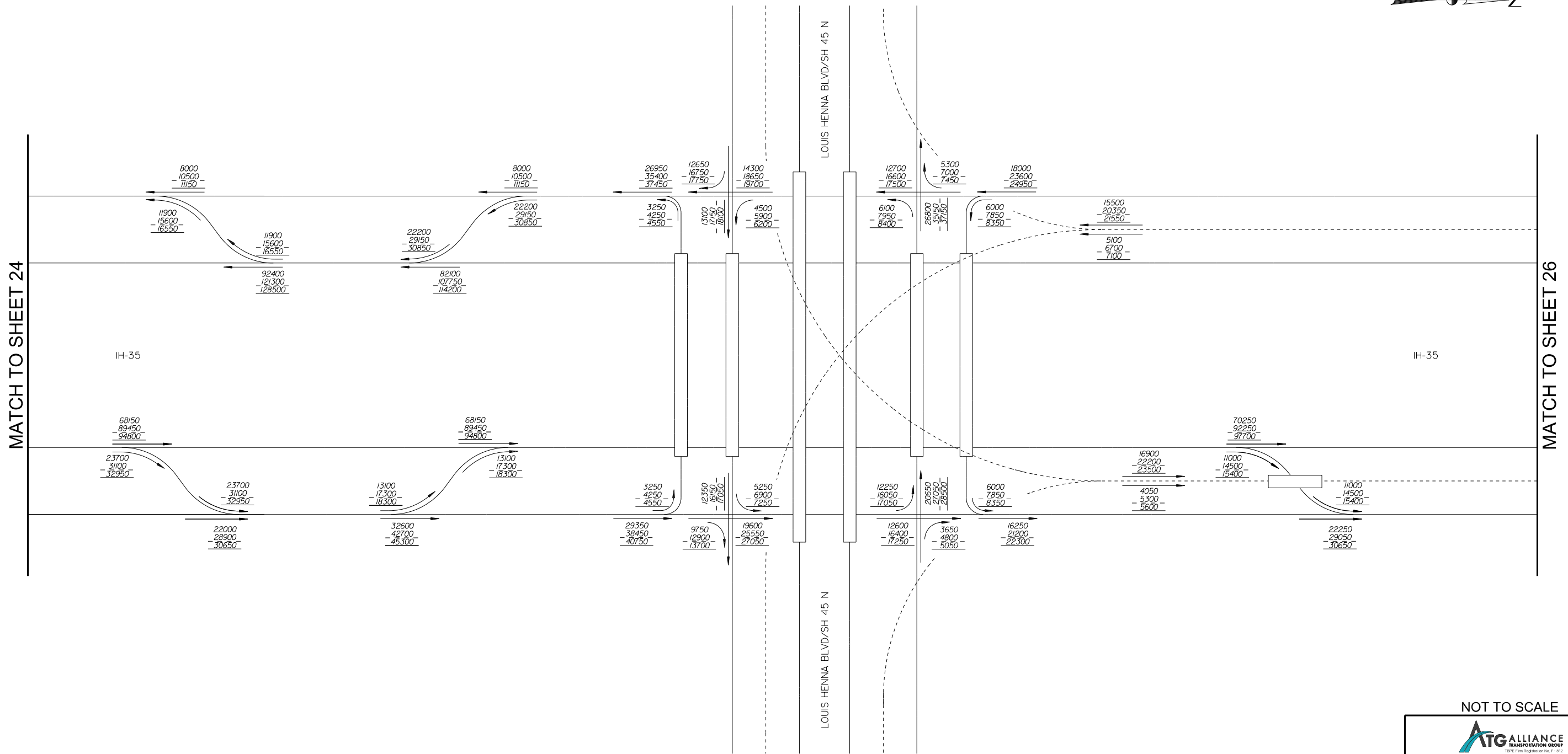
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 24 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 24 |

NO-BUILD CONFIGURATION





2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

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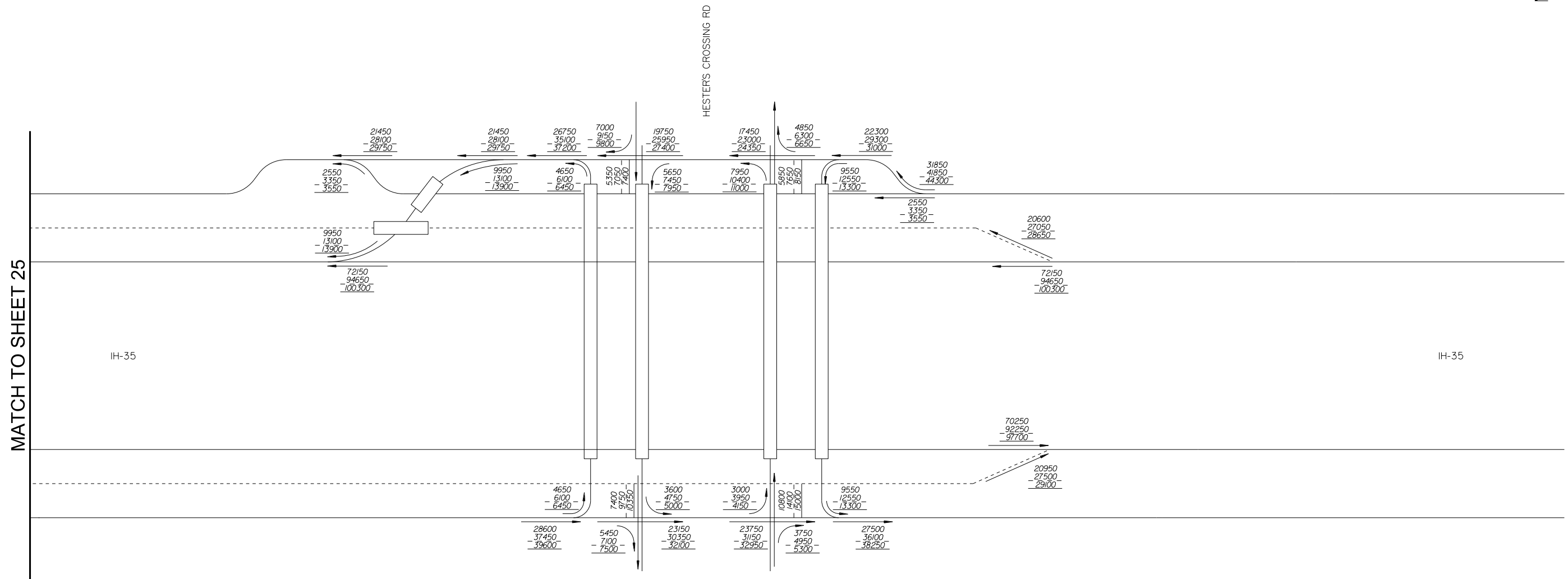
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 25 OF 28)

| | | | |
|------------------|----------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 25 |

NO-BUILD CONFIGURATION



... \2018.0011 *LineDiagrams*TPP*NB.dgn

THouston

11:12:08 AM

1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

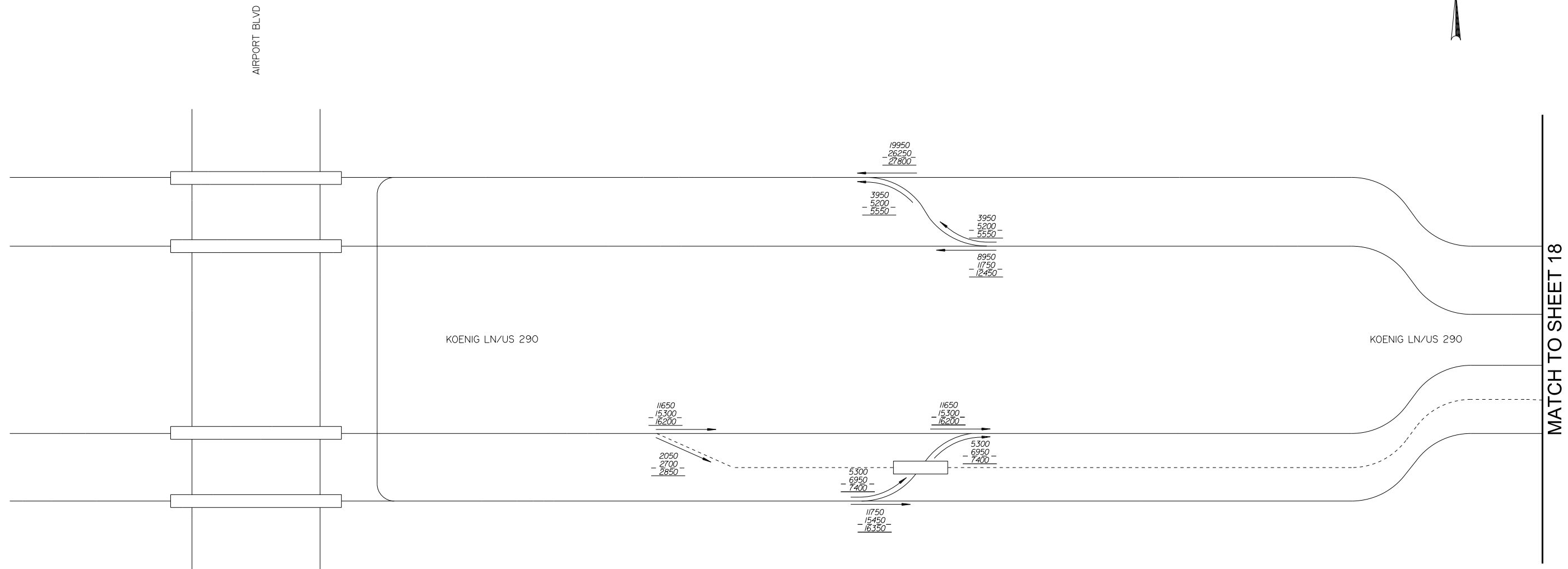


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 26 OF 28)

| | | | | |
|------------------|----------------|-------------------|------------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | WILLIAMSON | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 26 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

ATG ALLIANCE
TRANSPORTATION GROUP

Texas Department of Transportation

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 27 OF 28)

SCALE : N. T. S. PROJECT NO.

| | | | |
|---------|----------------|---------------|--------------------|
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 27 |

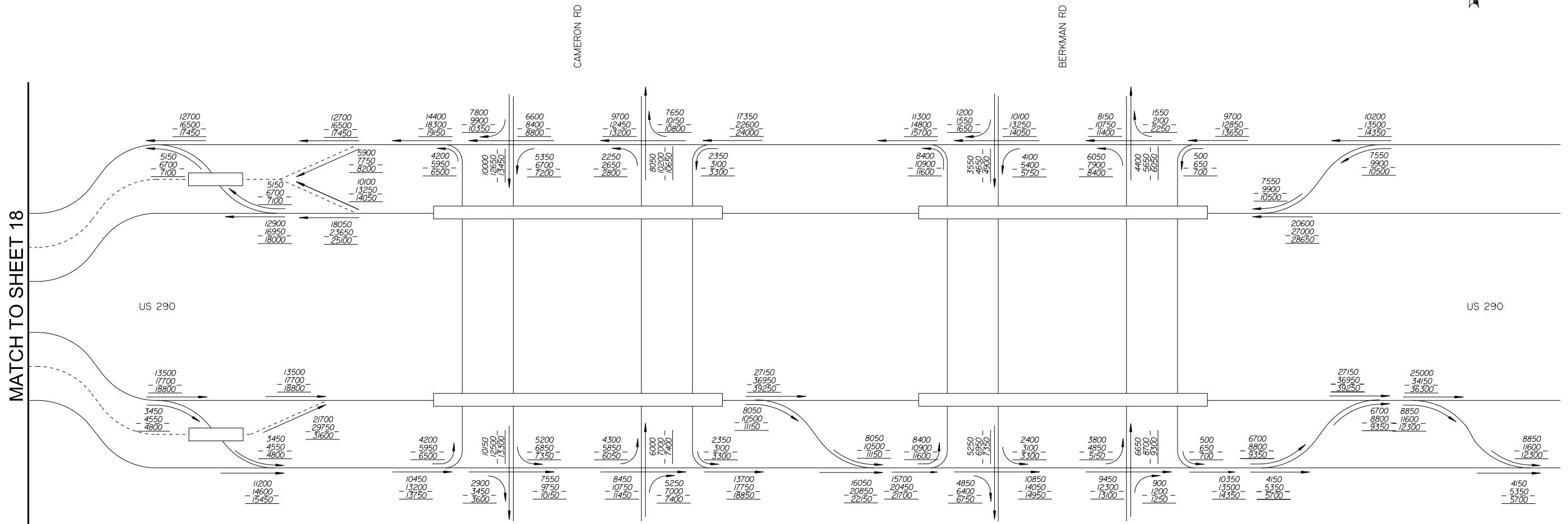
... \2018.0011 *LineDiagrams*TPP*NB.dgn

THouston

11:12:08 AM

1/25/2019


NO-BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



ATG ALLIANCE
TRANSPORTATION GROUP



Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 28 OF 28)

SCALE : N. T. S. PROJECT NO.

| | | | |
|---------|----------------|---------------|--------------------|
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 28 |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Mainlanes & Managed Lanes) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From MLK Blvd To St. Johns Ave Travis County | 234,700 | 293,200 | 51 - 49 | 6.0 | 8.9 | 4.0 | 13,600 | 20 | 83,750,500 | 3 | 117,583,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| Base Year | | | | | | | | | | | | |
| % of ADT | | | | | | | | | | | | |
| % of DHV | | | | | | | | | | | | |
| Light Duty | 91.1 | | 96.0 | | | | | | | | | |
| Medium Duty | 2.3 | | 1.0 | | | | | | | | | |
| Heavy Duty | 6.6 | | 3.0 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Mainlanes & Managed Lanes) | | | | | | | | | | | | |
| Section 2 | | | | | | | | | | | | |
| From MLK Blvd To St. Johns Ave Travis County | 234,700 | 312,150 | 51 - 49 | 6.0 | 8.9 | 4.0 | 13,700 | 20 | 130,136,000 | 3 | 182,706,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|---|---------|------------|----------|----------------|--------|--------|--------------------------------|---|------------|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 1</u></p> <p>From William Cannon Drive To Ben White Blvd/SH 71</p> <p>Travis County</p> | | | | | | | | | | | |
| 110,500 | 145,350 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,100 | 30 | 9,045,000 | 3 | 11,096,000 | 8" | |
| <p align="center">Data for Use in Air & Noise Analysis</p> | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 97.2 | | 97.9 | | | | | | | | | |
| Medium Duty | 1.7 | | 1.3 | | | | | | | | | |
| Heavy Duty | 1.1 | | 0.8 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 1</u></p> <p>From William Cannon Drive To Ben White Blvd/SH 71</p> <p>Travis County</p> | | | | | | | | | | | |
| 110,500 | 154,100 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,200 | 30 | 14,031,500 | 3 | 17,213,500 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Ben White Blvd/SH 71 To Oltorf Street</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 48,600 | 59,250 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 5,525,500 | 3 | 6,811,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 95.9 | | 96.9 | | | | | | | | | |
| Medium Duty | 2.4 | | 1.8 | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.3 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Ben White Blvd/SH 71 To Oltorf Street</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 48,600 | 63,450 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 8,611,500 | 3 | 10,614,500 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | |
|---|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | |
| <u>I-35 (Build Frontage Roads)</u> <u>Section 3</u> From Oltorf Street To MLK Blvd Travis County | | | | | | | | | | 113,700 | 143,450 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,200 | 30 | 9,090,500 | 3 | 11,152,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | |
| Light Duty | 97.2 | | 97.9 | | | | | | | | | | | | | | | | | | |
| Medium Duty | 1.7 | | 1.3 | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.1 | | 0.8 | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | |
| <u>I-35 (Build Frontage Roads)</u> <u>Section 3</u> From Oltorf Street To MLK Blvd Travis County | | | | | | | | | | 113,700 | 151,650 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,200 | 30 | 14,071,000 | 3 | 17,262,500 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 4</u></p> <p>From MLK Blvd To 38 1/2th Street</p> <p>Travis County</p> | | | | | | | | | | | | | | |
| | 47,300 | 60,750 | 51 - 49 | 6.0 | 4.2 | 3.2 | 11,900 | 30 | 5,668,000 | 3 | 6,988,000 | 8" | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | |
| Light Duty | 95.8 | | 96.8 | | | | | | | | | | | |
| Medium Duty | 2.5 | | 1.9 | | | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.3 | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 4</u></p> <p>From MLK Blvd To 38 1/2th Street</p> <p>Travis County</p> | | | | | | | | | | | | | | |
| | 47,300 | 65,400 | 51 - 49 | 6.0 | 4.2 | 3.2 | 11,900 | 30 | 8,868,000 | 3 | 10,933,500 | 8" | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 5</u></p> <p>From 38 1/2th Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 132,050 | 166,000 | 51 - 49 | 6.0 | 2.7 | 2.0 | 12,200 | 30 | 10,172,500 | 3 | 12,472,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 97.3 | | 98.0 | | | | | | | | | |
| Medium Duty | 1.6 | | 1.2 | | | | | | | | | |
| Heavy Duty | 1.1 | | 0.8 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 5</u></p> <p>From 38 1/2th Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 132,050 | 177,800 | 51 - 49 | 6.0 | 2.7 | 2.0 | 12,300 | 30 | 15,863,000 | 3 | 19,450,000 | 8" |

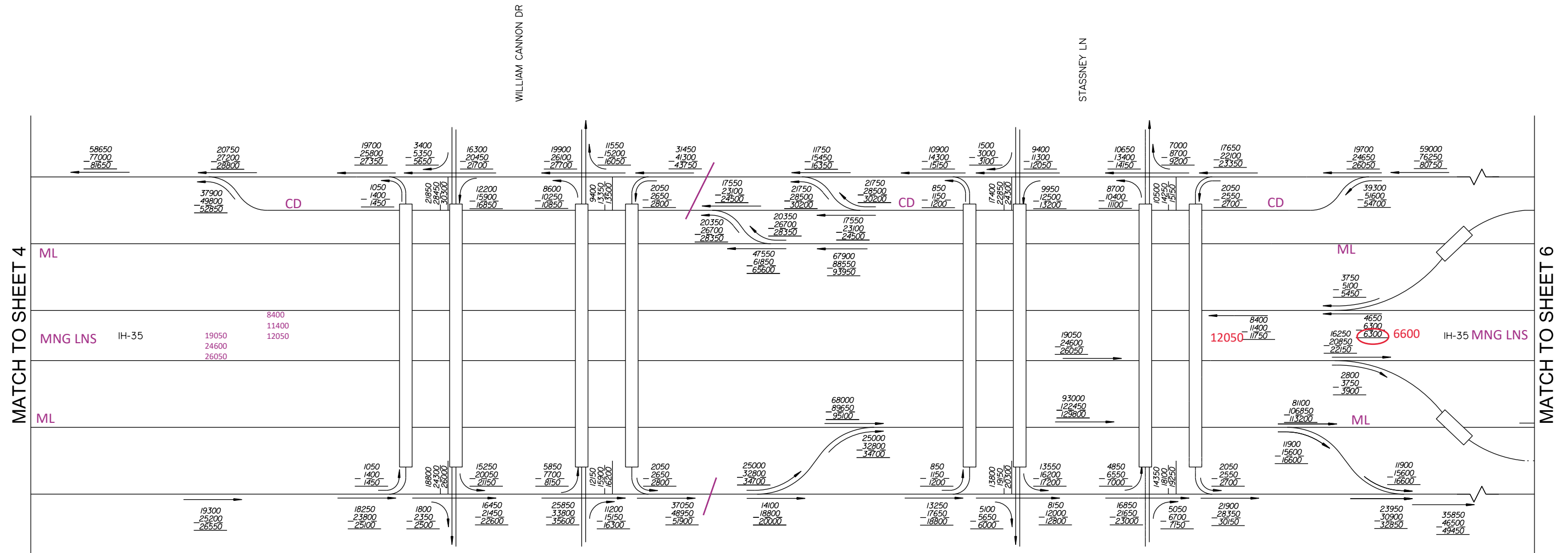
TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | | | |
|--|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--------|---------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From US 290 To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | | 74,050 | 91,600 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 6,868,000 | 3 | 8,444,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.7 | | 97.5 | | | | | | | | | | | | | | | | | | | | | |
| Medium Duty | 2.0 | | 1.5 | | | | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From US 290 To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | | 74,050 | 100,350 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 10,846,000 | 3 | 13,336,000 | 8" |

BUILD CONFIGURATION



BUILD SECTION 1:
 From William Cannon Dr
 To Ben White Blvd/SH 71
 Frontage Roads (Collector Distributor Lanes included)
 110500
 145350
 154100

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE



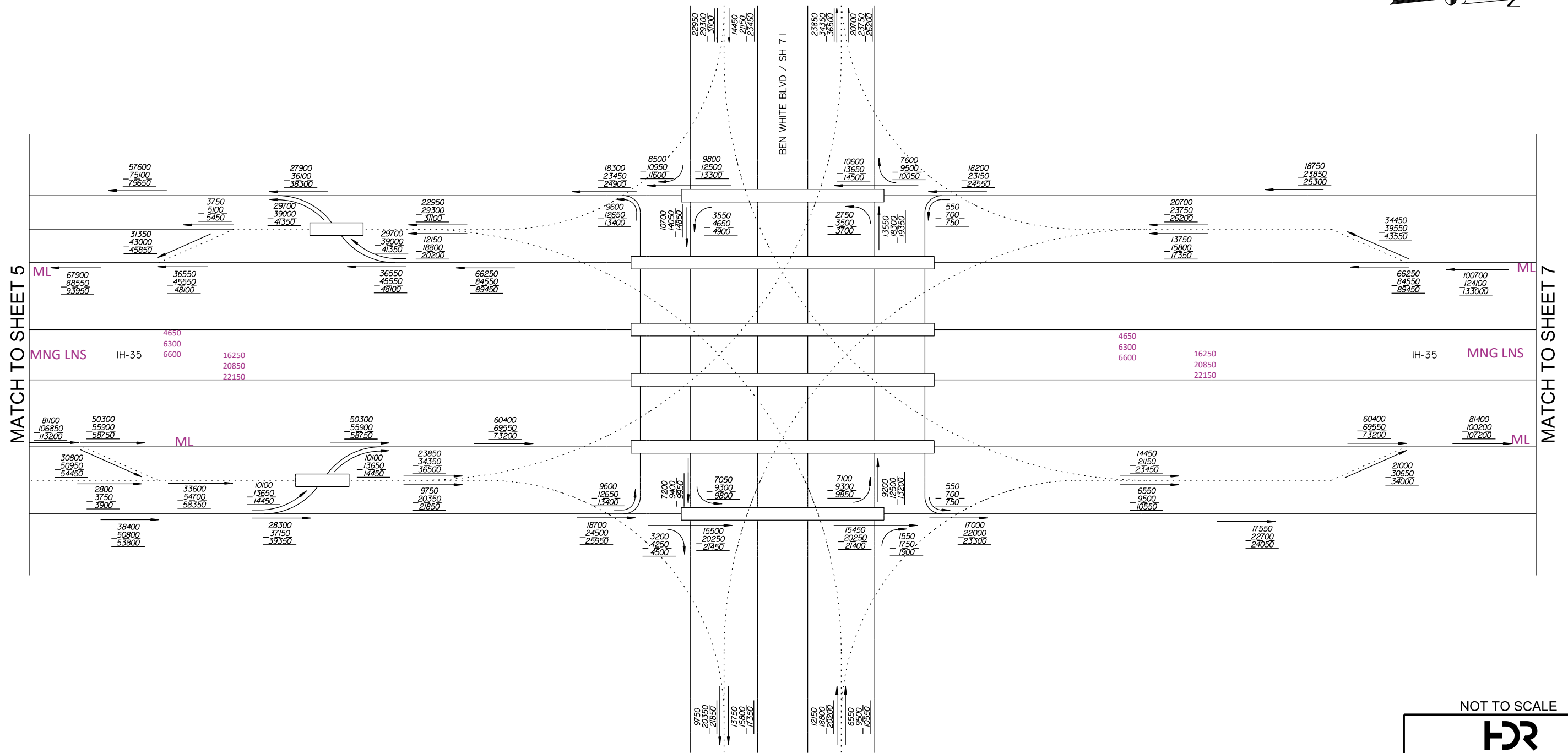
Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION

24 HOUR VOLUMES
 (SHEET 5 OF 28)

| | | | | |
|-----------------|----------|-------------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |


BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



HDR



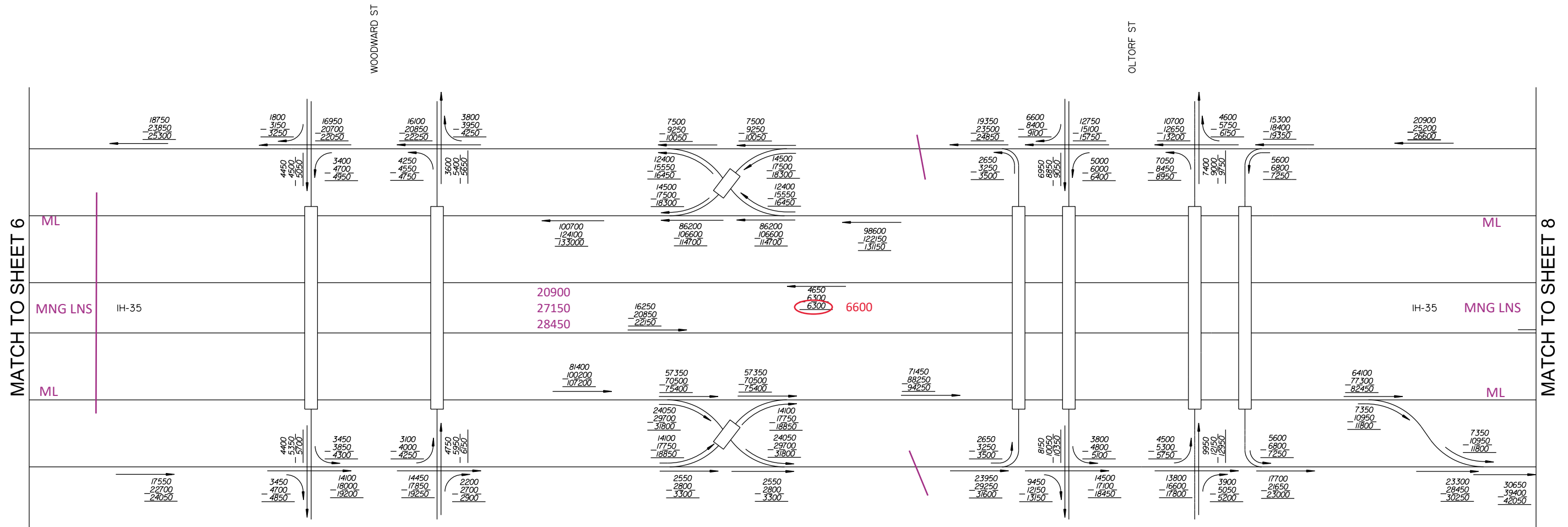
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 6 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 6 |

BUILD CONFIGURATION



BUILD SECTION 1:
From William Cannon Dr
To MLK Blvd

ML+Managed Lanes
203000
251450
268950

BUILD SECTION 2:
From Ben White Blvd/SH 71
To Oltorf Street

Frontage Roads
48600
59250
63450

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
→ TRAVEL DIRECTION

NOT TO SCALE

Texas Department of Transportation

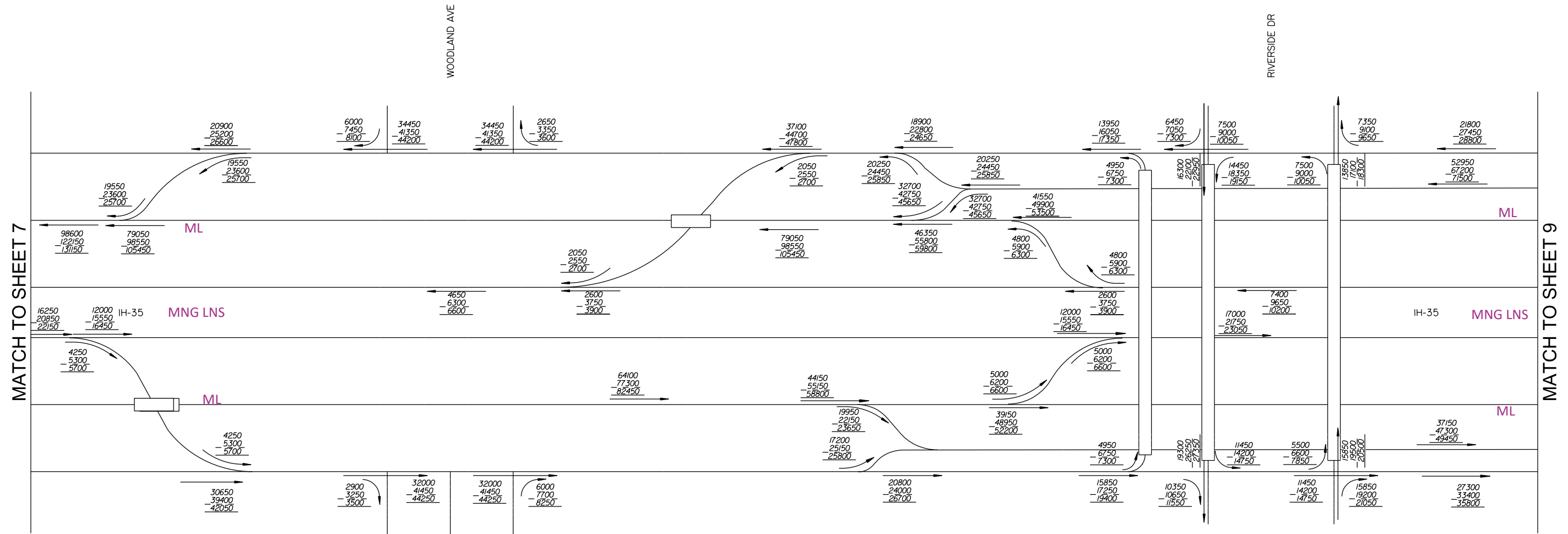
CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 7 OF 28)

SCALE: N. T. S. PROJECT NO.

| | | | |
|---------|----------------|-------------------|--------------------|
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 7 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE



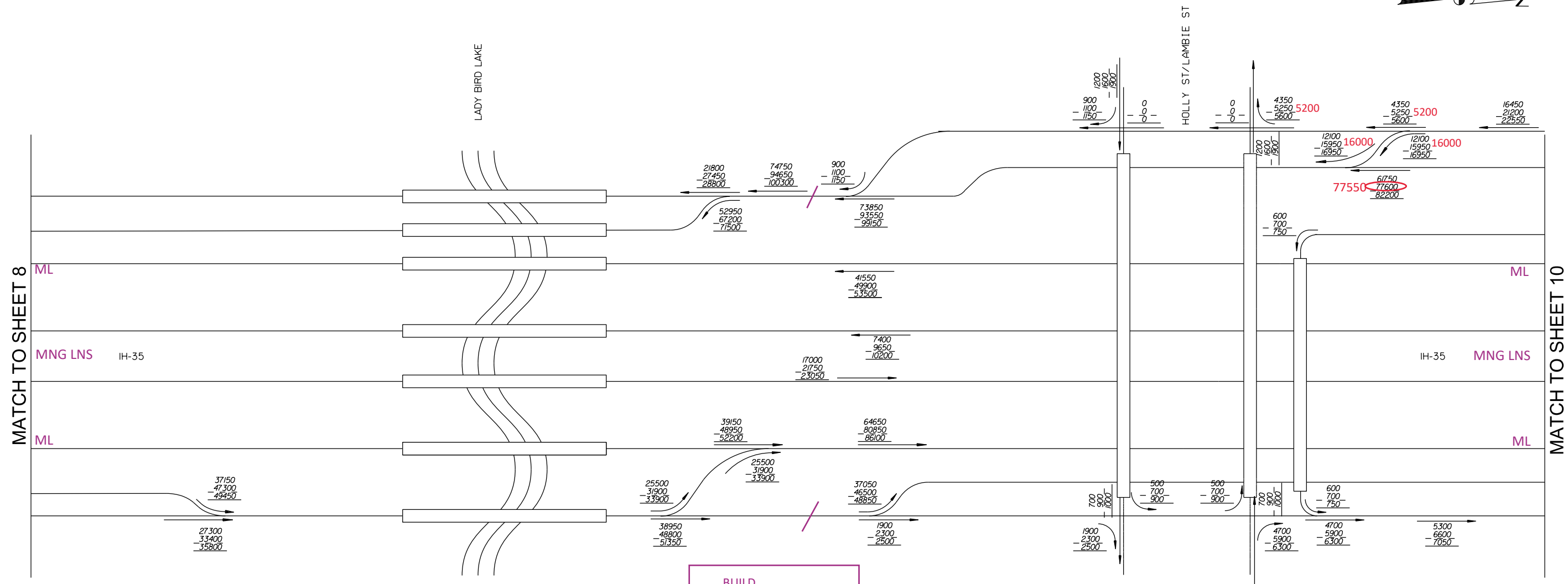
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 8 OF 28)

| | | | | |
|-----------------|----------------|---------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 8 |

BUILD CONFIGURATION



BUILD SECTION 3:
From Oltorf Street
To MLK Blvd
Frontage Roads
113700
143450
151650

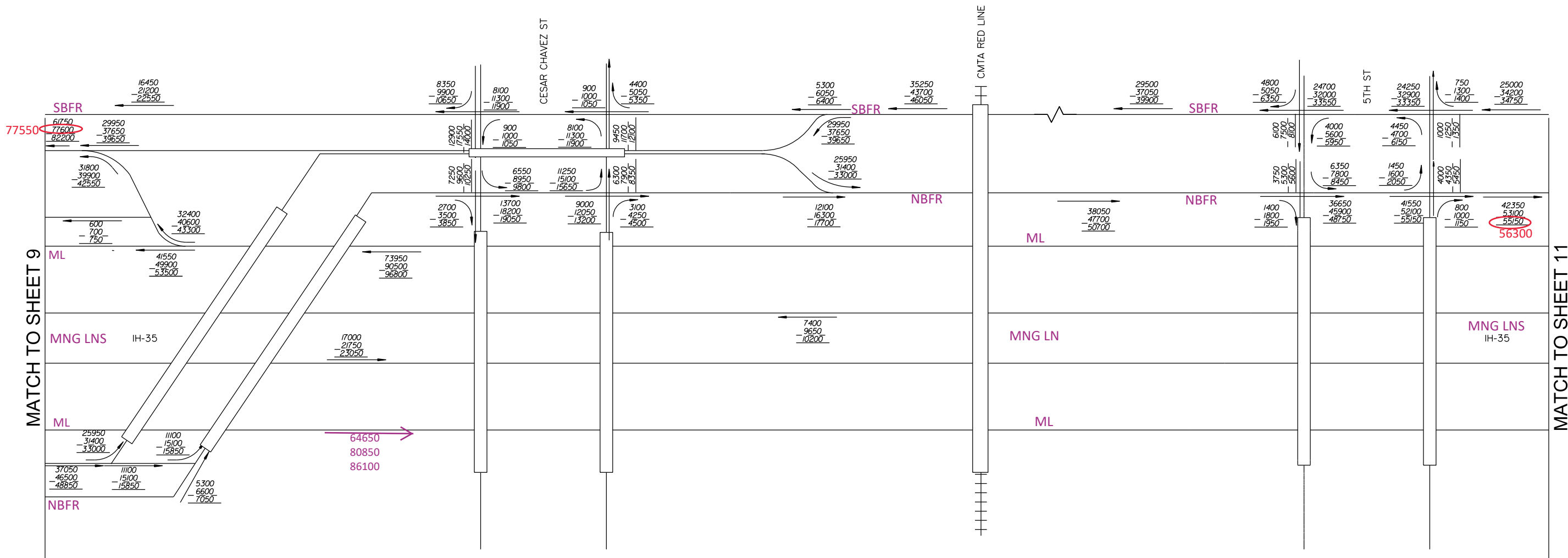
2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

HR
 Texas Department of Transportation
CAPITAL EXPRESS
 BUILD CONFIGURATION
 24 HOUR VOLUMES
 (SHEET 9 OF 28)
 SCALE: N.T.S. PROJECT NO.
 DWN: TH CKD: HH
 STATE DISTRICT FED. RD. DIV. NO. COUNTY
 TEXAS 14 6 TRAVIS
 CONTROL SECTION JOB HWY. NO. SHEET NO.
 5000 00 106 IH-35 9

BUILD CONFIGURATION




MATCH TO SHEET 9

MATCH TO SHEET 11

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



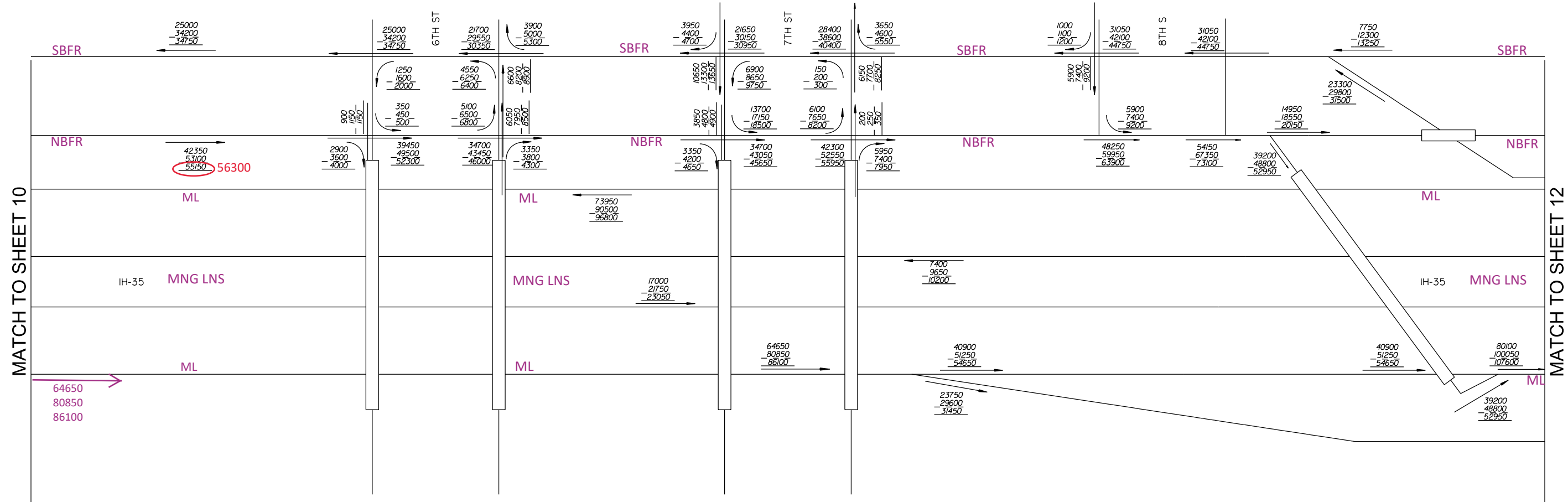
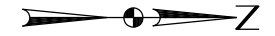
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 10 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 10 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

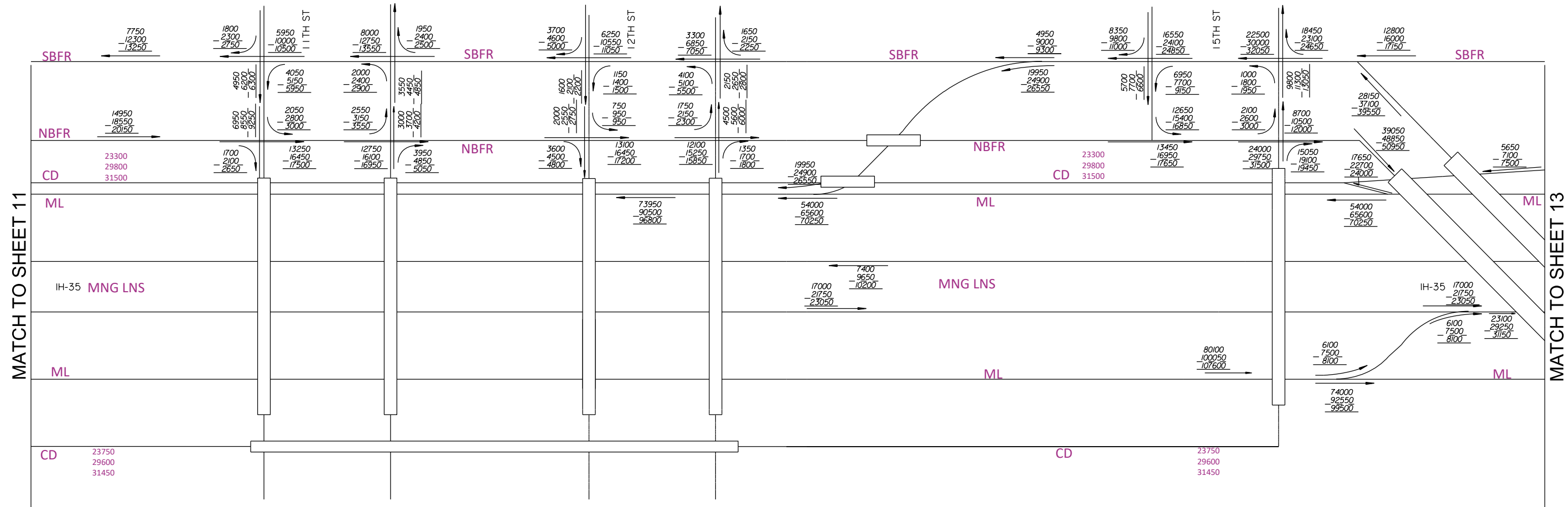


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 11 OF 28)

| | | | | |
|-----------------|----------|---------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 11 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE

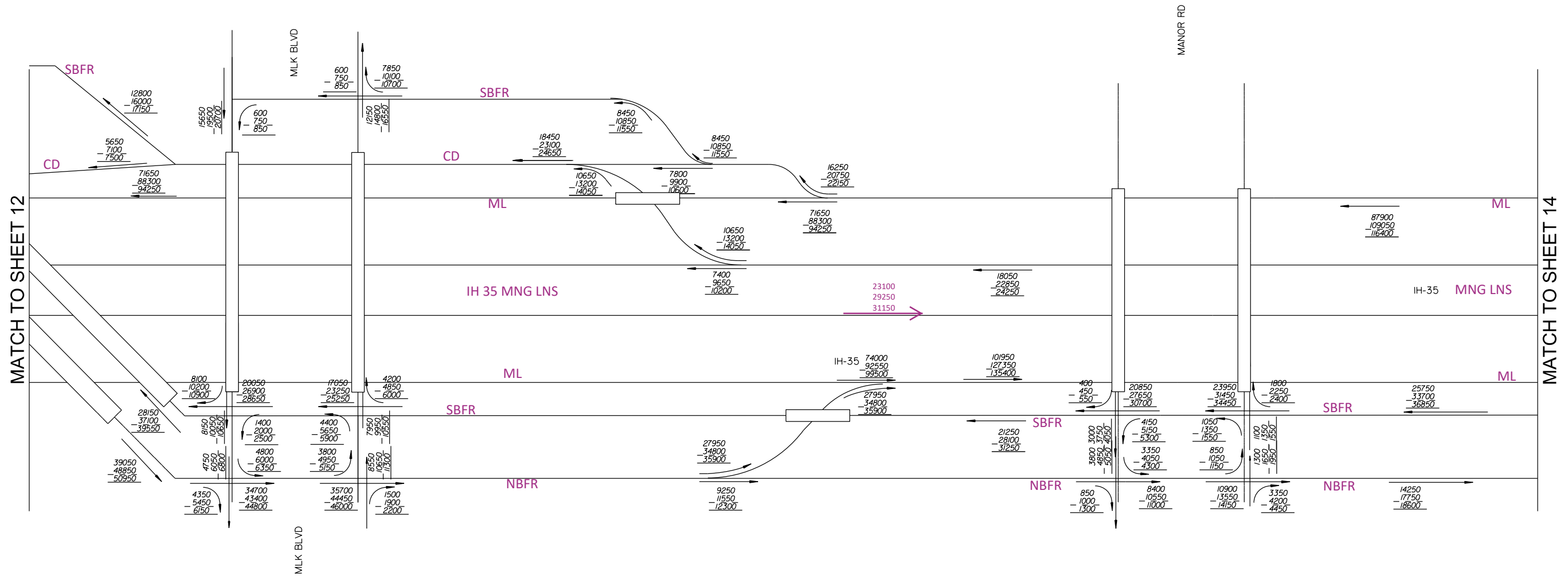
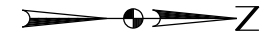


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 12 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 12 |


BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 13 OF 28)

SCALE: N. T. S. PROJECT NO.

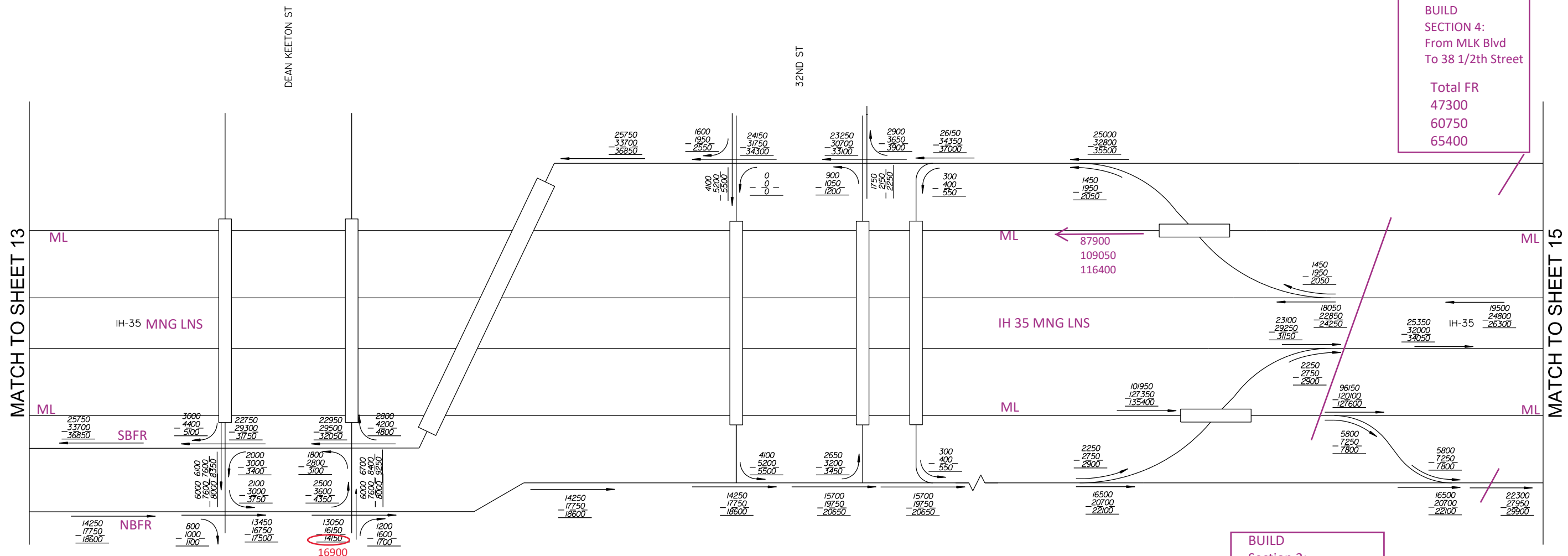
| | | | |
|---------|----------|-------------------|--------------------|
| DWN: TH | CKD: HH | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 13 |

BUILD CONFIGURATION



BUILD SECTION 4:
From MLK Blvd
To 38 1/2th Street

Total FR
47300
60750
65400



BUILD Section 2:
From MLK Blvd
To St. Johns Ave

ML+Managed Lanes
234700
293200
312150

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE



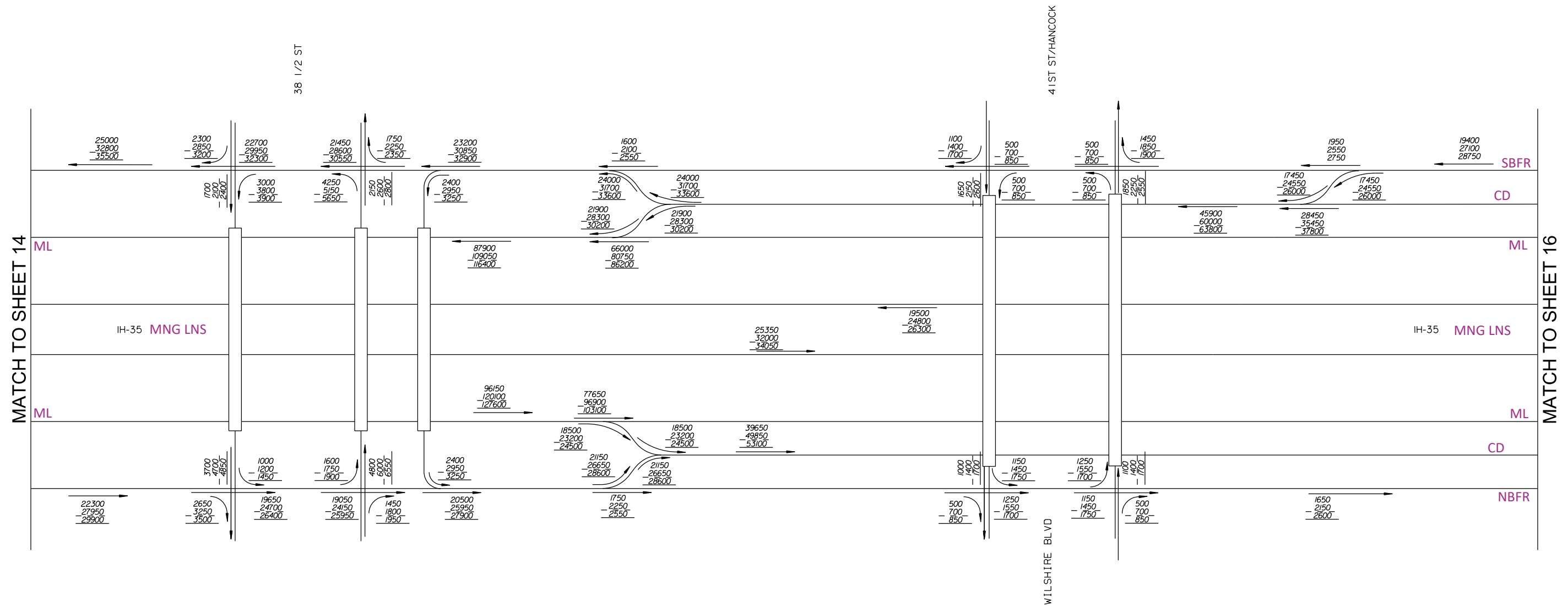
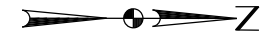
Texas Department of Transportation

CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 14 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 14 |


BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



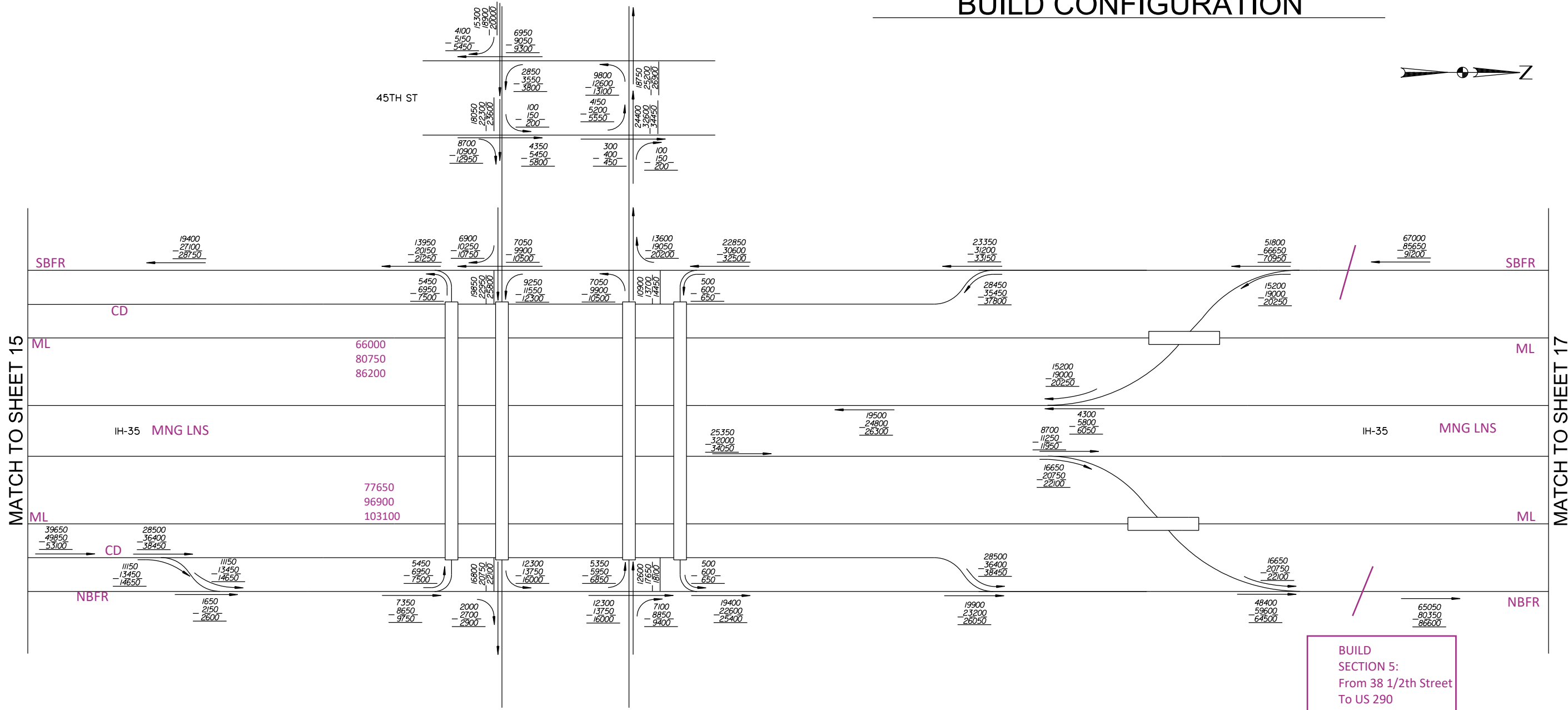
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 15 OF 28)

| | | | |
|-----------------|---------|----------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE DISTRICT | FED. RD. DIV. NO. |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 15 |

BUILD CONFIGURATION



MATCH TO SHEET 15

MATCH TO SHEET 17

AIRPORT BLVD

BUILD SECTION 5:
From 38 1/2th Street
To US 290

Total FR
132050
166000
177800

NOT TO SCALE



CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 16 OF 28)

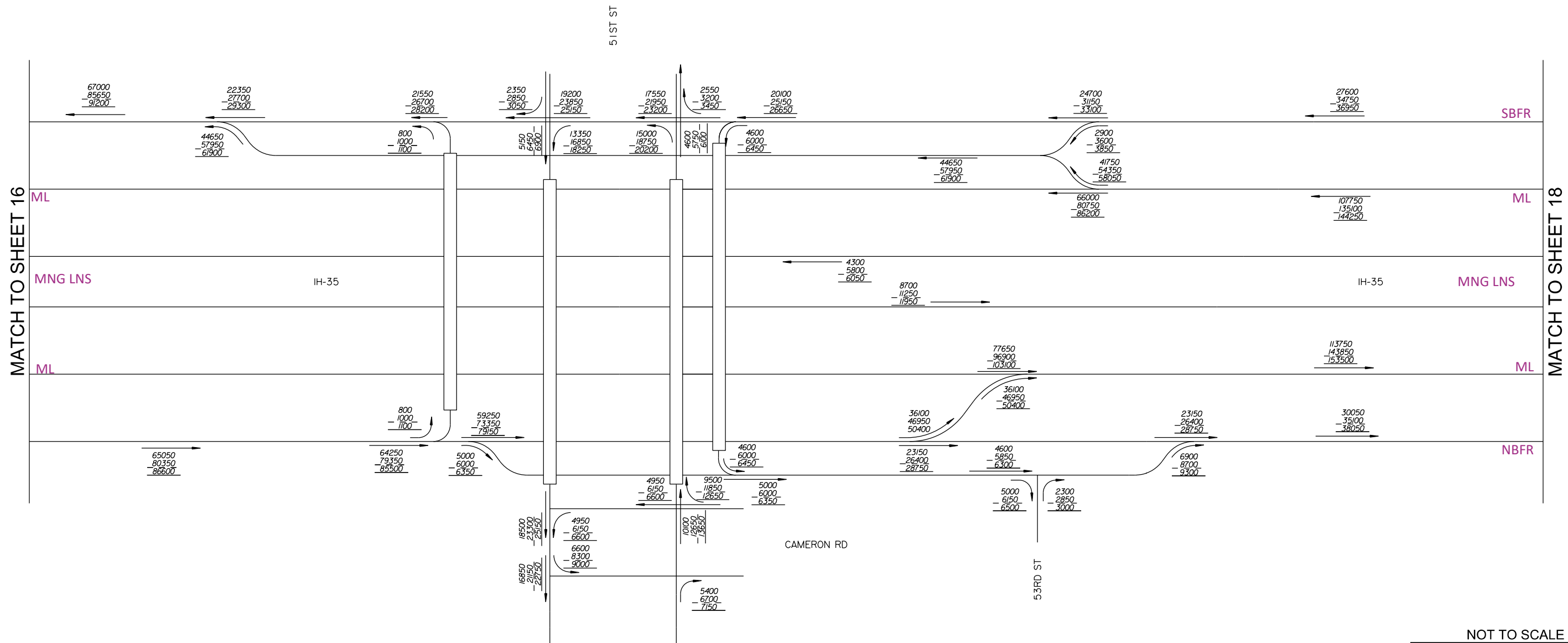
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| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE DISTRICT | FED. RD. DIV. NO. |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



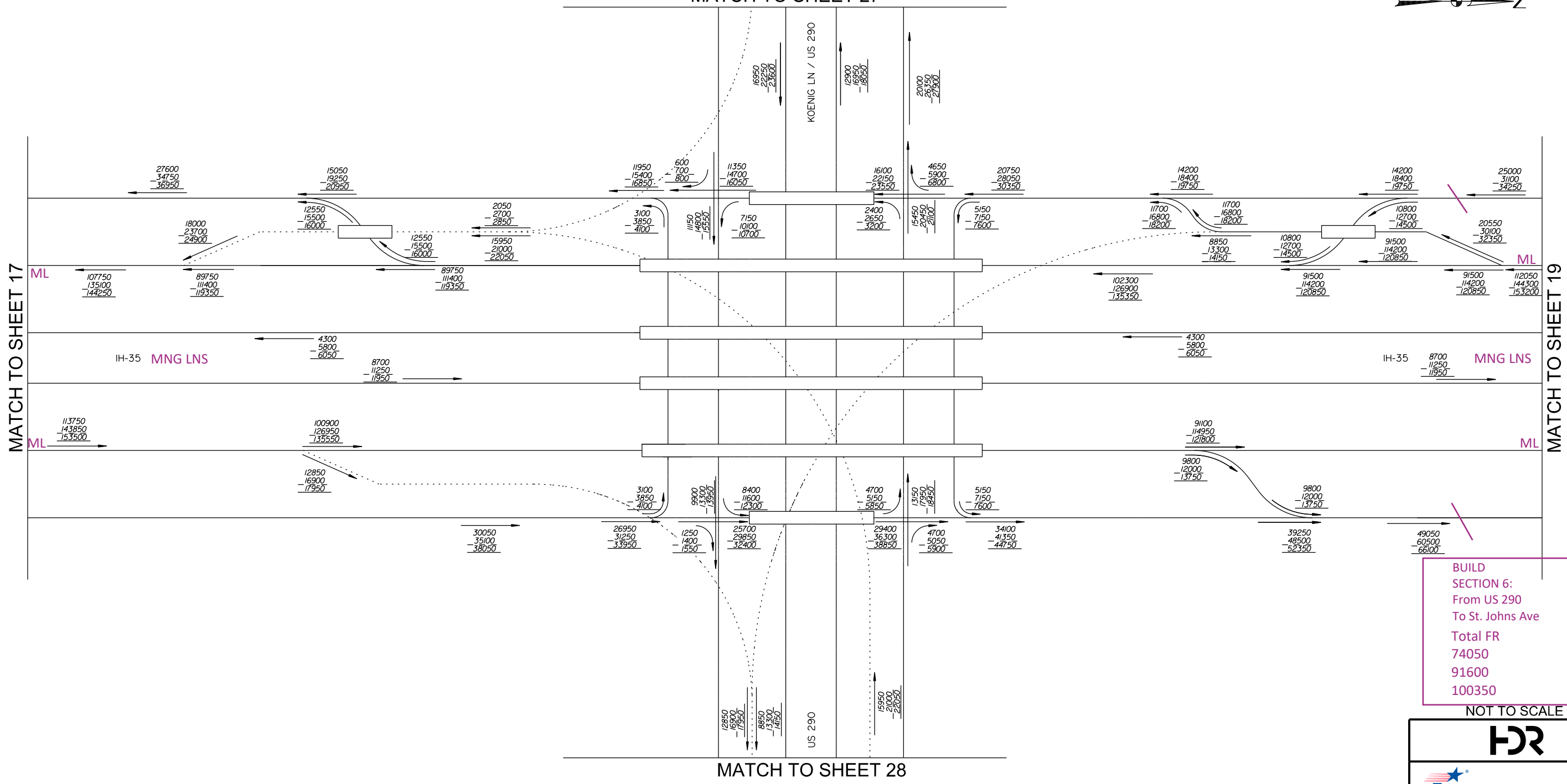
CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 17 OF 28)

| | | | | | |
|------------------|----------------|-------------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 17 | |

BUILD CONFIGURATION

MATCH TO SHEET 27



MATCH TO SHEET 17

MATCH TO SHEET 19

MATCH TO SHEET 28

BUILD SECTION 6:
From US 290
To St. Johns Ave
Total FR
74050
91600
100350

NOT TO SCALE



CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 18 OF 28)

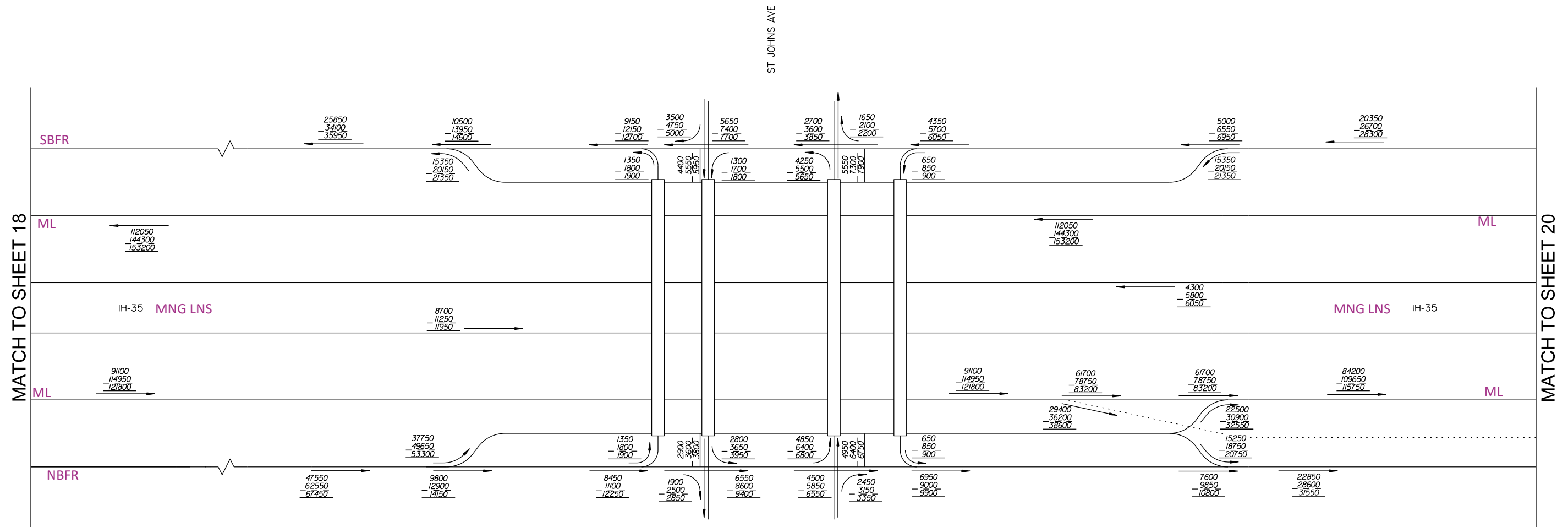
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|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

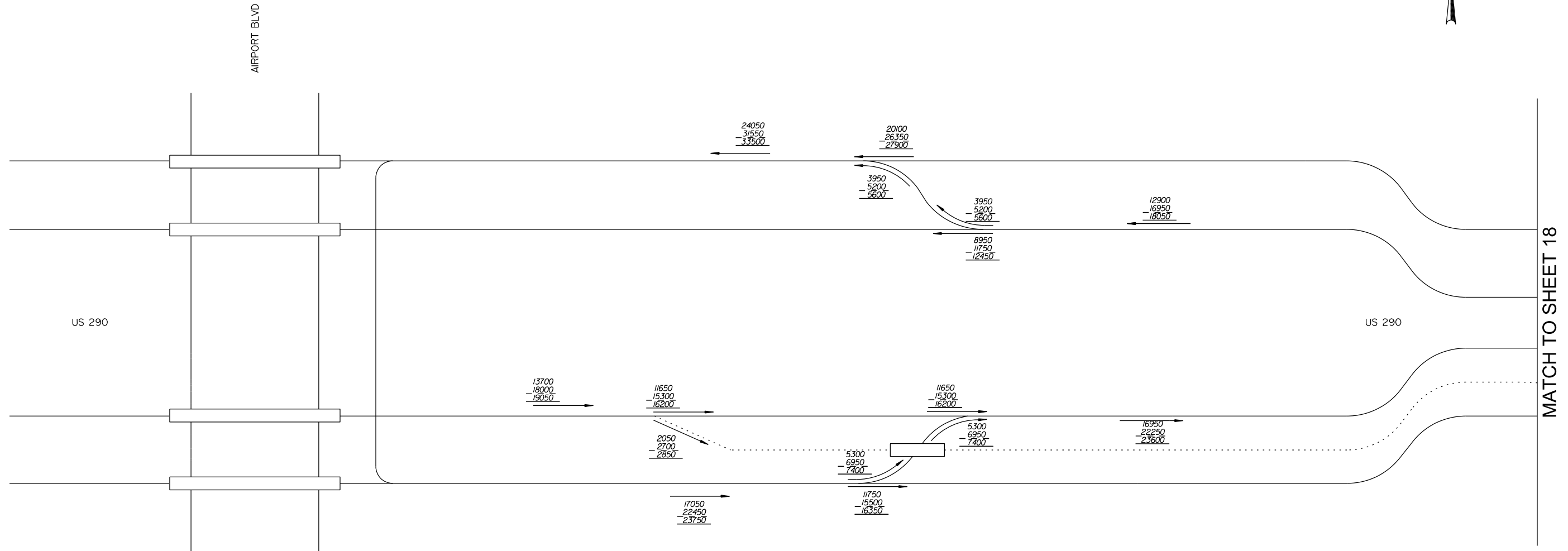


CAPITAL EXPRESS
 BUILD CONFIGURATION

24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | | |
|-----------------|----------------|-------------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 19 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE

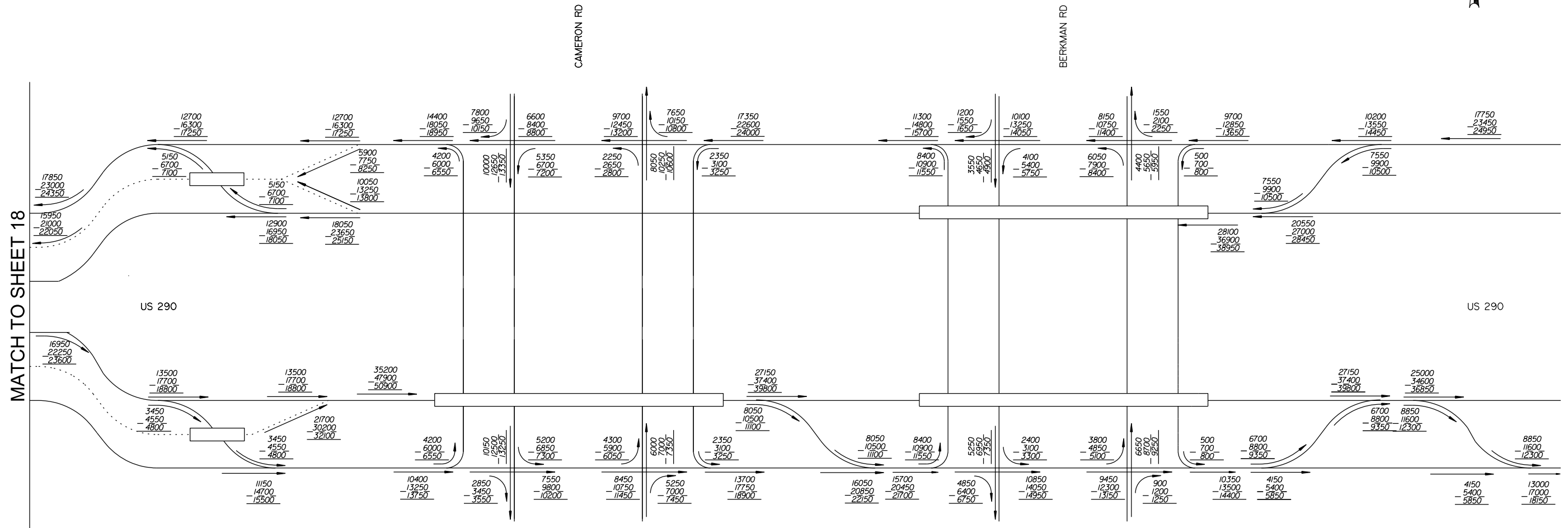


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 27 OF 28)

| | | | | |
|-----------------|----------------|-------------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 27 |

BUILD CONFIGURATION



MATCH TO SHEET 18

US 290

US 290

CAMERON RD

BERKMAN RD

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE



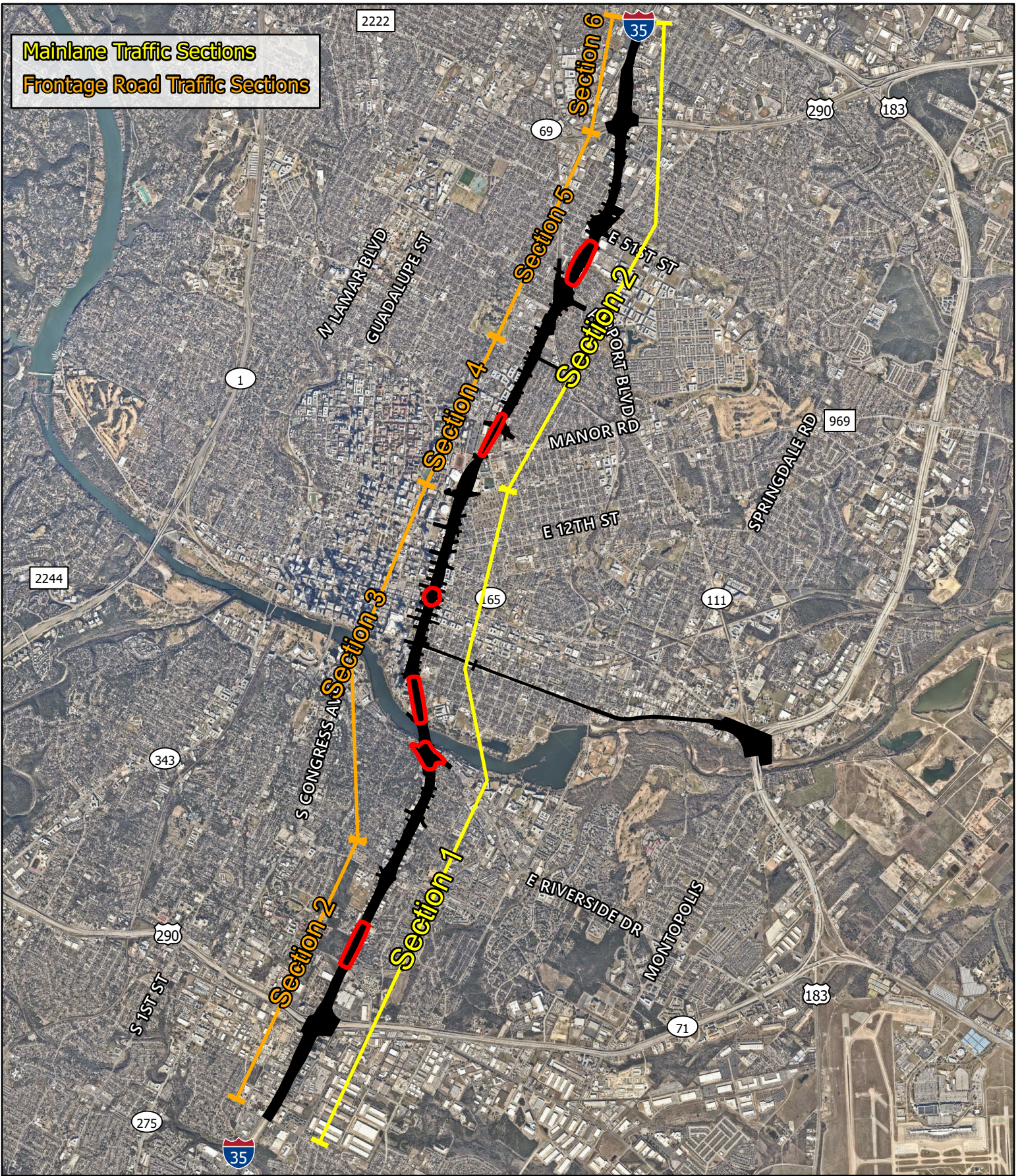
CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 28 OF 28)

| | | | | |
|-----------------|----------------|-------------------|-------------|-----------|
| SCALE: N. T. S. | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 28 |

APPENDIX C
CO Receptor Locations

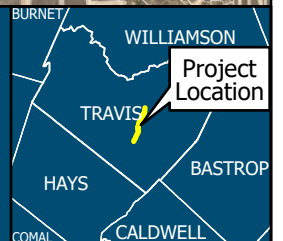
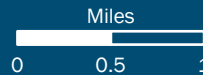
Mainlane Traffic Sections
Frontage Road Traffic Sections



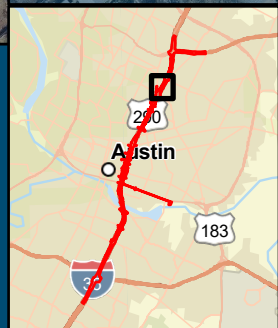
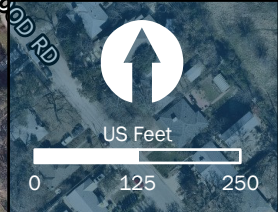
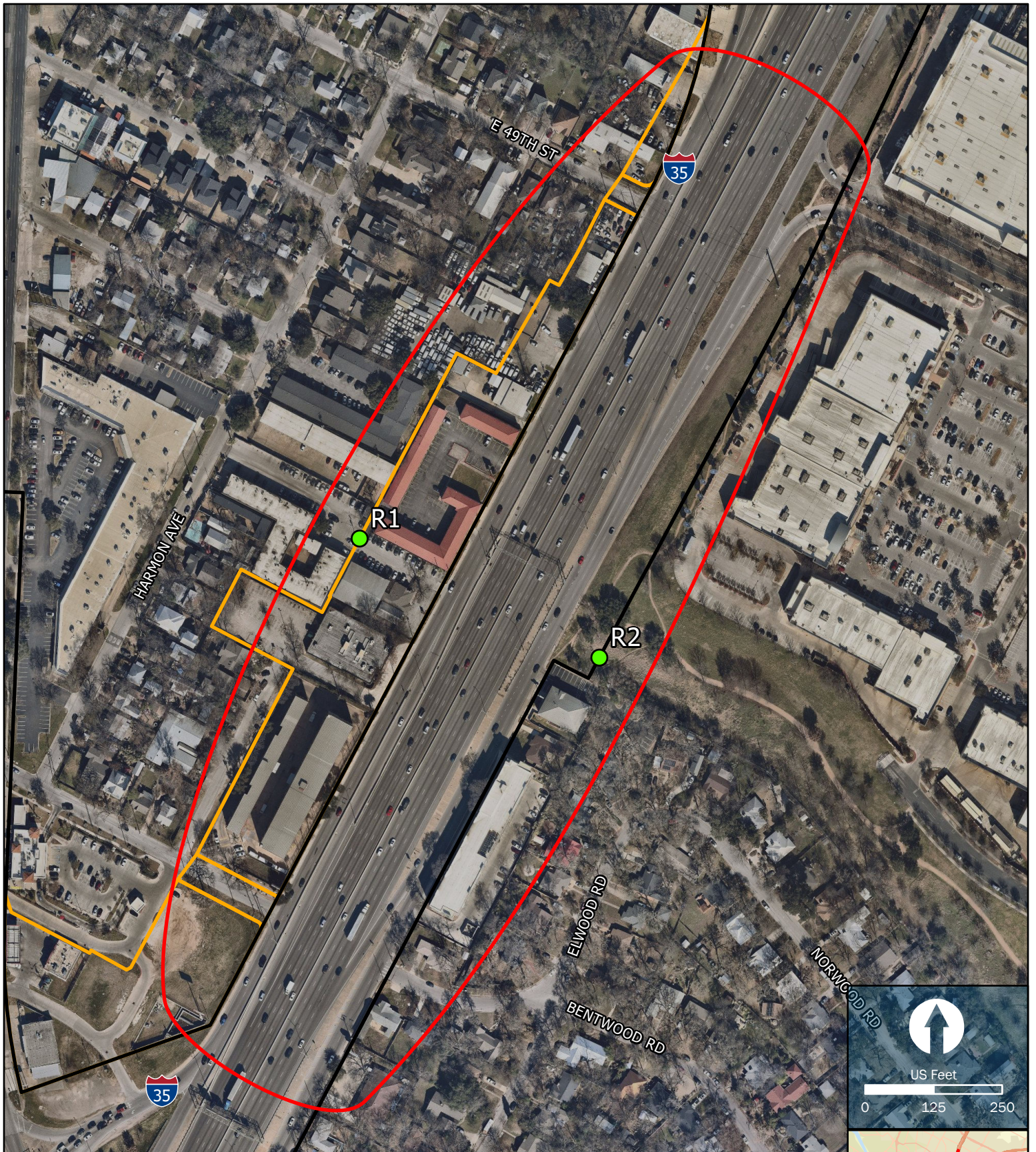
CO Modeling Locations Overview
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

- Project Location
- CO Modeling Area



Sources: ESRI Basemaps 2021







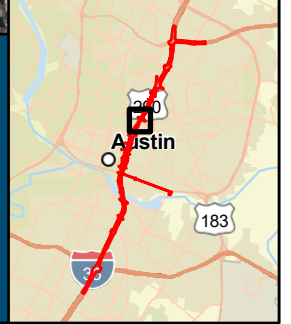
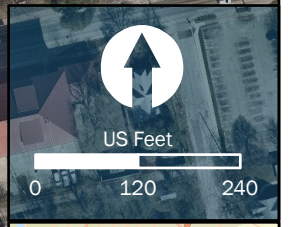
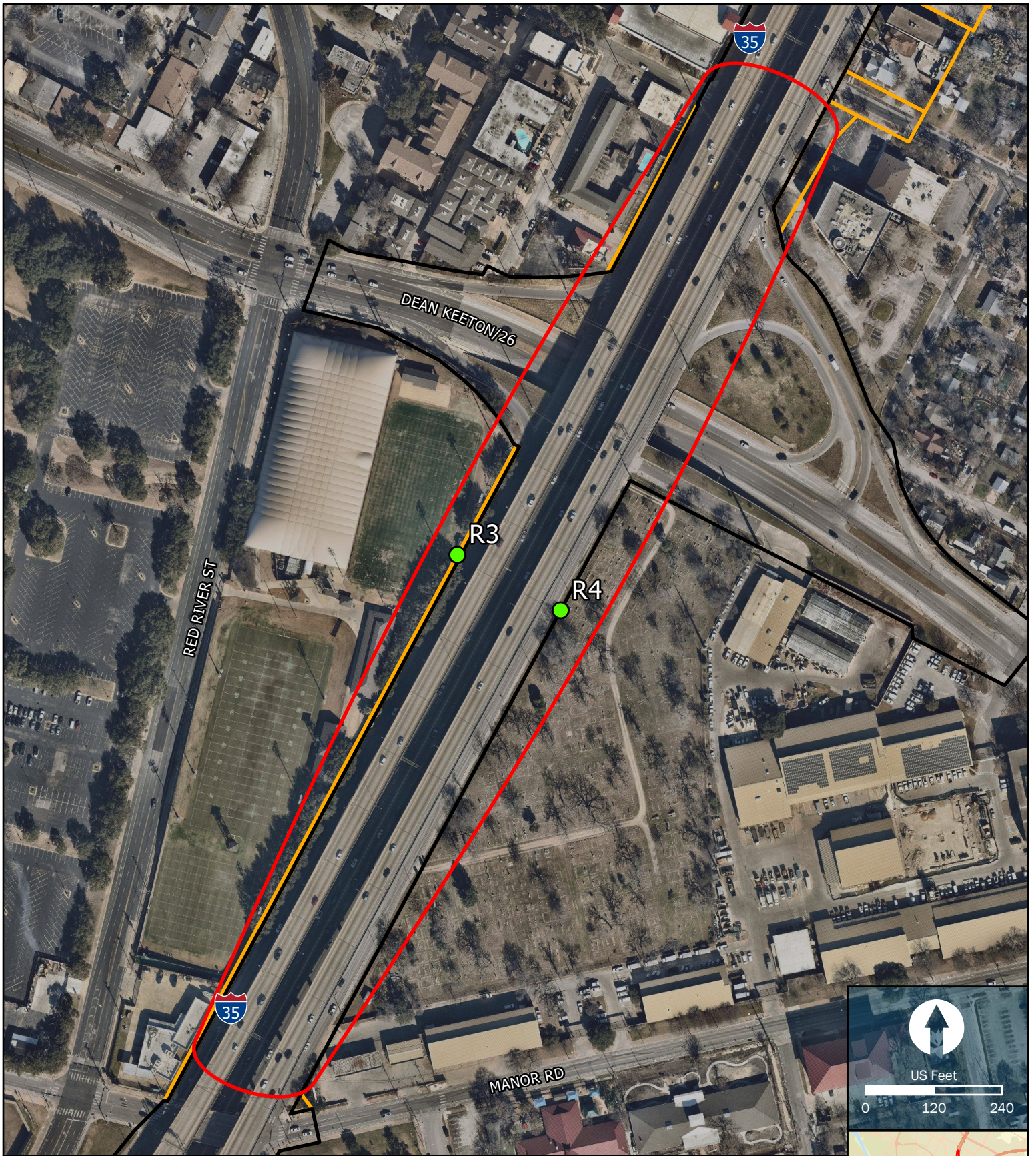
CO Receptors - Segment 1

I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: Nearmap 2022

-  Existing ROW
-  Proposed ROW
-  CO Modeling Area
-  Receptor Location



CO Receptors - Segment 2
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

- Existing ROW
- Proposed ROW
- CO Modeling Area
- Receptor Location





Sources: Nearmap 2022

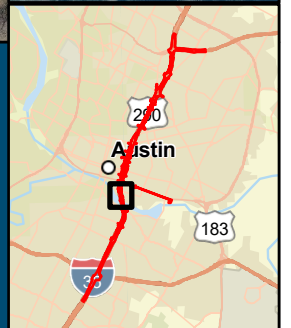
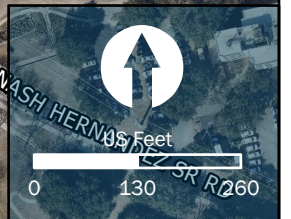


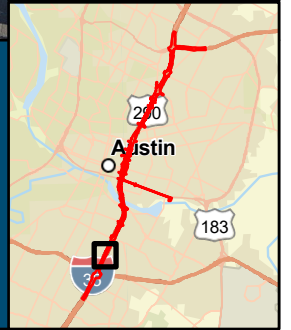
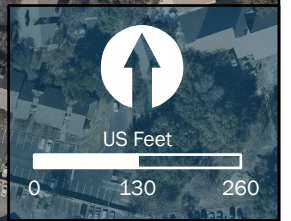
CO Receptors - Segment 3
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: Nearmap 2022





-  Existing ROW
-  Proposed ROW
-  CO Modeling Area
-  Receptor Location



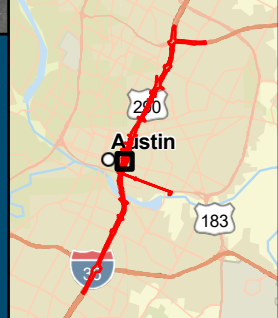
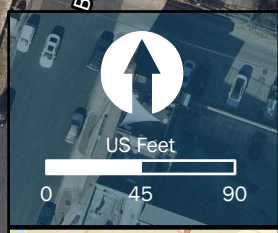
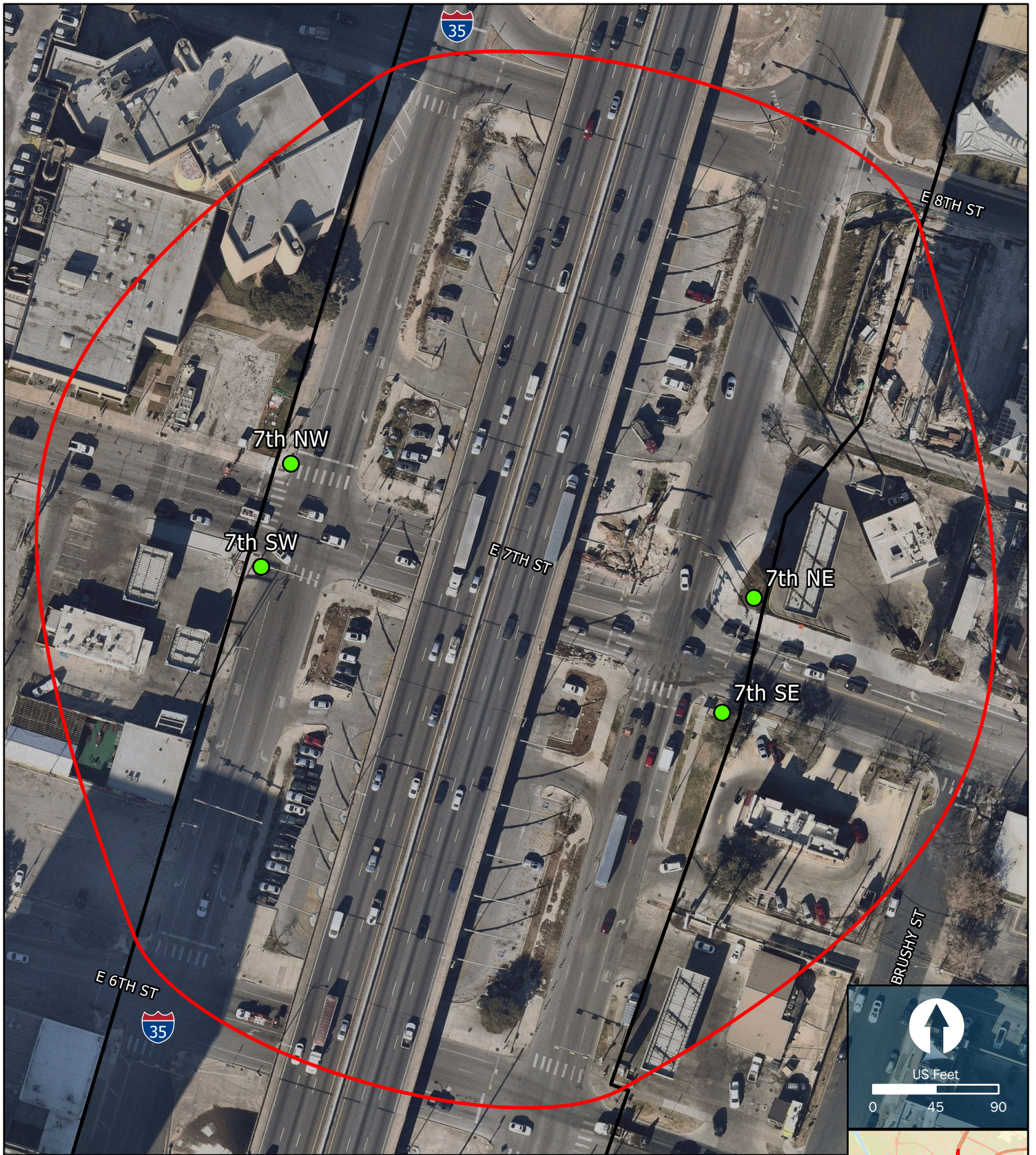


CO Receptors - Segment 4
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

-  Existing ROW
-  Proposed ROW
-  CO Modeling Area
-  Receptor Location





Sources: Nearmap 2022



CO Receptors - Segment 5
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: Nearmap 2022

-  Existing ROW
-  Proposed ROW
-  CO Modeling Area
-  Receptor Location







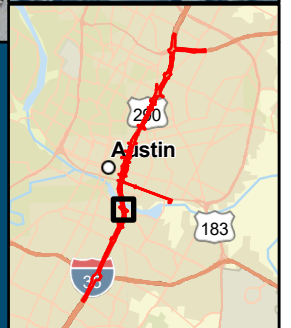
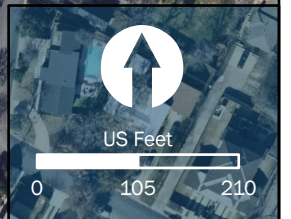
CO Receptors - Segment 6

I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: Nearmap 2022

-  Existing ROW
-  Proposed ROW
-  CO Modeling Area
-  Receptor Location



Quantitative MSAT Analysis Technical Report – Preferred Alternative



Quantitative Mobile Source Air Toxics Analysis

I-35 Capital Express Central Project

Travis County, Texas
Austin District
CSJ: 0015-13-388

August 2023

The environmental review, consultation, and other actions required by applicable Federal environmental laws for this project are being, or have been, carried out by TxDOT pursuant to 23 U.S.C. 327 and a Memorandum of Understanding dated December 9, 2019, and executed by FHWA and TxDOT.

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Appendices

Appendix A: Project Location Map

Appendix B: MSAT Conference Call Meeting Minutes

Appendix C: Traffic Data

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1.0 Background Information

The Texas Department of Transportation (TxDOT) Austin District is proposing improvements to Interstate Highway 35 (I-35) from US Highway 290 East (US 290E) to State Highway 71 (SH 71)/Ben White Boulevard (CSJ: 0015-13-388). See **Appendix A** for a Project Location Map.

Projects Subject to a Quantitative MSAT Analysis

Projects may be subject to a quantitative mobile source air toxics (MSAT) analysis if the project is adding capacity, the design year annual average daily traffic (AADT) is over 140,000 vehicles per day (vpd), there is public concern over air quality, or the project will affect an intermodal facility. Since the project would add capacity and the design year traffic volume is above 140,000 vpd, a quantitative MSAT is required to assess the level at which MSAT would increase or decrease as a result of this project.

The MSAT analysis methodology, including determining and approving the analysis years, the networks links to be included, and the sources for the traffic data used in the analysis, was coordinated via a conference call on April 30, 2021. The call participants consisted of representatives from TxDOT Environmental Affairs Division (ENV), TxDOT Austin District, and the consultant team. After the initial conference call, the estimated time of completion (ETC) for the project was changed from 2030 to 2032; therefore, it was determined via email correspondence that the interim scenario year should be adjusted to 2032. See **Appendix B** for a record of the meeting and subsequent coordination.

2.0 Qualitative MSAT Analysis

Background

Controlling air toxic emissions became a national priority with the passage of the Clean Air Act Amendments (CAAA) of 1990, whereby Congress mandated that the Environmental Protection Agency (EPA) regulate 188 air toxics, also known as hazardous air pollutants. The EPA has assessed this expansive list in their latest rule on the Control of Hazardous Air Pollutants from Mobile Sources (Federal Register, Vol. 72, No. 37, page 8430, February 26, 2007), and identified a group of 93 compounds emitted from mobile sources that are listed in their Integrated Risk Information System (IRIS)¹. In addition, EPA identified nine compounds with significant contributions from mobile sources that are among the national and regional-scale cancer risk drivers from their 2011 National Air Toxics

¹ <http://www.epa.gov/iris/>

Assessment (NATA)². These are 1,3-butadiene, acetaldehyde, acrolein, benzene, diesel particulate matter (DPM), ethylbenzene, formaldehyde, naphthalene, and polycyclic organic matter (POM). While the Federal Highway Administration (FHWA) considers these the priority MSAT, the list is subject to change and may be adjusted in consideration of future EPA rules.

Motor Vehicle Emissions Simulator (MOVES)

According to EPA, MOVES3 is a major revision to MOVES2014 and improves upon it in many respects. MOVES3 includes new data, new emissions standards, and new functional improvements and features. It incorporates substantial new data for emissions, fleet, and activity developed since the release of MOVES2014. These new emissions data are for light- and heavy-duty vehicles, exhaust and evaporative emissions, and fuel effects. MOVES3 also adds updated vehicle sales, population, age distribution, and vehicle miles travelled (VMT) data. In the November 2020 EPA issued MOVES3 Mobile Source Emissions Model Questions and Answers³ EPA states that for on-road emissions, MOVES3 updated heavy-duty (HD) diesel and compressed natural gas (CNG) emission running rates and updated HD gasoline emission rates. They updated light-duty (LD) emission rates for hydrocarbon (HC), carbon monoxide (CO) and nitrogen oxide (NOx) and updated light-duty (LD) particulate matter rates, incorporating new data on Gasoline Direct Injection (GDI) vehicles.

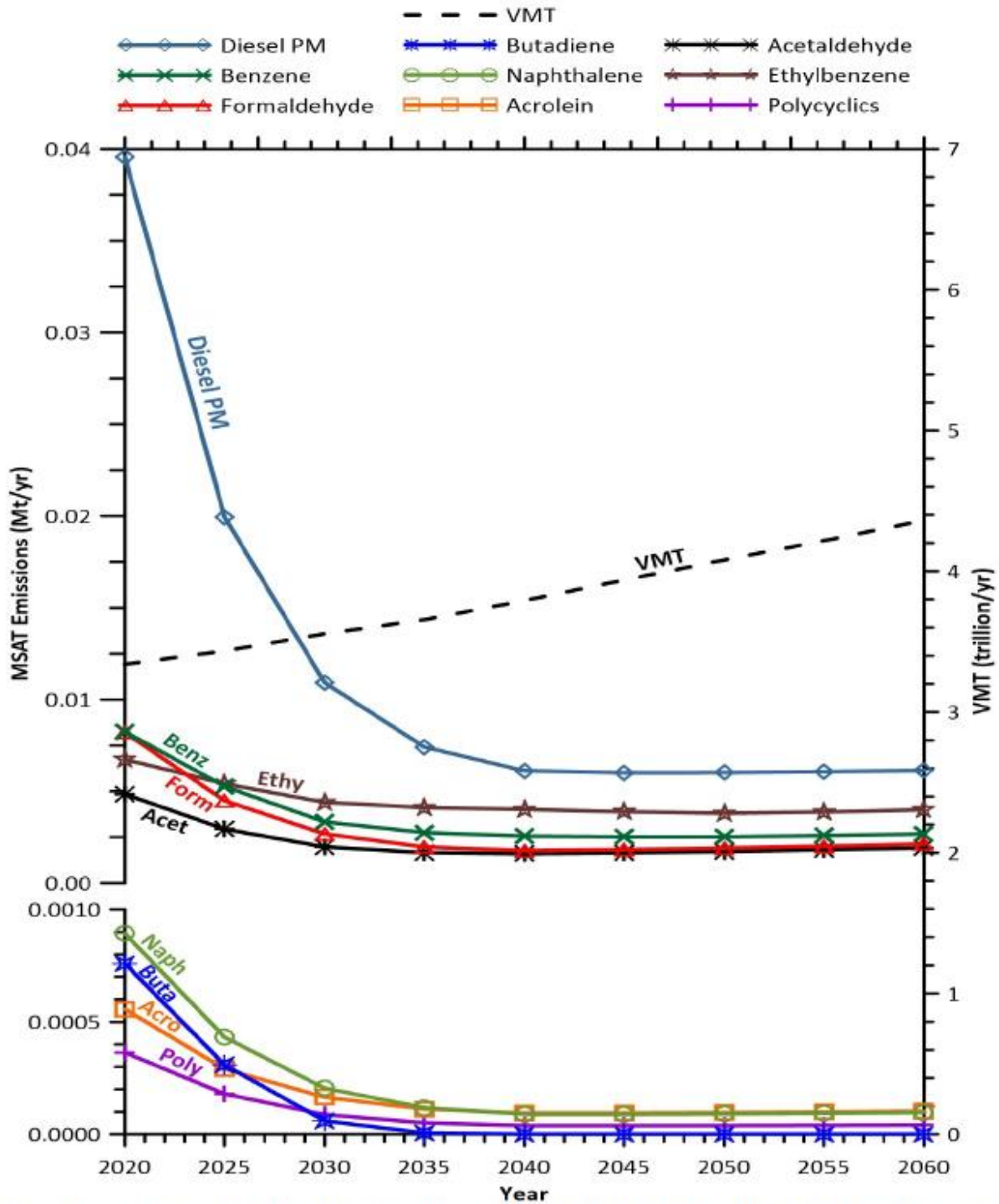
Using EPA's MOVES3 model, as shown in **Figure 1**, FHWA estimates that even if VMT increases by 31 percent from 2020 to 2060 as forecast, a combined reduction of 76 percent in the total annual emissions for the priority MSAT is projected for the same time period.

Diesel PM is the dominant component of MSAT emissions, making up 36 to 56 percent of all priority MSAT pollutants by mass, depending on calendar year. Users of MOVES3 will notice some differences in emissions compared with MOVES2014. MOVES3 is based on updated data on some emissions and pollutant processes compared to MOVES2014, and also reflects the latest Federal emissions standards in place at the time of its release. In addition, MOVES3 emissions forecasts are based on slightly higher VMT projections than MOVES2014, consistent with nationwide VMT trends.

²<https://www.epa.gov/national-air-toxics-assessment>

³ <https://nepis.epa.gov/Exe/ZyPDF.cgi?Dockkey=P1010M06.pdf>

Figure 1: Projected National MSAT Emissions Trends
 For Vehicles Operating on Roadways (2020–2060)



Note: Trends for specific locations may be different, depending on locally derived information representing vehicle-miles travelled, vehicle speeds, vehicle mix, fuels, emission control programs, meteorology, and other factors.
 Source: EPA MOVES3 model runs conducted by FHWA, March 2021.

MSAT Research

Air toxics analysis is a continuing area of research. While much work has been done to assess the overall health risk of air toxics, many questions remain unanswered. In particular, the tools and techniques for assessing project-specific health outcomes as a result of lifetime MSAT exposure remain limited. These limitations impede the ability to evaluate how potential public health risks posed by MSAT exposure should be factored into project-level decision-making within the context of NEPA.

Project-Specific MSAT Information

A qualitative analysis provides a basis for identifying and comparing the potential differences among MSAT emissions, if any, from the various alternatives. The qualitative assessment presented below is derived in part from a study conducted by FHWA entitled A Methodology for Evaluating Mobile Source Air Toxic Emissions Among Transportation Project Alternatives⁴.

For each alternative, the amount of MSAT emitted would be proportional to the vehicle miles traveled, or VMT, assuming that other variables such as fleet mix are the same for each alternative. The VMT estimated for the Build Alternative is slightly higher than that for the No Build Alternative, because the additional capacity increases the efficiency of the roadway and attracts rerouted trips from elsewhere in the transportation network. The emissions increase from the additional VMT is offset somewhat by lower MSAT emission rates due to increased speeds; according to the EPA's MOVES3 model, emissions of all of the priority MSAT decrease as speed increases. The additional travel lanes contemplated as part of the project alternatives will have the effect of moving some traffic closer to nearby homes, schools, and businesses; therefore, under each alternative there may be localized areas where ambient concentrations of MSAT could be higher under the Build Alternative than the No Build Alternative. The localized increases in MSAT concentrations would likely be most pronounced along the expanded roadway sections that would be built between Dean Keaton Street and Manor Road, and between 15th Street and Cesar Chavez Street. However, the magnitude and the duration of these potential increases compared to the No Build alternative cannot be reliably quantified due to incomplete or unavailable information in forecasting project-specific MSAT health impacts. Also, MSAT will be lower in other locations when traffic shifts away from them; therefore, on a regional basis, EPA's vehicle and fuel regulations, coupled with fleet turnover, will over time cause substantial reductions that, in almost all cases, will cause region- wide MSAT levels to be significantly lower than today.

⁴https://www.fhwa.dot.gov/environment/air_quality/air_toxics/research_and_analysis/mobile_source_air_toxics/msatemissions.cfm

Incomplete or Unavailable Information for Project-Specific MSAT Health Impacts Analysis

In FHWA's view, information is incomplete or unavailable to credibly predict the project-specific health impacts due to changes in MSAT emissions associated with a proposed set of highway alternatives. The outcome of such an assessment, adverse or not, would be influenced more by the uncertainty introduced into the process through assumption and speculation rather than any genuine insight into the actual health impacts directly attributable to MSAT exposure associated with a proposed action.

The EPA is responsible for protecting the public health and welfare from any known or anticipated effect of an air pollutant. They are the lead authority for administering the Clean Air Act and its amendments and have specific statutory obligations with respect to hazardous air pollutants and MSAT. The EPA is in the continual process of assessing human health effects, exposures, and risks posed by air pollutants. They maintain the Integrated Risk Information System (IRIS), which is "a compilation of electronic reports on specific substances found in the environment and their potential to cause human health effects"⁵. Each report contains assessments of non-cancerous and cancerous effects for individual compounds and quantitative estimates of risk levels from lifetime oral and inhalation exposures with uncertainty spanning perhaps an order of magnitude.

Other organizations are also active in the research and analyses of the human health effects of MSAT, including the Health Effects Institute (HEI). A number of HEI studies are summarized in Appendix D of FHWA's Updated Interim Guidance on Mobile Source Air Toxic Analysis in NEPA Documents⁶. Among the adverse health effects linked to MSAT compounds at high exposures are; cancer in humans in occupational settings; cancer in animals; and irritation to the respiratory tract, including the exacerbation of asthma. Less obvious is the adverse human health effects of MSAT compounds at current environmental concentrations⁷ or in the future as vehicle emissions substantially decrease.

The methodologies for forecasting health impacts include emissions modeling; dispersion modeling; exposure modeling; and then final determination of health impacts – each step in the process building on the model predictions obtained in the previous step. All are encumbered by technical shortcomings

⁵ EPA, <http://www.epa.gov/iris/>

⁶ http://www.fhwa.dot.gov/environment/air_quality/air_toxics/policy_and_guidance/msat/index.cfm

⁷ HEI Special Report 16, <https://www.healtheffects.org/publication/mobile-source-air-toxics-critical-review-literatureexposure-and-health-effects>

or uncertain science that prevents a more complete differentiation of the MSAT health impacts among a set of project alternatives. These difficulties are magnified for lifetime (i.e., 70 year) assessments, particularly because unsupportable assumptions would have to be made regarding changes in travel patterns and vehicle technology (which affects emissions rates) over that time frame, since such information is unavailable. It is particularly difficult to reliably forecast 70-year lifetime MSAT concentrations and exposure near roadways; to determine the portion of time that people are actually exposed at a specific location; and to establish the extent attributable to a proposed action, especially given that some of the information needed is unavailable.

There are considerable uncertainties associated with the existing estimates of toxicity of the various MSAT, because of factors such as low-dose extrapolation and translation of occupational exposure data to the general population, a concern expressed by HEI⁸. As a result, there is no national consensus on air dose-response values assumed to protect the public health and welfare for MSAT compounds, and in particular for diesel PM. The EPA states that with respect to diesel engine exhaust, “[t]he absence of adequate data to develop a sufficiently confident dose-response relationship from the epidemiologic studies has prevented the estimation of inhalation carcinogenic risk⁹.”

There is also the lack of a national consensus on an acceptable level of risk. The current context is the process used by the EPA as provided by the Clean Air Act to determine whether more stringent controls are required in order to provide an ample margin of safety to protect public health or to prevent an adverse environmental effect for industrial sources subject to the maximum achievable control technology standards, such as benzene emissions from refineries. The decision framework is a twostep process. The first step requires EPA to determine an “acceptable” level of risk due to emissions from a source, which is generally no greater than approximately 100 in a million. Additional factors are considered in the second step, the goal of which is to maximize the number of people with risks less than 1 in a million due to emissions from a source. The results of this statutory two-step process do not guarantee that cancer risks from exposure to air toxics are less than 1 in a million; in some cases, the residual risk determination could result in maximum individual cancer risks that are as high as approximately 100 in a million. In a June 2008 decision, the U.S. Court of Appeals for the District of Columbia Circuit upheld EPA’s approach to addressing risk in its two-step decision

⁸Special Report 16, <https://www.healtheffects.org/publication/mobile-source-air-toxics-critical-review-literatureexposure-and-health-effects>

⁹ EPA IRIS database, Diesel Engine Exhaust, Section II.C., https://iris.epa.gov/static/pdfs/0642_summary.pdf

framework. Information is incomplete or unavailable to establish that even the largest of highway projects would result in levels of risk greater than deemed acceptable¹⁰.

3.0 Analysis Methodology

The approach used in the analysis of MSATs along the project area considers the on-road sources for the nine priority MSATs in five different scenarios: Existing Conditions/Base (2023), Interim No Build (2032) and Build (2050), and Design No Build (2032) and Build (2050).

A project links method was used for the analysis. The managed lanes, general purpose lanes, collector-distributors, frontage roads, and ramps within the project were represented as links in the analysis, with a distinct traffic volume, length, and speed for each scenario. Each project link's length was multiplied by the corresponding DHV to obtain a VMT for link. The VMT for each link was then multiplied by an emission rate for each of the nine priority MSATs for a total in each scenario.

Variable emission rates were used in the analysis based on a combination of non-peak free-flow speeds, ranging from 35 to 60 mph, and worst-case peak period speeds, ranging from 3 to 67 mph. The rates were derived from the TxDOT Running Emission Rates Lookup Table (ERLT) for MSAT (*TxDOT Air Quality Toolkit, January 2023*) for the Austin region, which are based on the MOVES3 emission model for each of the priority MSATs for the corresponding analysis years and associated roadway link parameters.

4.0 Analysis Results

The resulting emission inventory for the nine priority MSATs for the project link network is summarized in **Table 1** and **Figures 2** and **3**. The analysis indicates that a decrease in MSAT emissions can be expected for both the Build and No Build Alternatives in 2050, compared to the existing year of 2023. Under the Build Alternative, emissions of total MSAT are predicted to decrease by 51% from 2023 to 2050, even though VMT is expected to rise by 40%. Compared to the No-Build 2032 and 2050 scenarios, the Build Alternative emissions of total MSAT are predicted to increase by 12 and 9 percent, respectively, with VMT increasing by 1 percent and 0.4 percent, respectively.

¹⁰ [https://www.cadc.uscourts.gov/internet/opinions.nsf/284E23FFE079CD59852578000050C9DA/\\$file/07-1053-1120274.pdf](https://www.cadc.uscourts.gov/internet/opinions.nsf/284E23FFE079CD59852578000050C9DA/$file/07-1053-1120274.pdf)

All nine MSAT compounds are expected to decrease from the base scenario in both the Build and No-Build scenarios. Of the nine priority MSAT compounds, DPM contributes the most to the emissions total for all scenarios, followed by benzene. In future years, the difference in No-Build and Build DPM emissions is predicted to decrease, with a calculated 9 percent difference in 2032 and 8 percent difference in 2050.

Table 1: MSAT Emission Inventory by Scenario (2023, 2032, and 2050)

| Compound | Year/Scenario | | | | | Percent Change by Year/Scenario | | | |
|------------------------|---------------|--------------|-------------|---------------|---------------|---------------------------------|------------------------------|--------------------------|-------------------------|
| | 2023 Base | 2032 Interim | | 2050 Design | | Base No-Build / Interim Build | Base No-Build / Design Build | Interim No-Build / Build | Design No-Build / Build |
| | No-Build | No-Build | Build | No-Build | Build | | | | |
| Benzene | 0.93502 | 0.45697 | 0.51596 | 0.53534 | 0.57625 | -45% | -38% | 13% | 8% |
| Napthalene | 0.09444 | 0.02341 | 0.02637 | 0.02087 | 0.02238 | -72% | -76% | 13% | 7% |
| Butadiene | 0.05403 | 0.00143 | 0.00167 | 0.00 | 0.00 | -97% | -100% | 17% | 0% |
| Formaldehyde | 0.92953 | 0.28794 | 0.33079 | 0.30708 | 0.33586 | -64% | -64% | 15% | 9% |
| Acetaldehyde | 0.59211 | 0.25521 | 0.29817 | 0.33205 | 0.36785 | -50% | -38% | 17% | 11% |
| Acrolein | 0.07110 | 0.02508 | 0.02923 | 0.02985 | 0.03302 | -59% | -54% | 17% | 11% |
| Ethylbenzene | 0.63281 | 0.36160 | 0.43176 | 0.50162 | 0.55487 | -32% | -12% | 19% | 11% |
| DPM | 5.05475 | 1.99634 | 2.17010 | 2.04080 | 2.19794 | -57% | -57% | 9% | 8% |
| POM | 0.03990 | 0.01002 | 0.01119 | 0.00877 | 0.00935 | -72% | -77% | 12% | 7% |
| Total MSAT (Tons/Year) | 8.40367 | 3.41800 | 3.81524 | 3.77638 | 4.09752 | -55% | -51% | 12% | 9% |
| Total VMT (Miles/Year) | 780,848,847 | 884,570,721 | 894,016,004 | 1,089,574,405 | 1,093,990,268 | 14% | 40% | 1% | 0.4% |

Figure 2: Projected MSAT Emissions vs. VMT by Scenario

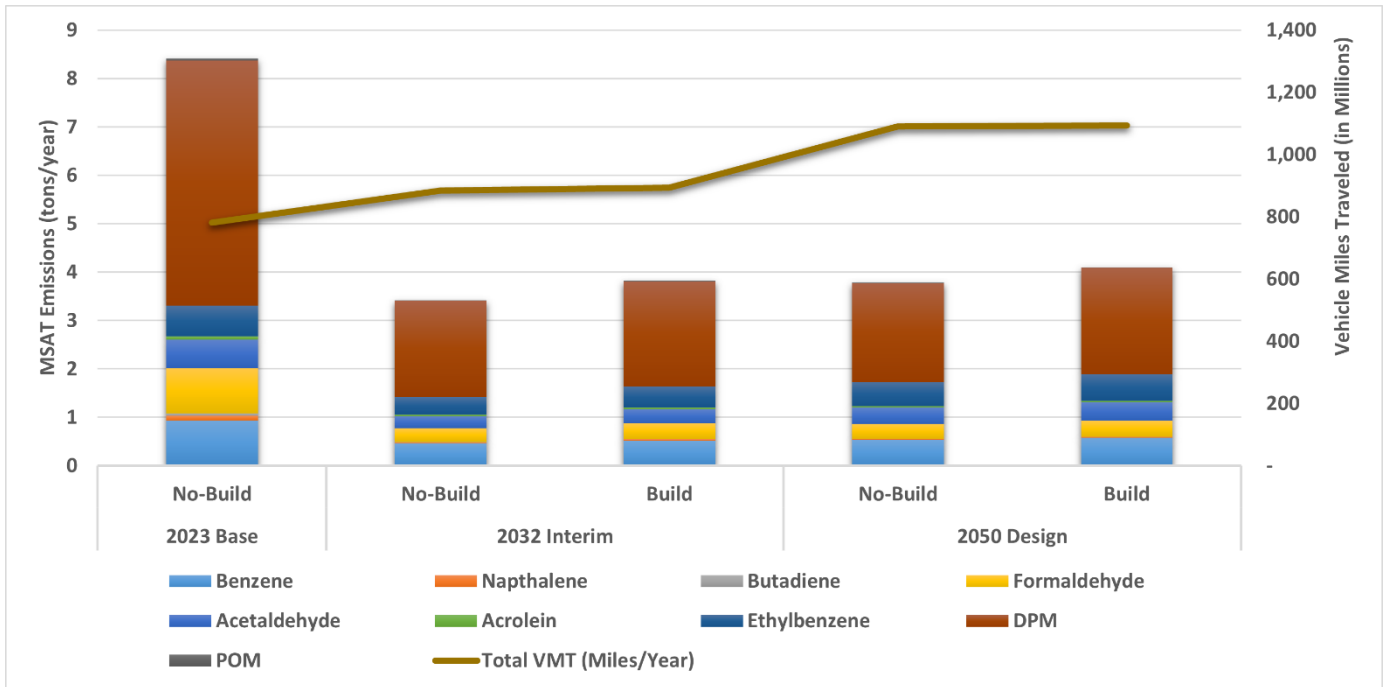
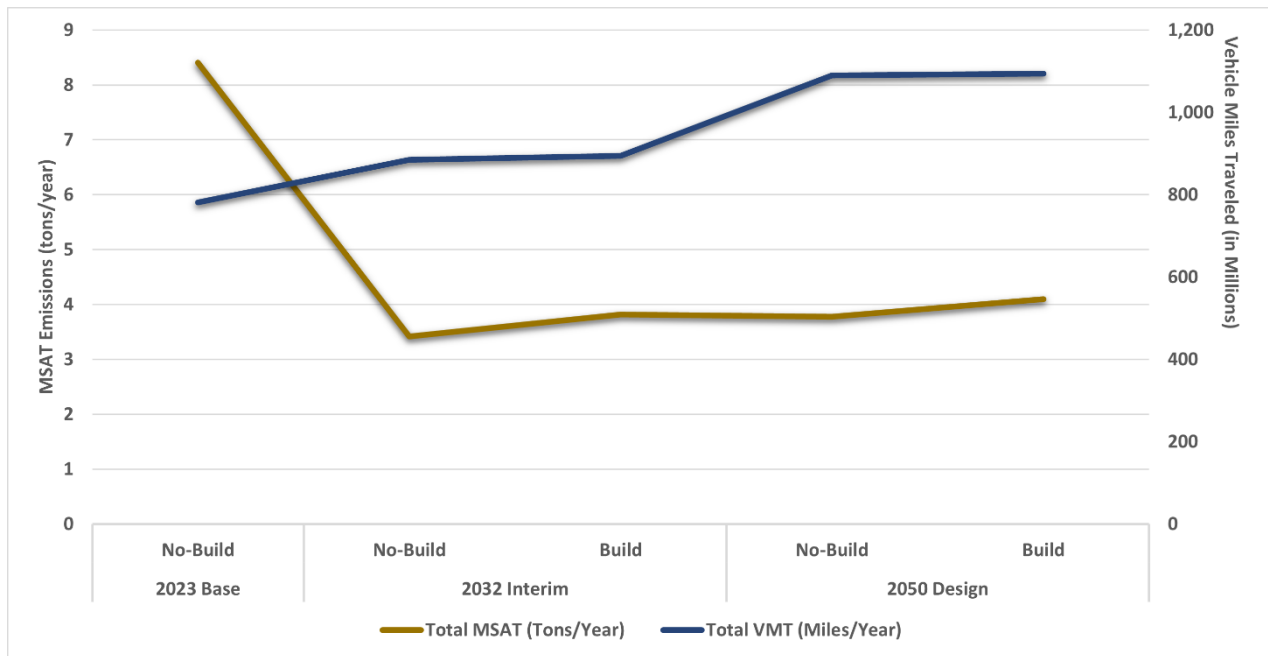


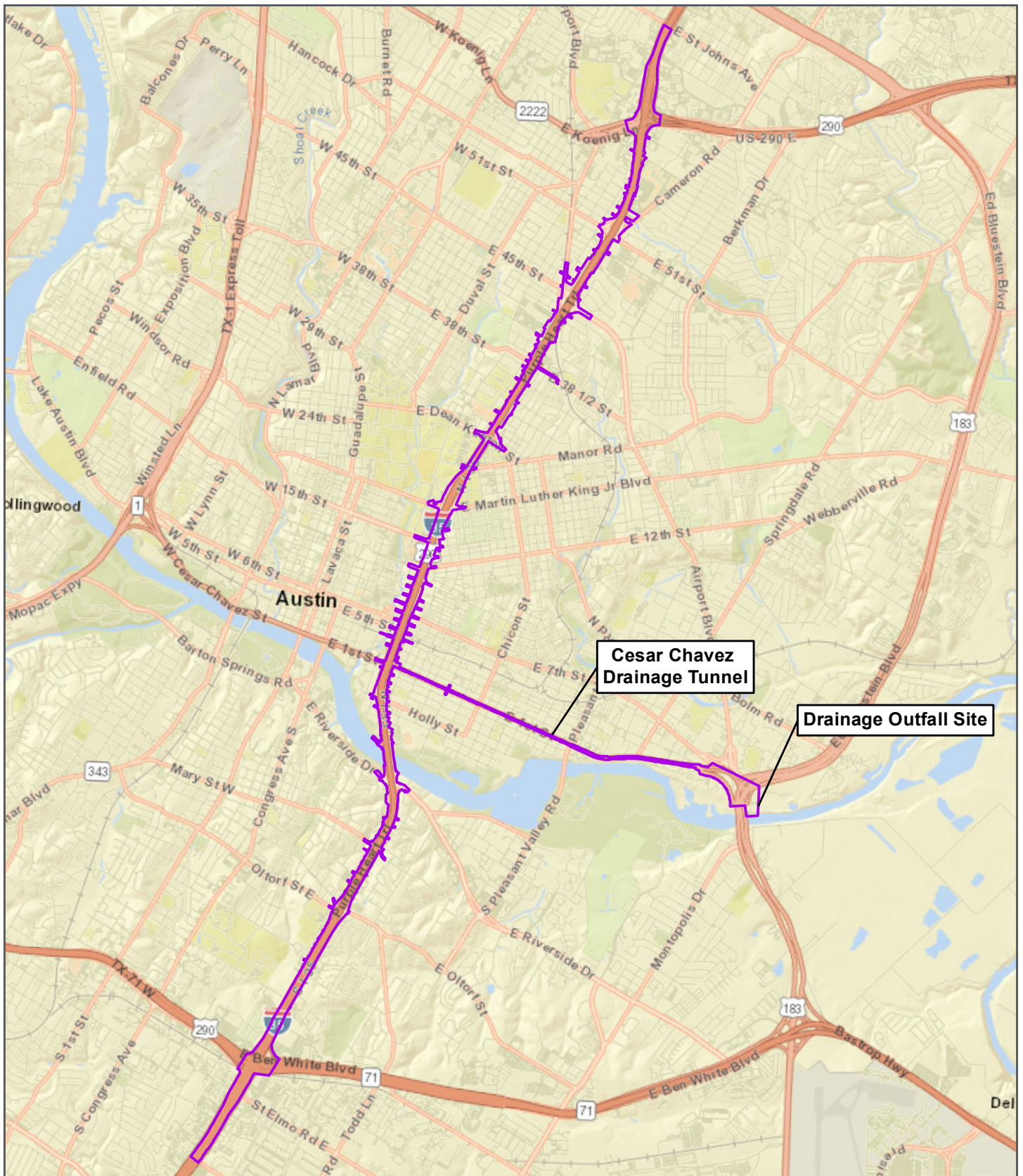
Figure 3: Comparison of Total MSAT Emissions vs. VMT by Scenario



5.0 Conclusion

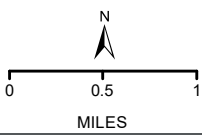
In sum, both the Build and No Build Alternative in the design year are expected to be associated with lower levels of MSAT emissions compared to the base year. There is a minor increase in MSAT emissions expected between the No Build and Build Alternatives for the design year. Under all alternatives, MSAT levels are likely to decrease over time due to nationally mandated cleaner vehicles and fuels.

APPENDIX A
Project Location Map

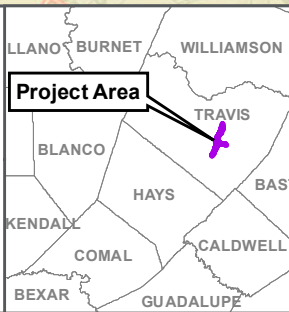


**Cesar Chavez
Drainage Tunnel**

Drainage Outfall Site



Legend
 MODIFIED
 ALTERNATIVE 3 -
 PREFERRED
 ALTERNATIVE



PROJECT LOCATION MAP

I-35 CAPITAL EXPRESS
 CENTRAL PROJECT
 TRAVIS COUNTY, TX

APRIL 2023

FIGURE 1



APPENDIX B
MSAT Conference Call Meeting Minutes

Quantitative MSAT and CO TAQA Discussion

CapEx Central from US 290E to SH 71

0015-13-388

Date: April 30, 2021

Facilitator: Shane Valentine, P.G.

Time: 10:00 am

Location: Microsoft Teams

Purpose: Quantitative MSAT and CO TAQA Discussion

Agenda:

1. Introductions

2. Overview

a. Project Description

- i. Capital Express Central (I-35 from US 290E to SH 71/US 290W)
- ii. Project Description – highlight tunnels

b. Reason for Call

- i. To discuss the years of analysis and methodology required for MSAT and CO TAQA. The project is added capacity and has AADT > 140,000.

1. Project will require MSAT and CO analysis.

- a. MSAT – Tunnels don't matter. Will be measuring total emissions not doing dispersion modeling.
- b. CO – may need to analyze worst case scenario and measure areas at tunnel exits on either end. Likely use CAL3QHC model and load all traffic onto tunnel exits.
 - i. CPY provided example from Seattle using AERMOD. May use receptors at window locations or air intake ducts at some sensitive receptors. TW – receptors should be at ROW line for even greater sensitivity.
 - ii. Model could incorporate ventilation fans.
 - iii. For analysis we need to assume where ventilation shafts could be installed.

c. Anticipated Environmental Approval

- i. Anticipated environmental clearance date: **Summer 2023**
- ii. Base year: **2021**
- iii. The estimated time to completion (ETC) year: **2030**
 1. (ETC refers to the conclusion of construction and the opening year of the project.)
 2. Design/Horizon Year: **2050**

- a. Design year of 2050 chosen based on the traffic study
- d. Timing / Alternatives / Technical Reports
 - i. All build alternatives vs. only preferred alternative
 - 1. We will model all 3 build alternatives for both the ETC and Design Year for the CO analysis
 - a. Tim Wood also recommending modeling a No-Build for both the ETC and Design Year
 - 2. We will only model the preferred alternative for the quantitative MSAT
 - ii. Approach - EIS Chapter vs. technical reports-
 - 1. TW sees no issues but would recommend that the technical analysis be appended rather than put in the EIS document.
 - 2. Toolkit templates would be appended. Narrative results and summation data table would be provided in EIS.
 - a. Further discussions
- e. Traffic Data
 - i. Discuss traffic data available/in development
 - 1. Matt Best discussed the microsimulation study that is being conducted for the years of 2030 and 2050
 - 2. The methodology is being approved by TPP, but not the actual numbers – so traffic data developed using this methodology for any scenario will be acceptable to use once approved by TPP
 - ii. Specific traffic data needs for air quality analysis:
 - 1. No-Build/Existing conditions line diagram with ADT for specified base year
 - a. Instead of the corridor-wide 2018 line diagram that was used for the noise analysis and for CapEx North and South, the updated microsimulation study for the base/existing year for 2019 will be used and the numbers grown to 2021. This is to be used instead because of the availability of congested/peak period speeds.
 - b. Need 2050 numbers for no-build design year.
 - 2. Build conditions line diagram with ADT for specified ETC and design year
 - a. Data Needed:
 - i. Line Diagrams for the 3 Build Alternatives for the years 2030 and 2050
 - ii. Congested/peak period speeds for the 3 Build Alternatives for the years 2030 and 2050

1. A table detailing the average speed between major intersections is sufficient
 - b. MSAT largely the same for all build alts.
 - i. No-build qualitative MSAT and quantitative CO
 - ii. For DEIS Build alts we will provide qualitative MSAT and quantitative CO analysis.
 1. Provide Quantitative MSAT for **preferred** alternative in DEIS.
 - c. CO analysis needs to evaluate all build alts.
 - d. TPP will approve methodology for 2030 (CO) and 2050 (MSAT & CO).
3. Peak period/congested speeds
- a. Will be provided by Traffic team.
 - i. Mainlanes, managed lanes, and frontage roads.

3. MSAT Analysis

- a. Analysis Years
 - i. Base year: 2021 – (traffic data for 2019 will be grown to 2021)
 - ii. Design/horizon year: 2050
 - iii. Interim year (if applicable): 2030
- b. Methodology
 - i. Project Links analysis – only the linework for the project will be included in the analysis
 - ii. Speed data – discuss availability of congested speed data in AM/PM for use in the analysis
 1. Availability of this data for all roadways in the project (mainlanes, frontage roads, etc.)
- c. Emission Rates
 - i. Utilize the MSAT ERLT in the TxDOT Air Quality Toolkit
 1. New emission rate tables to be provided with data out to 2050.

4. CO TAQA

- a. Analysis Years
 - i. ETC year: 2030
 - ii. The design/horizon year: 2050
- b. Methodology
 - i. Use CAL3QHC model for analysis
 1. For tunnel segments, will load traffic data at entrance and exit points and place a receptor
 - a. Will also place a receptor at ventilation points

- ii. Will consider doing additional intersection analysis if there are determined to be any intersections with a LOS of DEF as a result of the project segments to model
 - 1. Will model all 3 Build Alternatives
 - a. Specific segments will be determined based on ROW width and high ADT, as well as traffic sections and location of tunnel entrances, exits, and ventilation points
 - 2. Will also model No-Build Alternatives for 2030
 - c. Emission Rates
 - i. Utilize the updated CO ERLT in the TxDOT Air Quality Toolkit
 - d. Special Considerations
 - i. Deck Plaza – currently trying to stay below ventilation threshold -
 - ii. Tunnels
- 5. **Schedule –**
 - a. When will traffic data be available:
 - i. ADTs – within next week.
 - ii. Existing speeds will require re-run of models – possibly deliver next week.
 - iii. Congested speeds for no-build and build – trying for end of May.
 - iv. TPP approved volumes for all alternatives build and no-build – Likely beyond May.
- 6. **Data Needs for AQ Team:**
 - a. Design DGNs for all 3 Build Alternatives
 - i. Existing and proposed ROW
 - ii. Lane striping and pavement
 - iii. Tunnel configuration – including ventilation, once available
 - b. Traffic Data:
 - i. Line Diagrams with ADT for all 3 Build Alternatives – for the years of 2030 and 2050
 - ii. Line Diagrams with ADT for existing, no-build facility for the year of 2019 (we will grow the numbers to 2021)
 - iii. Line Diagrams with ADT for No-Build facility for the years or 2030 and 2050
 - iv. Congested/peak period speeds for the 3 Build Alternatives for the years 2030 and 2050
 - 1. Needed for the full facility (MLs, FRs, DCs, CDs)
 - 2. A table detailing the average speed between major intersections is sufficient
 - v. Intersection analysis showing the LOS for each intersection of the project
 - 1. Need to ID any intersections with a LOS of DEF because of the project

Action Item Summary (Previous Meeting)

| Item: | Responsibility: |
|--|------------------------|
| CPY to send Tim Wood the Seattle AQ analysis study. | Angela Gillmeister |
| Updated ERLTs with data out to 2050 provided to HDR team | Tim Wood |
| | |
| | |
| | |
| | |
| | |

APPENDIX C
Traffic Data

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | | | |
|---|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|---------|---------|---------|-----|-----|-----|--------|----|-------------|---|-------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Mainlanes)</u></p> <p align="center"><u>Section 2</u></p> <p>From William Cannon Dr. To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 245,200 | 305,900 | 51 - 49 | 6.0 | 8.8 | 4.0 | 13,700 | 20 | 86,456,000 | 3 | 121,376,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | | | | |
| Light Duty | 91.2 | | 96.0 | | | | | | | | | | | | | | | | | | | | | |
| Medium Duty | 2.3 | | 1.0 | | | | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 6.5 | | 3.0 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Mainlanes)</u></p> <p align="center"><u>Section 2</u></p> <p>From William Cannon Dr. To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 245,200 | 326,200 | 51 - 49 | 6.0 | 8.8 | 4.0 | 13,700 | 20 | 134,461,000 | 3 | 188,770,500 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | | |
| Light Duty | 90.4 | 95.7 | | | | | | | | | | | |
| Medium Duty | 2.6 | 1.2 | | | | | | | | | | | |
| Heavy Duty | 7.0 | 3.1 | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| I-35 (No Build Mainlanes) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From US 183 To SH 45 N Travis County | 209,150 | 274,500 | 53 - 47 | 6.8 | 9.6 | 4.3 | 13,600 | 20 | 81,221,500 | 3 | 114,057,000 | 8" | |
| I-35 (No Build Mainlanes) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From US 183 To SH 45 N Travis County | 209,150 | 290,750 | 53 - 47 | 6.8 | 9.6 | 4.3 | 13,600 | 20 | 125,926,000 | 3 | 176,834,000 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| <u>I-35 (No Build Frontage Roads)</u> <u>Section 1</u> From SH 45 South To Slaughter Creek Travis County | 9,300 | 12,150 | 52 - 48 | 7.0 | 4.3 | 3.2 | 10,800 | 40 | 1,151,000 | 3 | 1,419,500 | 8" | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | |
| Light Duty | 95.7 | | 96.8 | | | | | | | | | | |
| Medium Duty | 2.6 | | 2.0 | | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.2 | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| <u>I-35 (No Build Frontage Roads)</u> <u>Section 1</u> From SH 45 South To Slaughter Creek Travis County | 9,300 | 12,850 | 52 - 48 | 7.0 | 4.3 | 3.2 | 10,800 | 40 | 1,783,500 | 3 | 2,199,000 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | |
|---|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|-----------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Slaughter Creek To Slaughter Lane</p> <p>Travis County</p> | | | | | | | | | | | | | 6,116,000 | 3 | 7,534,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | | | | | |
| Light Duty | 96.1 | 97.1 | | | | | | | | | | | | | | |
| Medium Duty | 2.3 | 1.7 | | | | | | | | | | | | | | |
| Heavy Duty | 1.6 | 1.2 | | | | | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Slaughter Creek To Slaughter Lane</p> <p>Travis County</p> | | | | | | | | | | | | | 9,496,000 | 3 | 11,699,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | |
| Light Duty | 96.8 | | 97.6 | | | | | | | | | | |
| Medium Duty | 1.9 | | 1.4 | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From Slaughter Lane To William Cannon Dr. | 79,000 | 103,550 | 52 - 48 | 7.0 | 3.2 | 2.4 | 12,000 | 30 | 7,345,500 | 3 | 9,028,500 | 8" | |
| Travis County | | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | | |
| Section 3 | | | | | | | | | | | | | |
| From Slaughter Lane To William Cannon Dr. | 79,000 | 109,650 | 52 - 48 | 7.0 | 3.2 | 2.4 | 12,000 | 30 | 11,386,500 | 3 | 13,995,000 | 8" | |
| Travis County | | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | |
| Light Duty | 96.6 | | 97.4 | | | | | | | | | | |
| Medium Duty | 2.0 | | 1.5 | | | | | | | | | | |
| Heavy Duty | 1.4 | | 1.1 | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| <u>I-35 (No Build Frontage Roads)</u> | | | | | | | | | | | | | |
| <u>Section 4</u> | | | | | | | | | | | | | |
| From William Cannon Dr. To Lady Bird Lake | 71,050 | 89,450 | 52 - 48 | 7.0 | 3.4 | 2.6 | 12,000 | 30 | 6,850,500 | 3 | 8,426,500 | 8" | |
| Travis County | | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 5 | | | | | | | | | | | | |
| From Lady Bird Lake To 38 1/2th Street Travis County | 48,400 | 60,200 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 5,564,000 | 3 | 6,858,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| | Light Duty | 95.9 | 96.9 | | | | | | | | | |
| Medium Duty | 2.4 | | 1.8 | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.3 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | | | | | | | | | | | | |
| I-35 (No Build Frontage Roads) | | | | | | | | | | | | |
| Section 5 | | | | | | | | | | | | |
| From Lady Bird Lake To 38 1/2th Street Travis County | 48,400 | 64,350 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 8,665,000 | 3 | 10,681,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | |
|---|--------------------------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|---------|----------------|----------|----------------|-----|--------|--------------------------------|-------------------|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | |
| | Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.8 | | 97.6 | | | | | | | | | | | | | | | | | |
| Medium Duty | 1.9 | | 1.4 | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | |
| <u>I-35 (No Build Frontage Roads)</u> <u>Section 6</u> From 38 1/2th Street To 51st Street Travis County | | | | | | | | | 84,400 | 105,100 | 51 - 49 | 6.0 | 3.2 | 2.4 | 12,000 | 30 | 7,625,000 | 3 | 9,372,000 | 8" |
| Description of Location | | | | | | | | | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | | | | | | | | | 2030 | 2060 | | | ADT | DHV | | | | | | |
| <u>I-35 (No Build Frontage Roads)</u> <u>Section 6</u> From 38 1/2th Street To 51st Street Travis County | | | | | | | | | 84,400 | 112,000 | 51 - 49 | 6.0 | 3.2 | 2.4 | 12,100 | 30 | 11,854,500 | 3 | 14,570,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | |
|---|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|-----------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 7</u></p> <p>From 51st Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | | 6,150,500 | 3 | 7,572,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | |
| | Light Duty | | 96.3 | | 97.2 | | | | | | | | | | | |
| | Medium Duty | | 2.2 | | 1.7 | | | | | | | | | | | |
| | Heavy Duty | | 1.5 | | 1.1 | | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 7</u></p> <p>From 51st Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | | 9,562,500 | 3 | 11,774,000 | 8" |

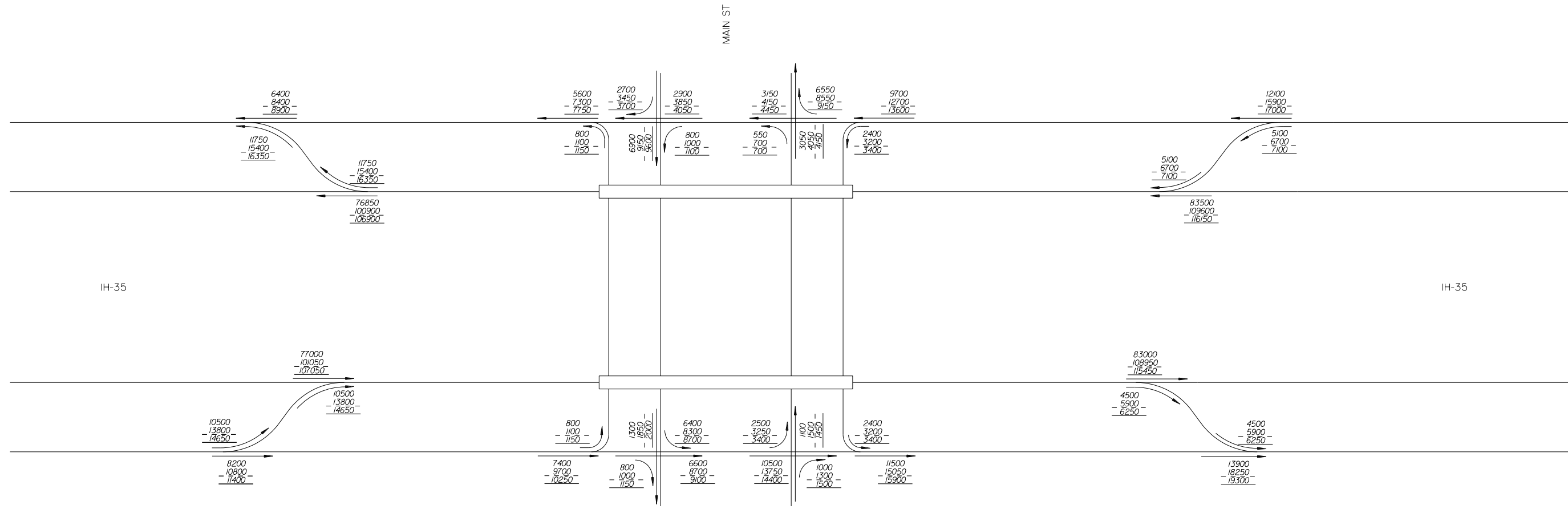
TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

February 22, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | | | |
|--|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--------|---------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 8</u></p> <p>From US 290 To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 74,450 | 95,450 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 7,044,000 | 3 | 8,661,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.7 | | 97.5 | | | | | | | | | | | | | | | | | | | | | |
| Medium Duty | 2.0 | | 1.5 | | | | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (No Build Frontage Roads)</u></p> <p align="center"><u>Section 8</u></p> <p>From US 290 To US 183</p> <p>Travis County</p> | | | | | | | | | | | | | 74,450 | 101,750 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 10,958,000 | 3 | 13,473,500 | 8" |

NO-BUILD CONFIGURATION



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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

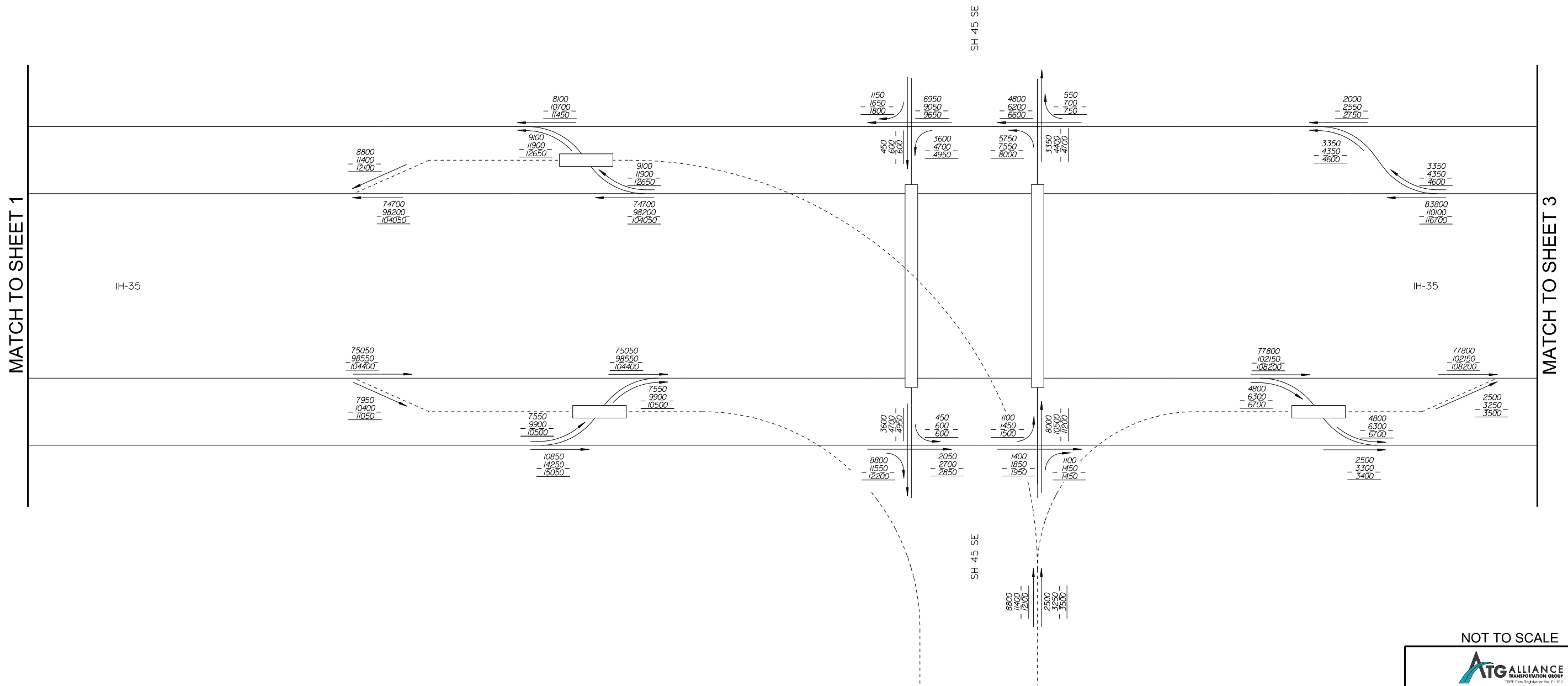


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 1 OF 28)

| | | | | |
|------------------|----------------|-------------------|-------------|-----------|
| SCALE : N. T. S. | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | HAYS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 1 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 2 OF 28)

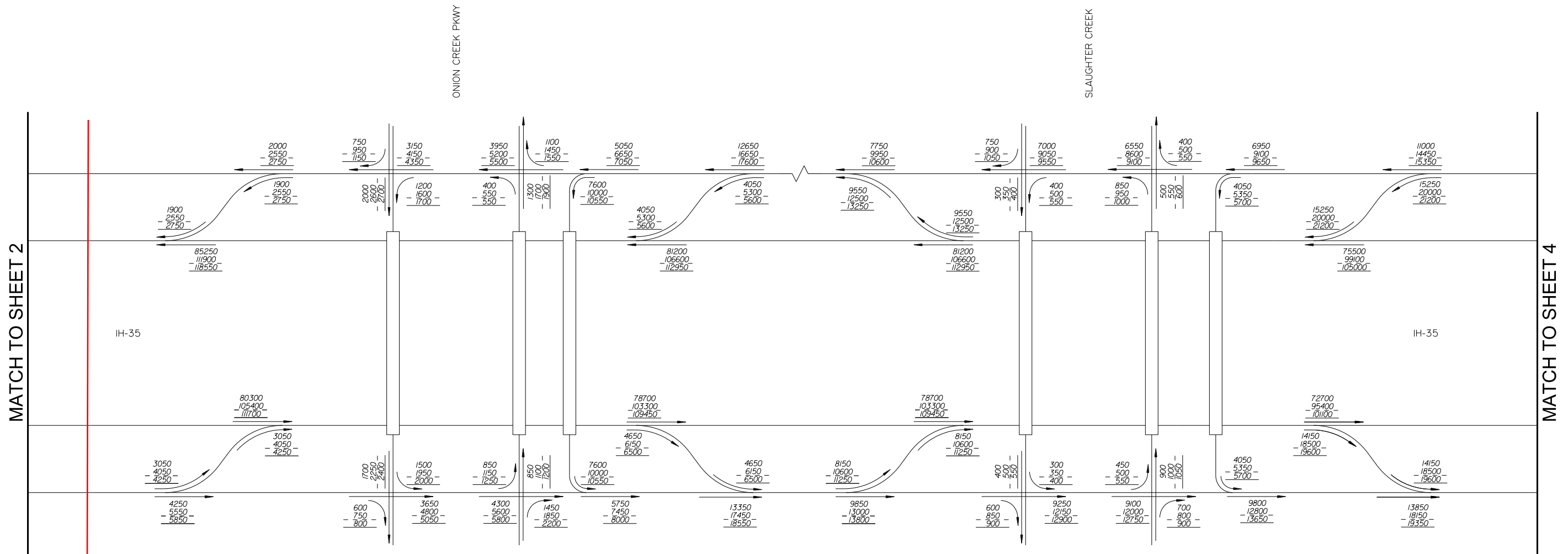
| | | | |
|------------------|----------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 2 |

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NO-BUILD CONFIGURATION



MATCH TO SHEET 2

MATCH TO SHEET 4

IH-35

IH-35

Frontage Road
Section 1

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

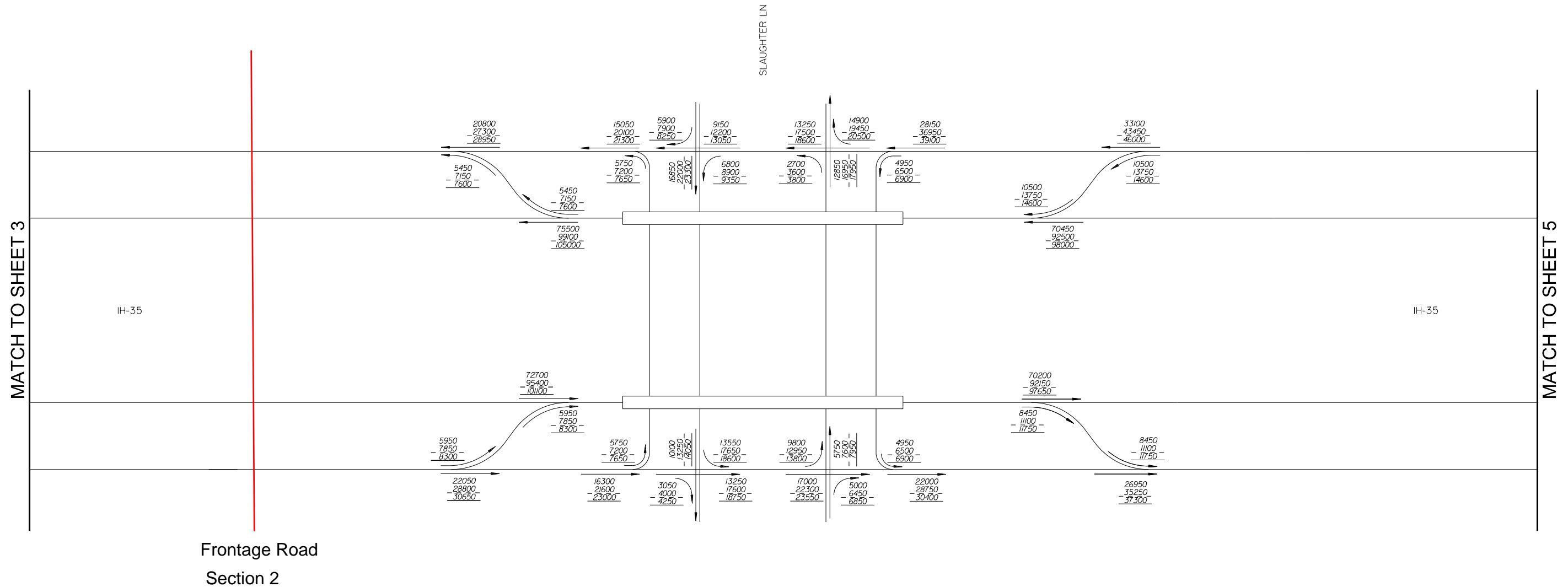


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 3 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 3 |



NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 4 OF 28)

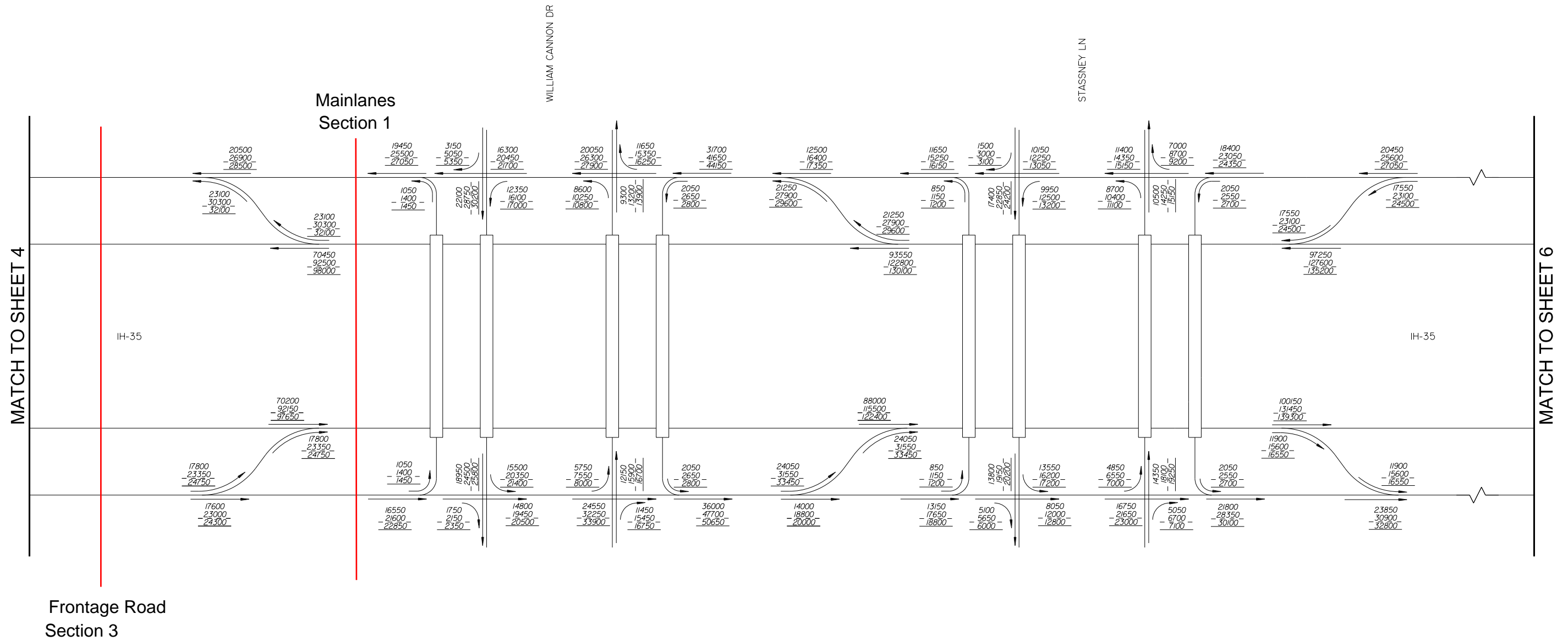
| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 4 |

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NO-BUILD CONFIGURATION



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THouston

11:12:01 AM



1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

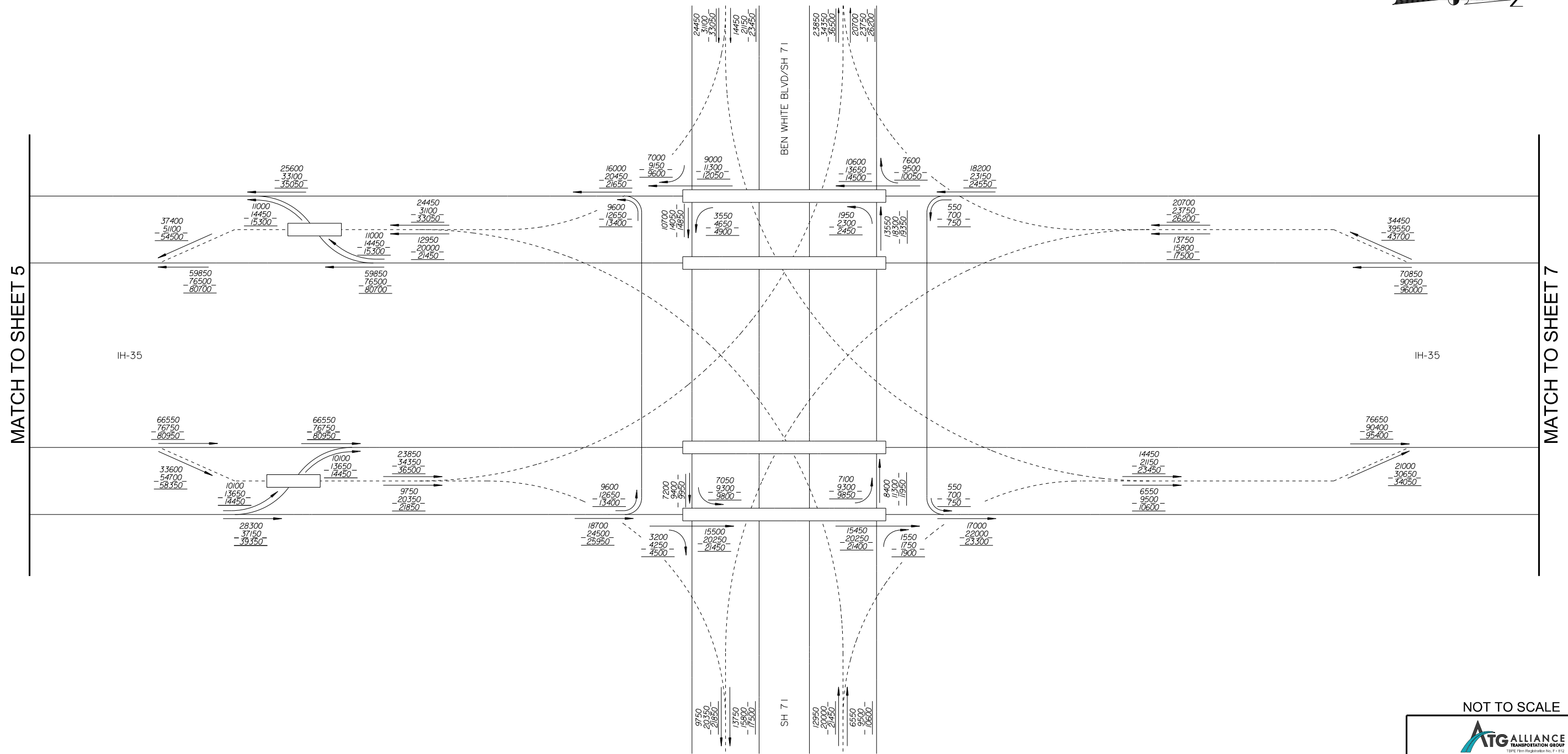
LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|---|----------|-------------------|----------|-----------|
|  <small>TRANSPORTATION GROUP</small> <small>TP&E Firm Registration No. F-112</small> | | | | |
|  Texas Department of Transportation | | | | |
| CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 5 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |

NO-BUILD CONFIGURATION




MATCH TO SHEET 5

MATCH TO SHEET 7


2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



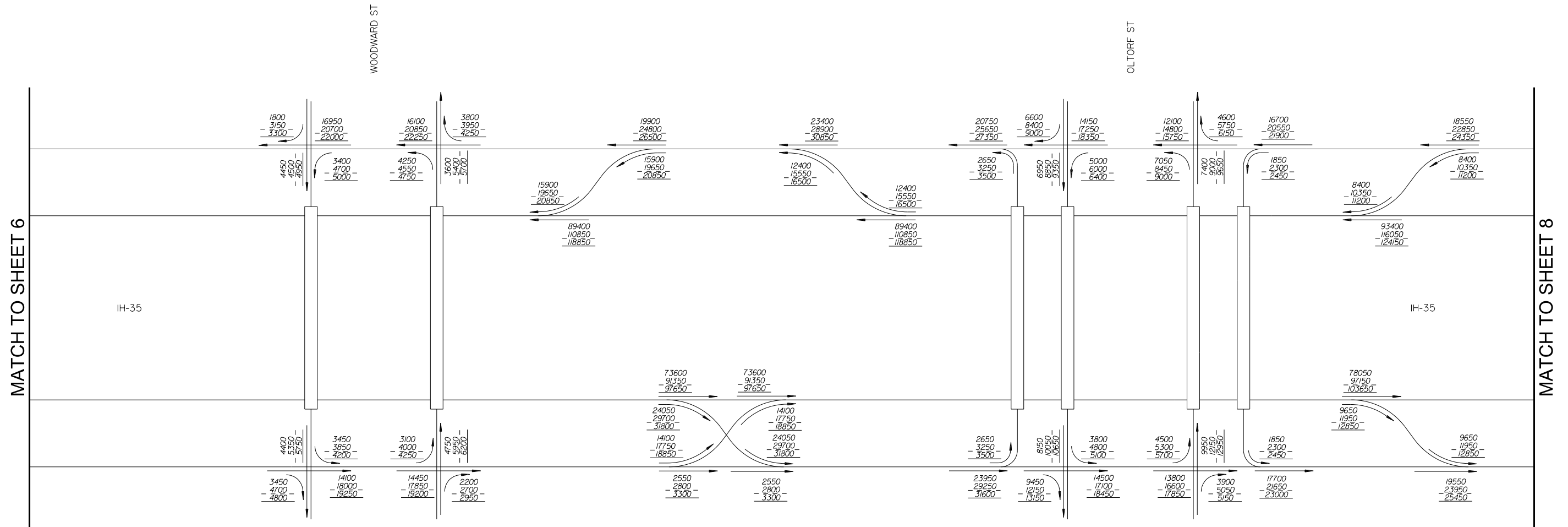
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 6 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 6 |

NO-BUILD CONFIGURATION



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THouston

11:12:02 AM

1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

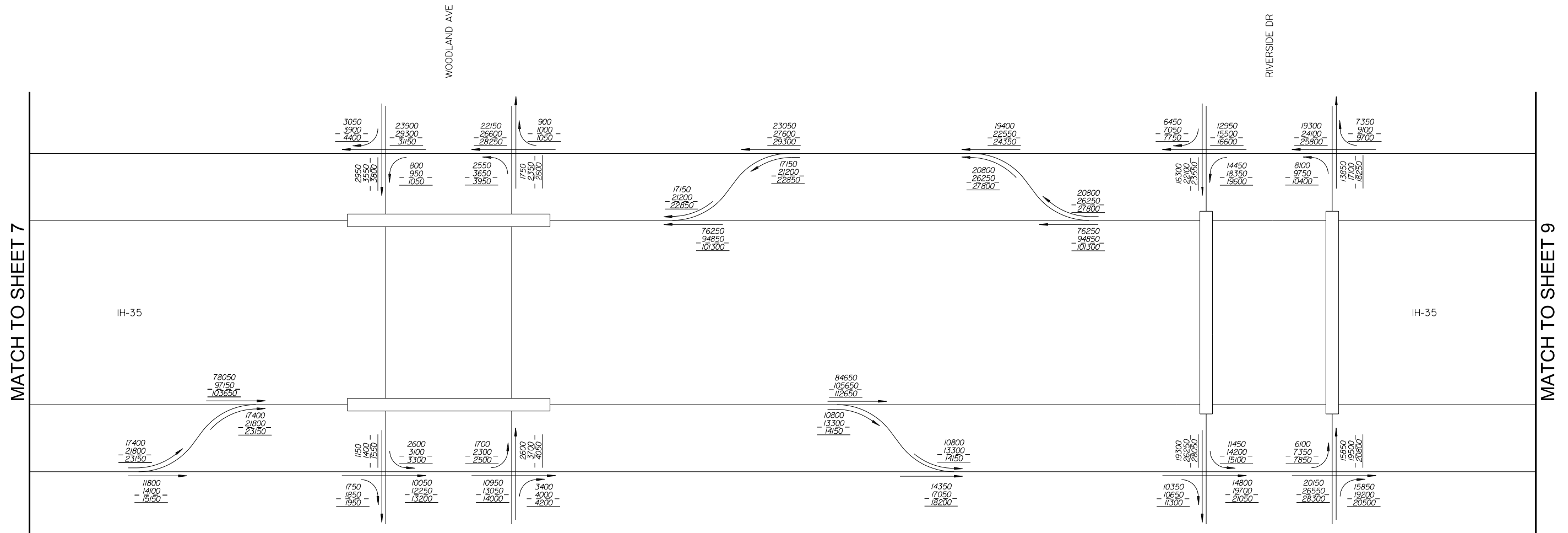
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 7 OF 28)

| | | | | | |
|------------------|----------------|---------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. NO. | COUNTY | |
| TEXAS | 14 | 6 | | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 7 | |

NO-BUILD CONFIGURATION



MATCH TO SHEET 7

MATCH TO SHEET 9

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

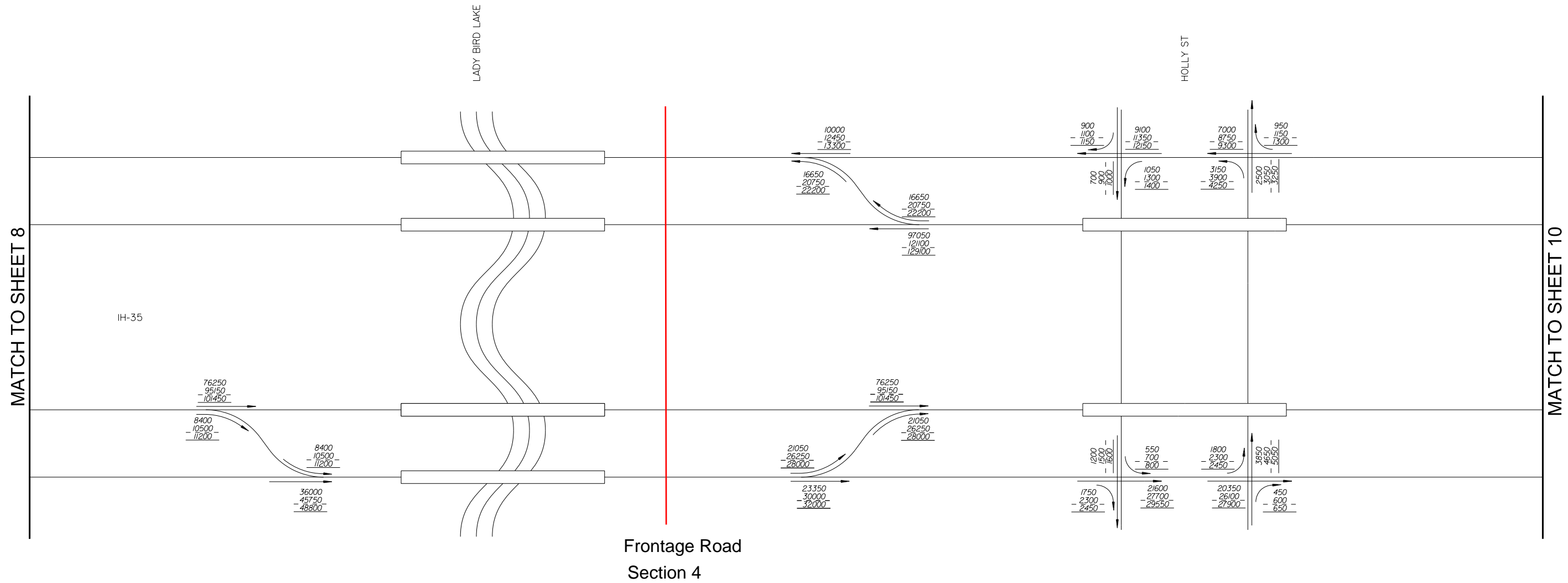
CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES

(SHEET 8 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 8 |

NO-BUILD CONFIGURATION



Frontage Road
Section 4

MATCH TO SHEET 8

MATCH TO SHEET 10

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

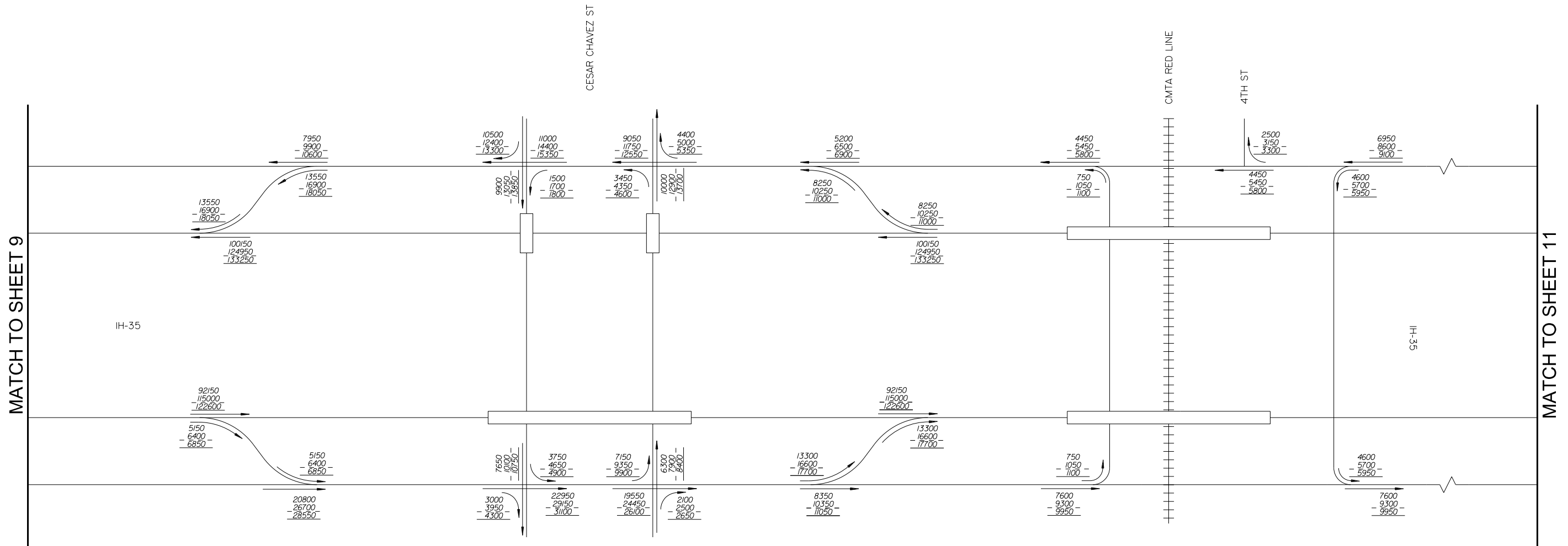
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 9 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 9 |

NO-BUILD CONFIGURATION



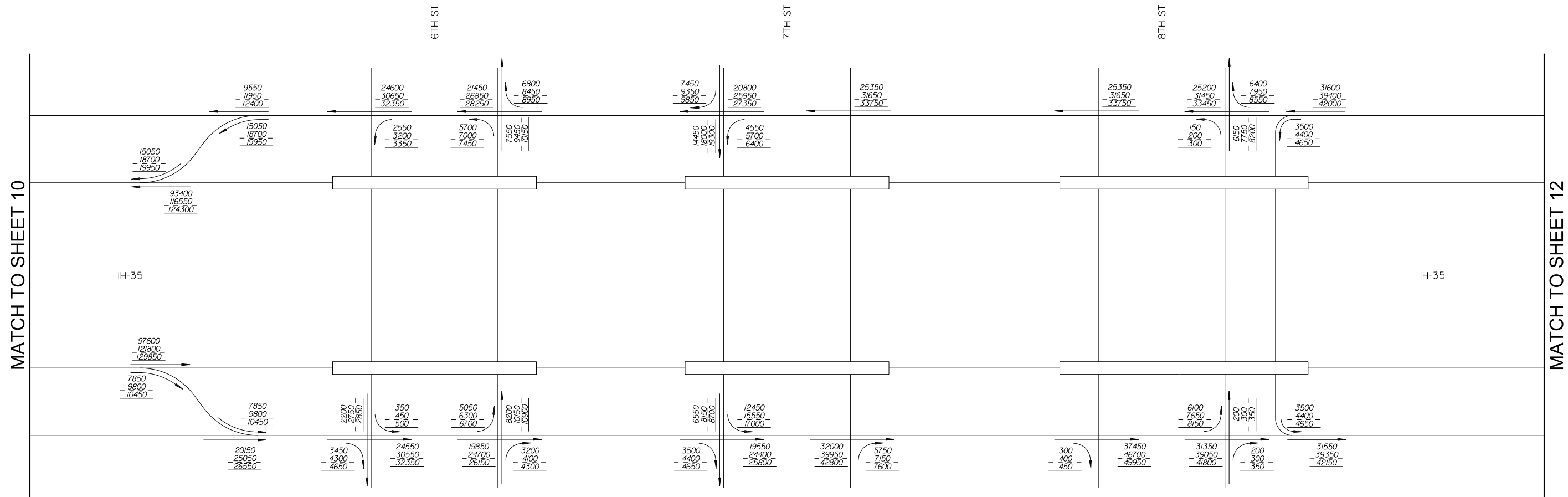
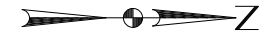
2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|---|----------------|-------------------|----------|-----------|
| | | | | |
| | | | | |
| CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 10 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 10 |


NO-BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



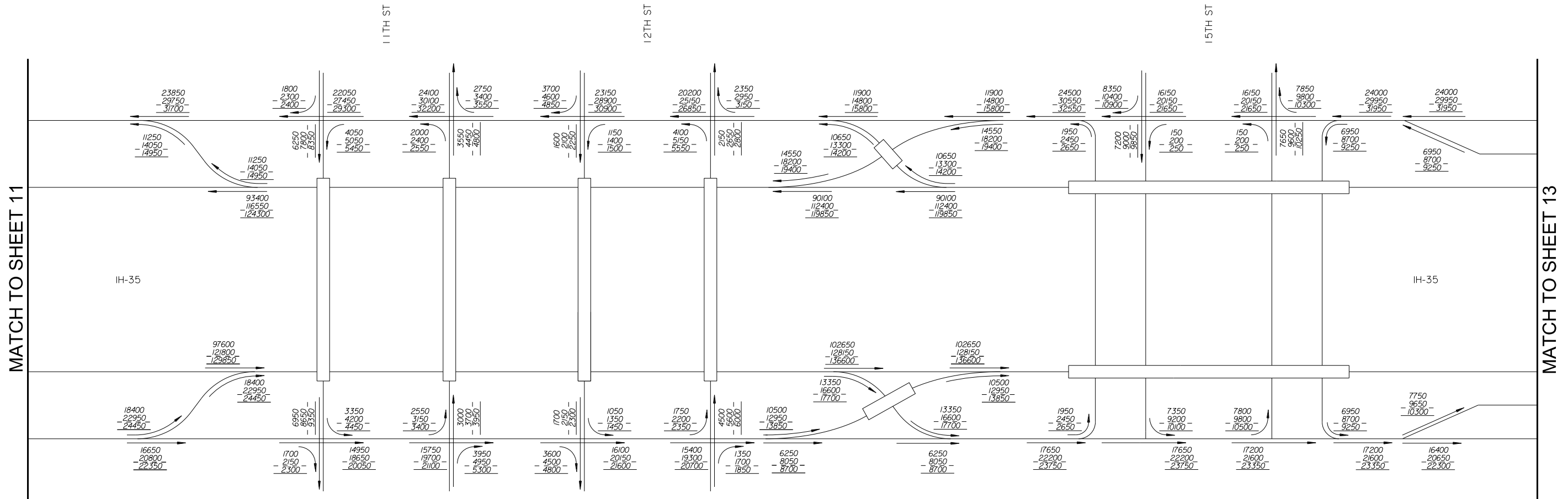
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 11 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 11 |

NO-BUILD CONFIGURATION



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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

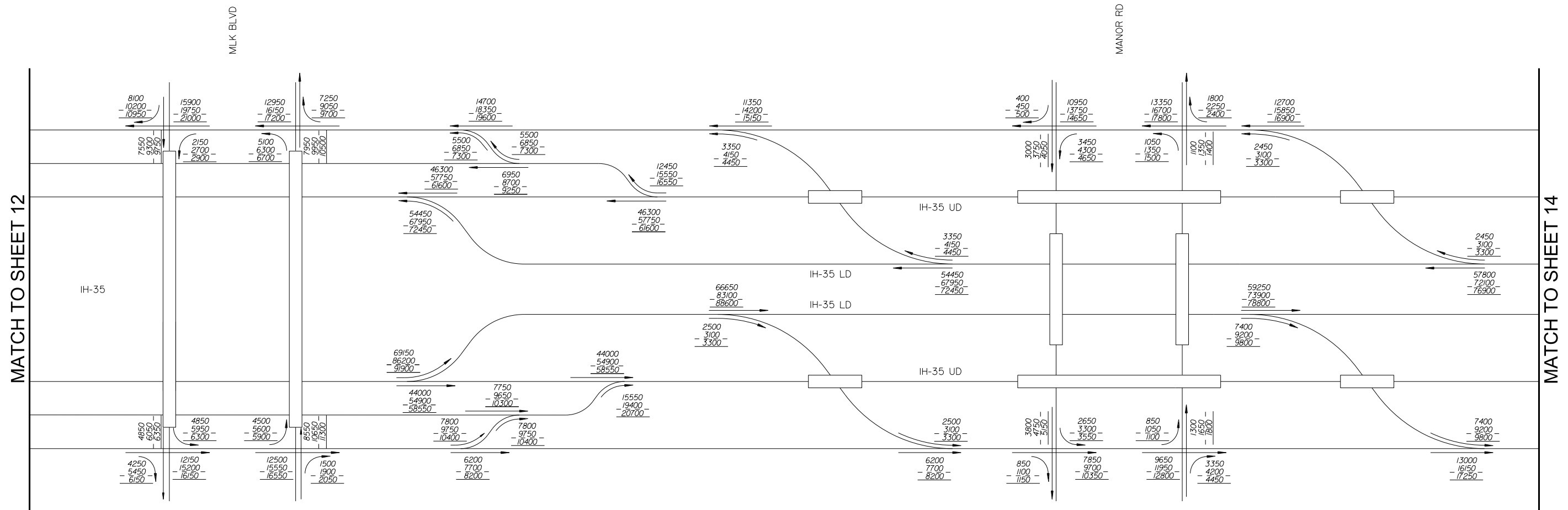
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 12 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 12 |

NO-BUILD CONFIGURATION



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Houston


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1/25/2019


2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



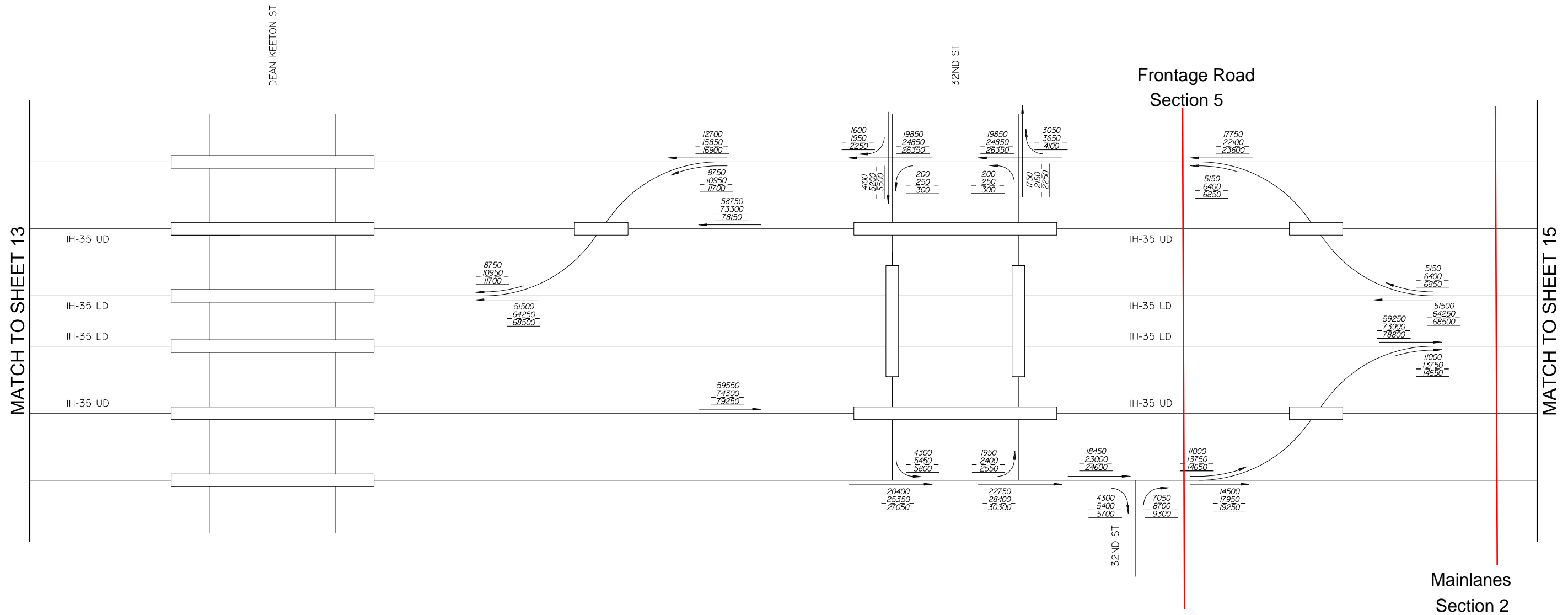
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 13 OF 28)

| | | | |
|------------------|---------|-------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE | FED. RD. DISTRICT |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 13 |



NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

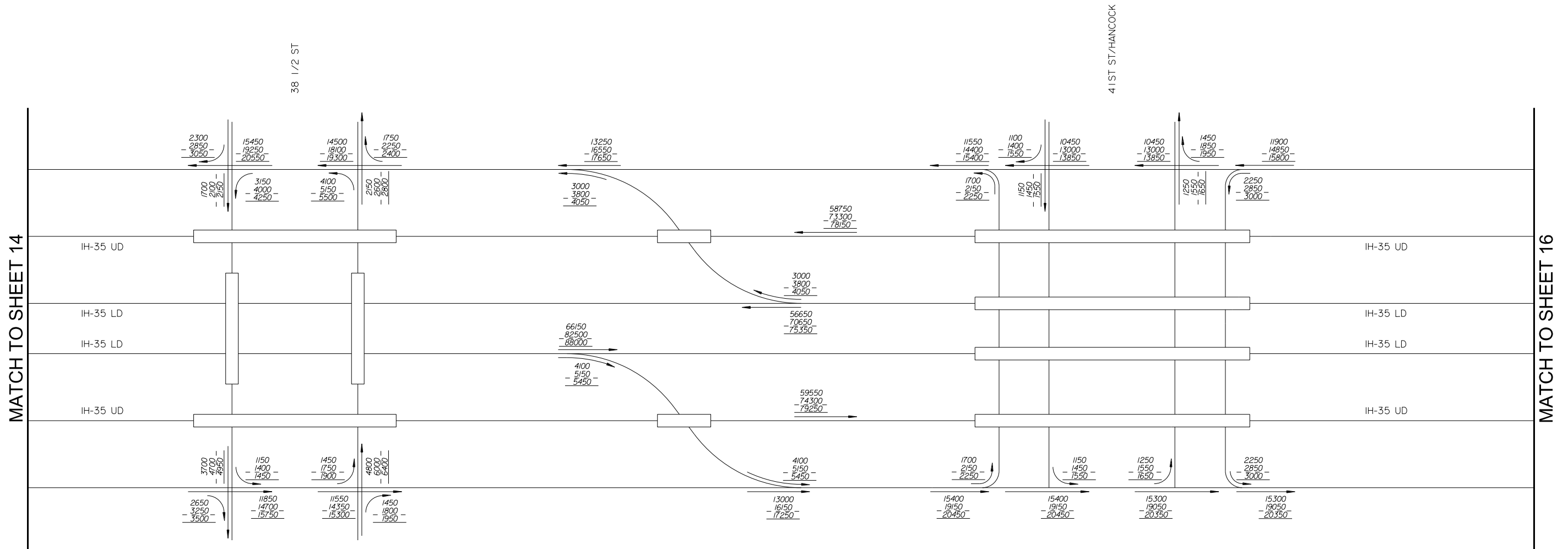
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 14 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 14 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

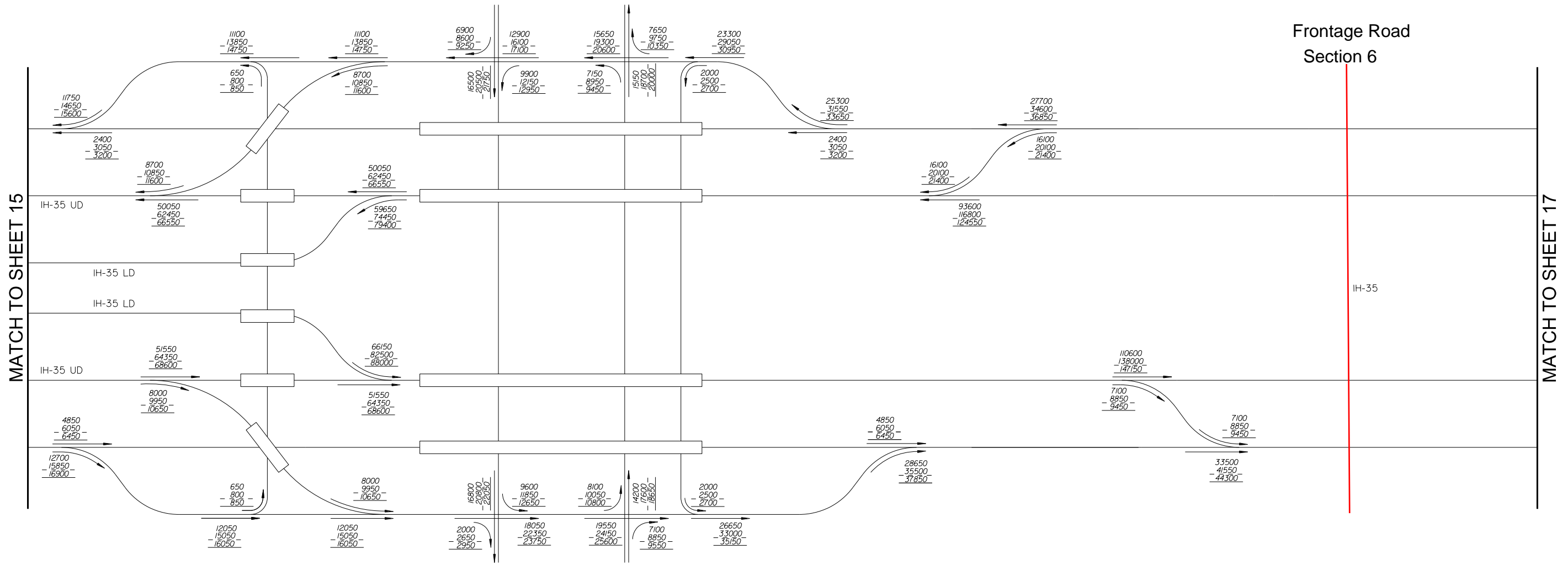
(SHEET 15 OF 28)

| | | | | |
|------------------|----------------|---------------|------------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 15 |

NO-BUILD CONFIGURATION



Frontage Road Section 6



MATCH TO SHEET 15

MATCH TO SHEET 17

AIRPORT BLVD

IH-35

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

ATG ALLIANCE
TRANSPORTATION GROUP

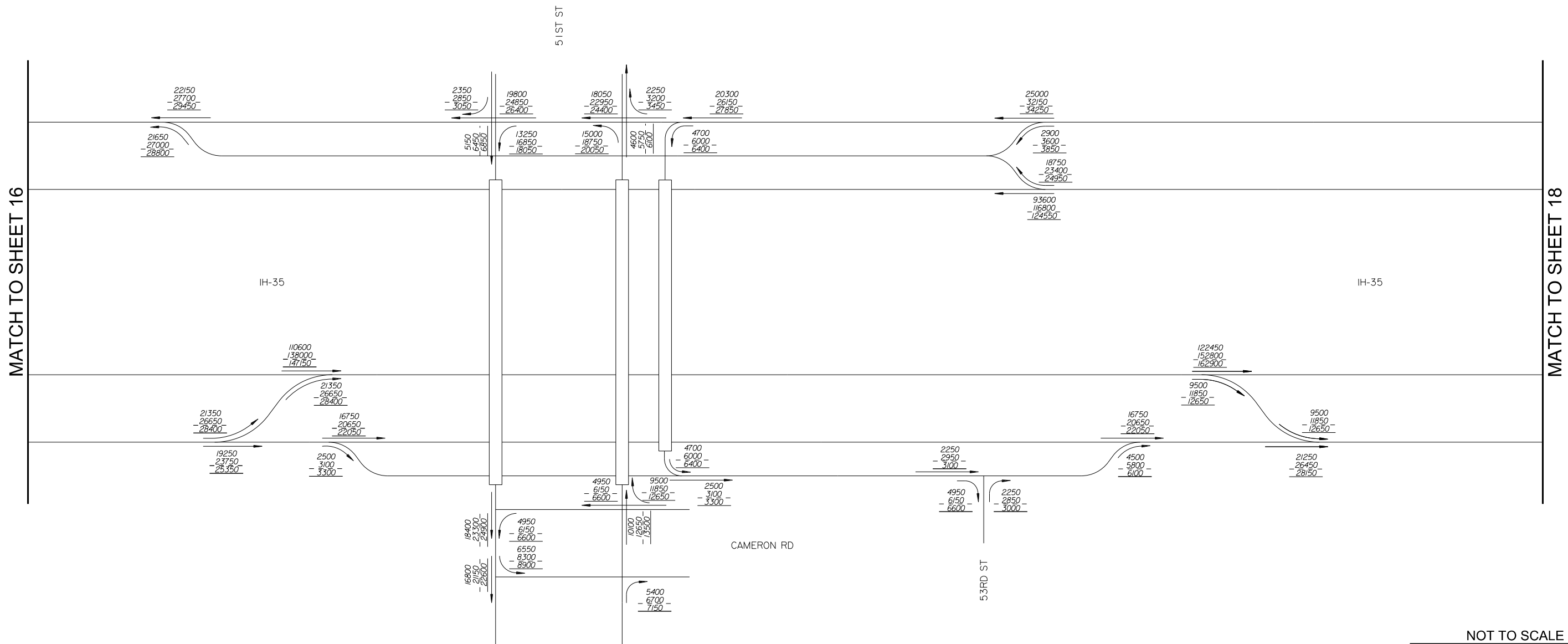
CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 16 OF 28)

| | | | |
|------------------|----------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

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NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 17 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
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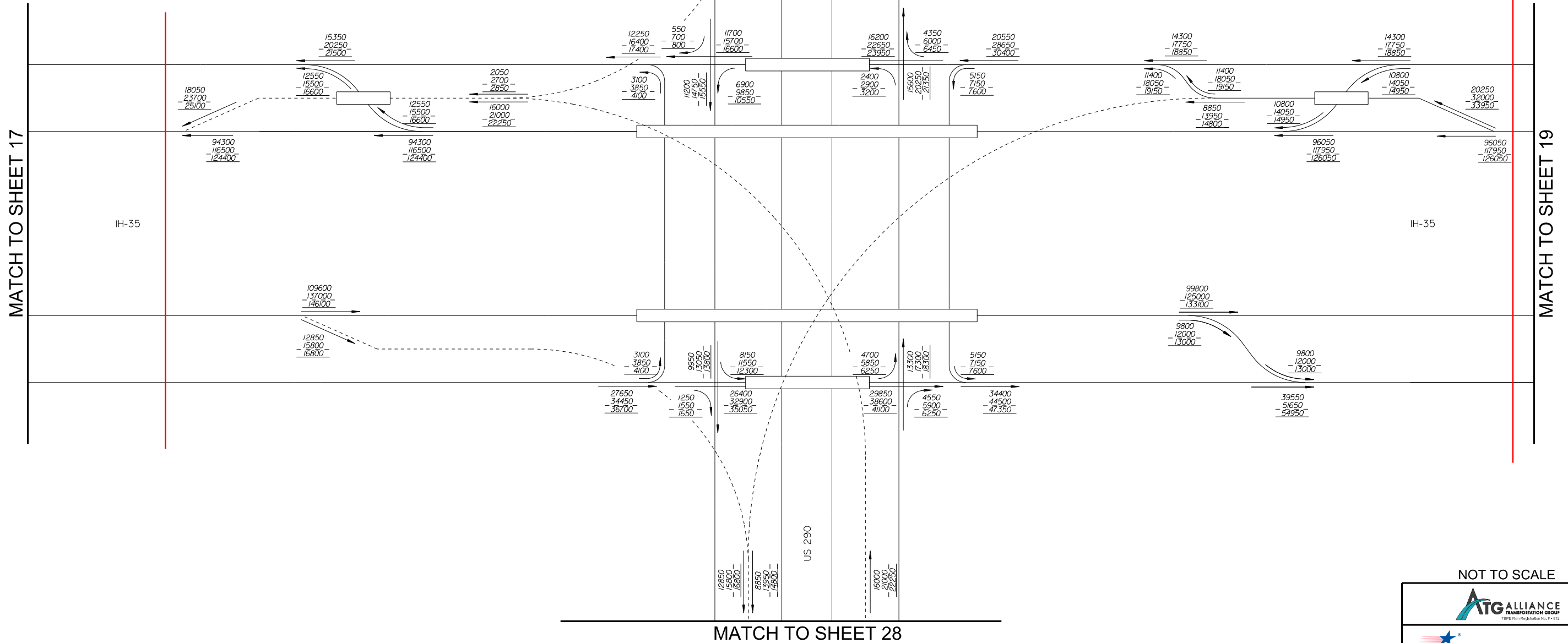
NO-BUILD CONFIGURATION

MATCH TO SHEET 27



Frontage Road
Section 7

Frontage Road
Section 8



NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 18 OF 28)

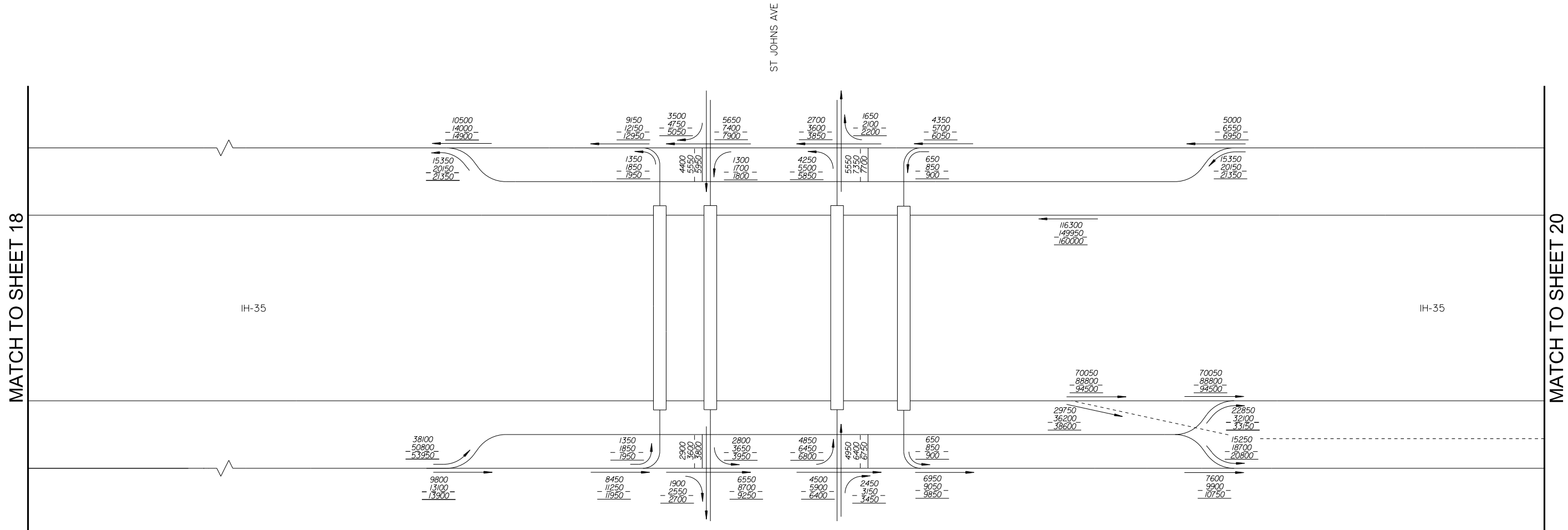
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|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

NO-BUILD CONFIGURATION



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

ATG ALLIANCE
TRANSPORTATION GROUP

Texas Department of Transportation

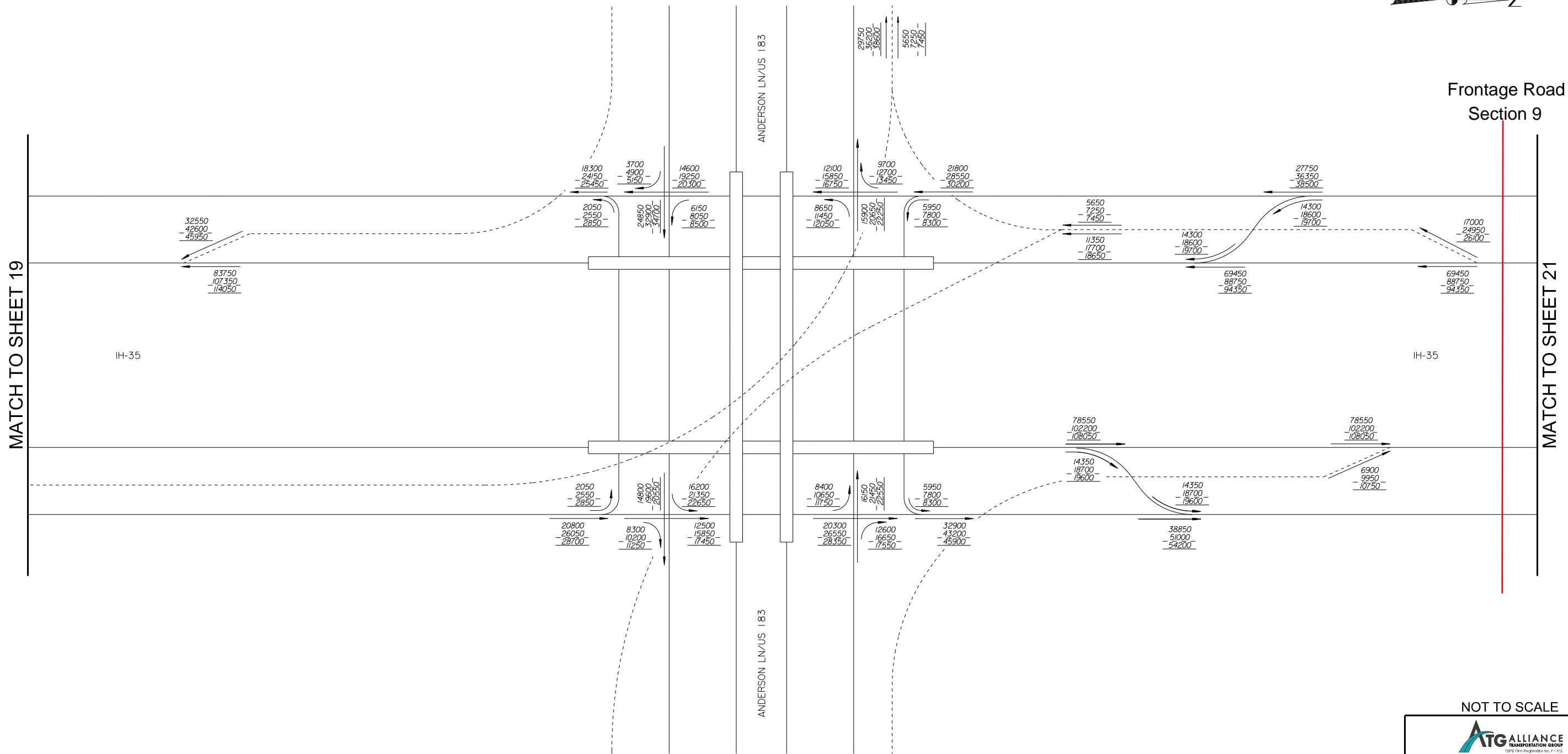
CAPITAL EXPRESS
 NO-BUILD CONFIGURATION
 24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 19 |

NO-BUILD CONFIGURATION



Frontage Road
Section 9





2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

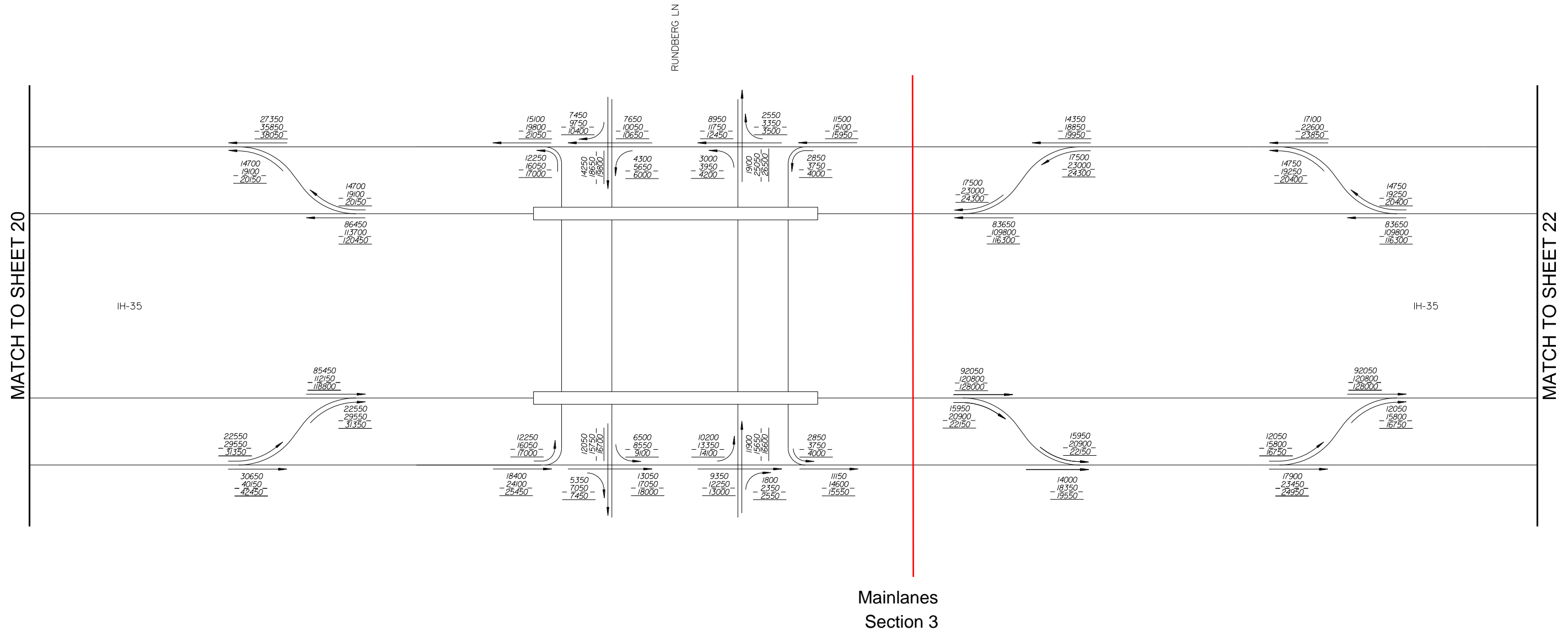
LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|--|----------------|---------------|------------|-----------|
|   | | | | |
| CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 20 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 20 |

NO-BUILD CONFIGURATION



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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

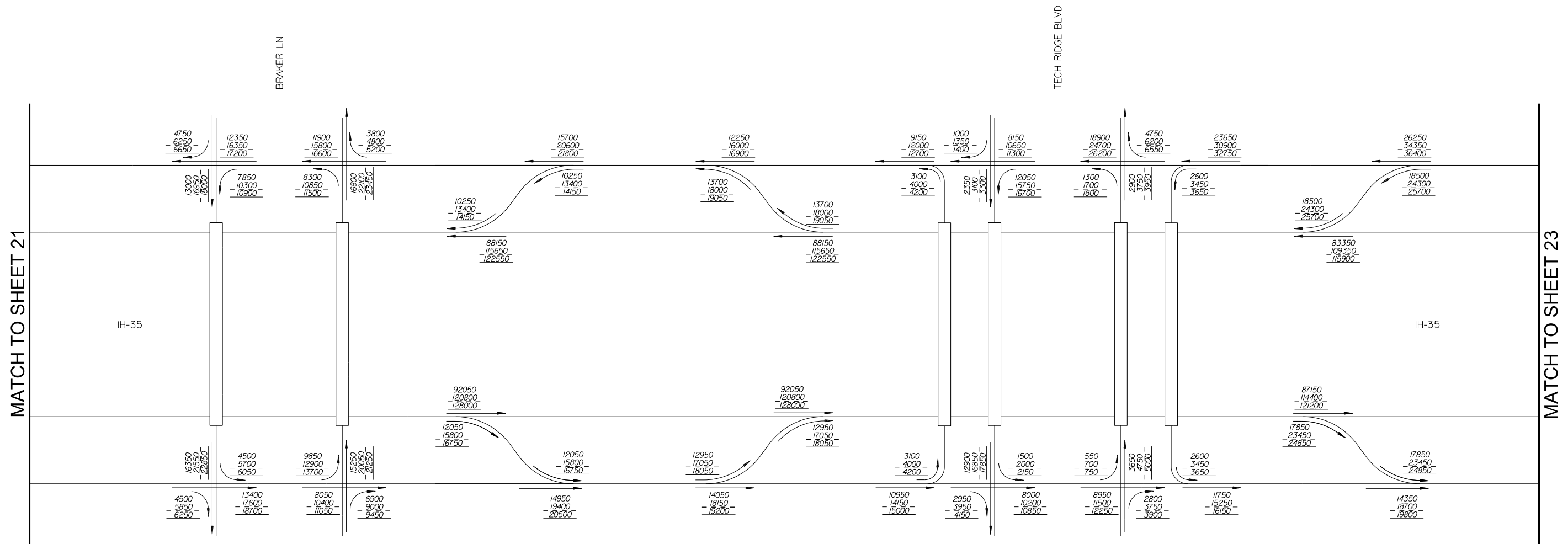


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 21 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 21 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

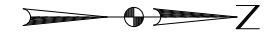
LEGEND

1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
LD - LOWER DECK
UD - UPPER DECK
→ TRAVEL DIRECTION

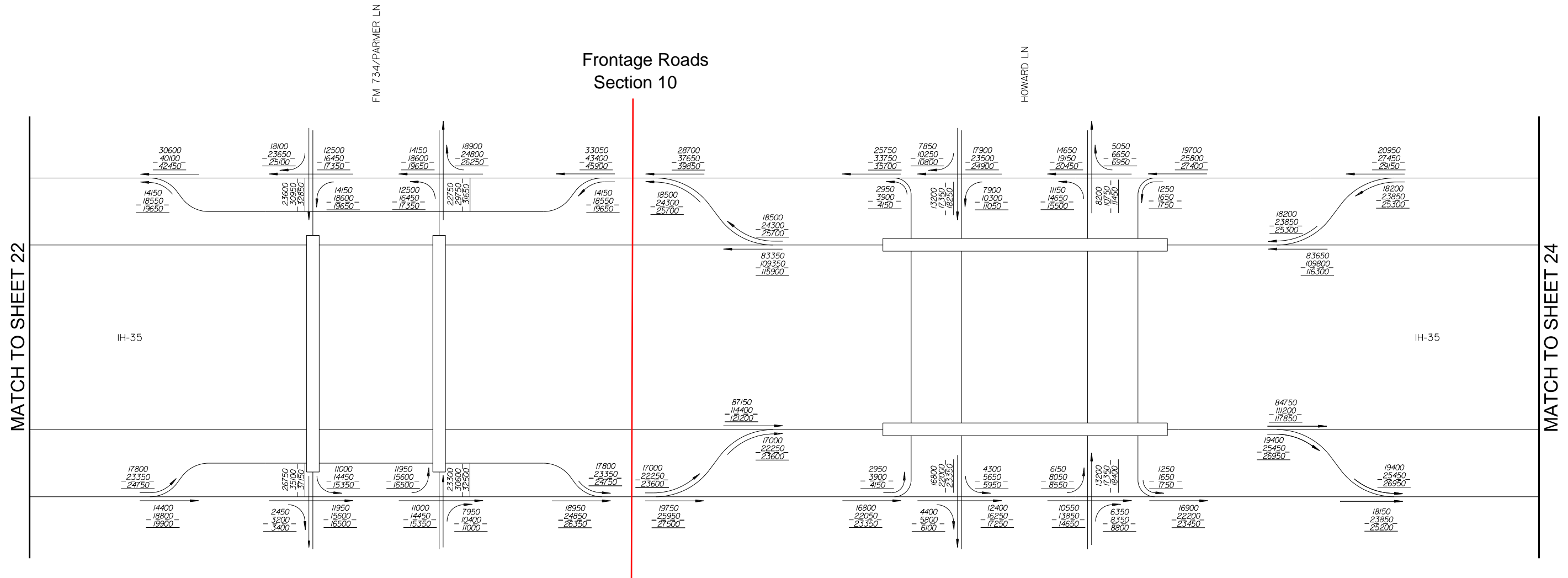
NOT TO SCALE

| | | | | |
|---|----------------|-------------------|----------|-----------|
| | | | | |
| | | | | |
| CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 22 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 22 |

NO-BUILD CONFIGURATION



Frontage Roads Section 10



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Thouston

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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

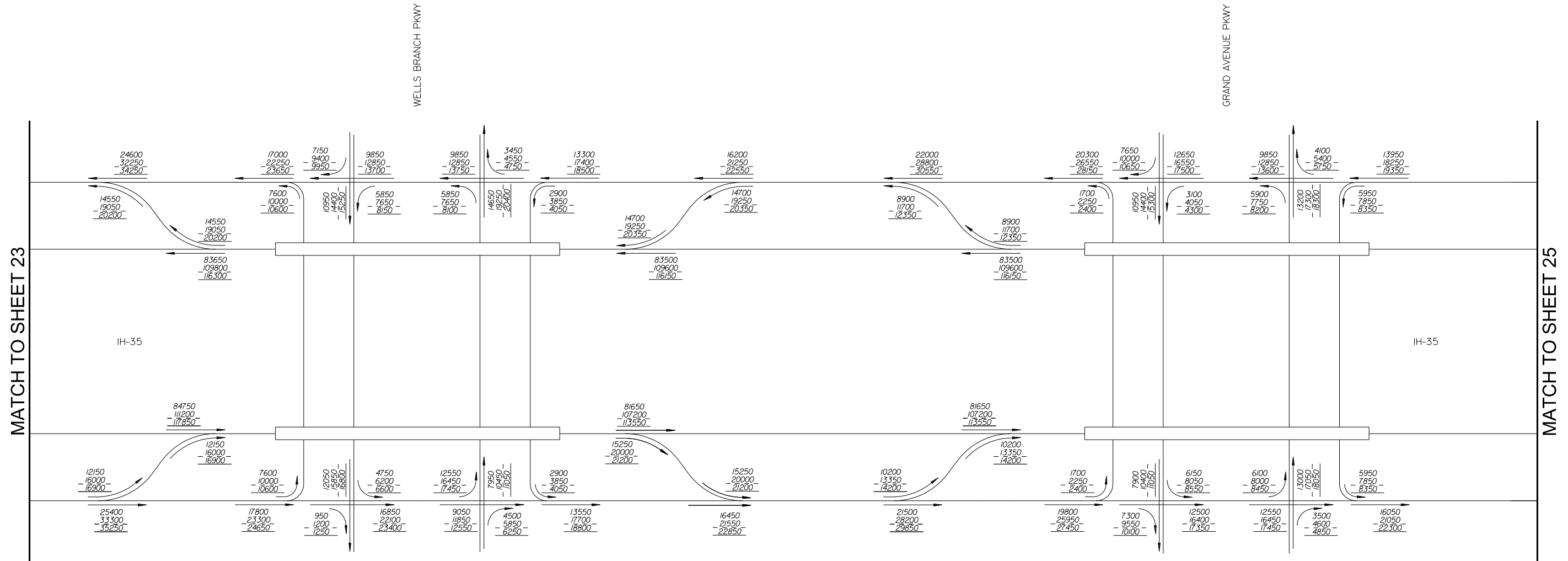


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 23 OF 28)

| | | | | |
|------------------|----------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 23 |

NO-BUILD CONFIGURATION





1/25/2019 11:12:07 AM THouston ... \2018.0011*LineDiagrams*TPP*NB.dgn

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

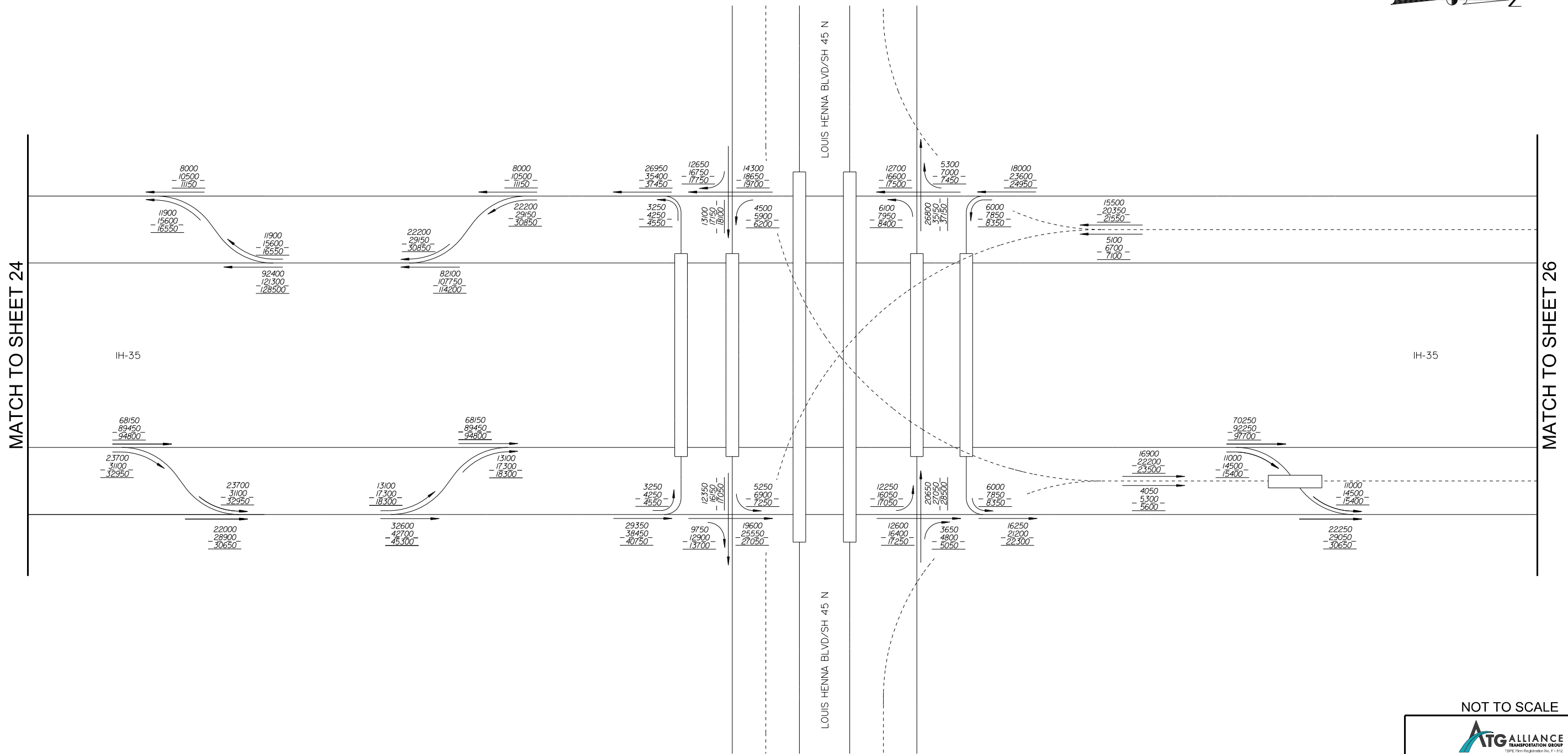
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 24 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 24 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

... \2018.0011 *LineDiagrams*TPP*NB.dgn


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1/25/2019

NOT TO SCALE



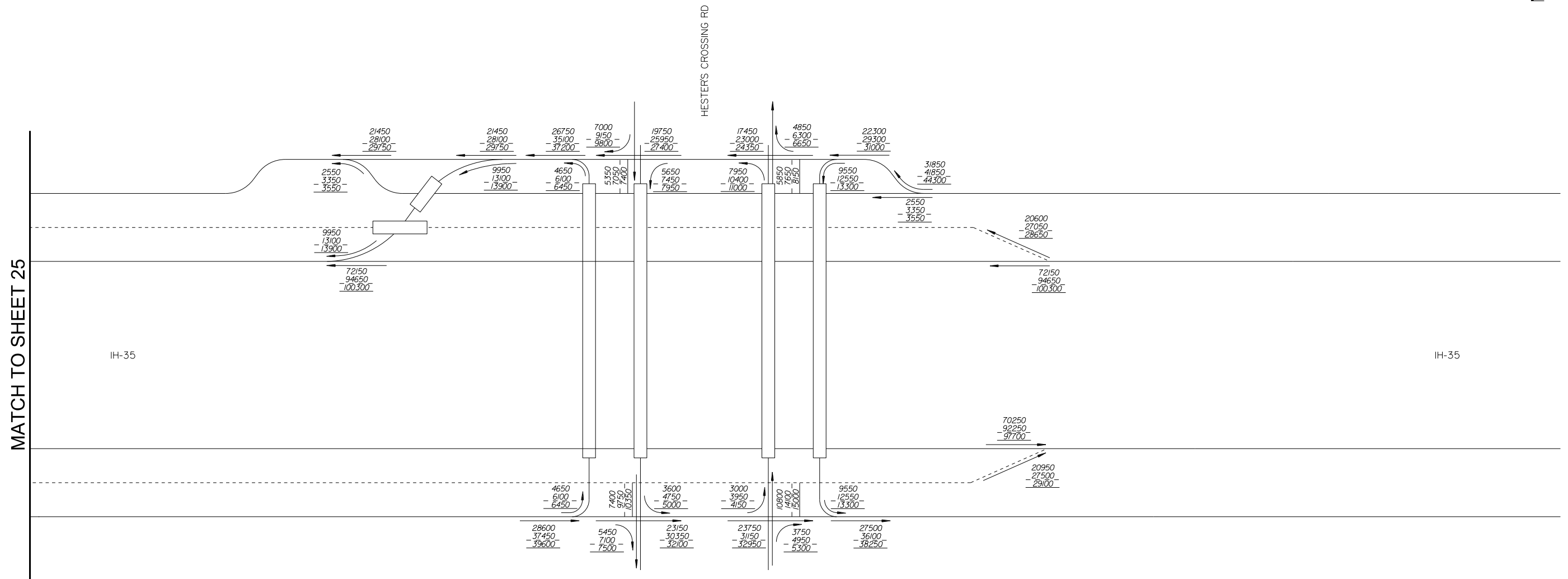
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 25 OF 28)

| | | | |
|------------------|----------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 25 |

NO-BUILD CONFIGURATION



... \2018.0011 *LineDiagrams*TPP*NB.dgn

THouston

11:12:08 AM

1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

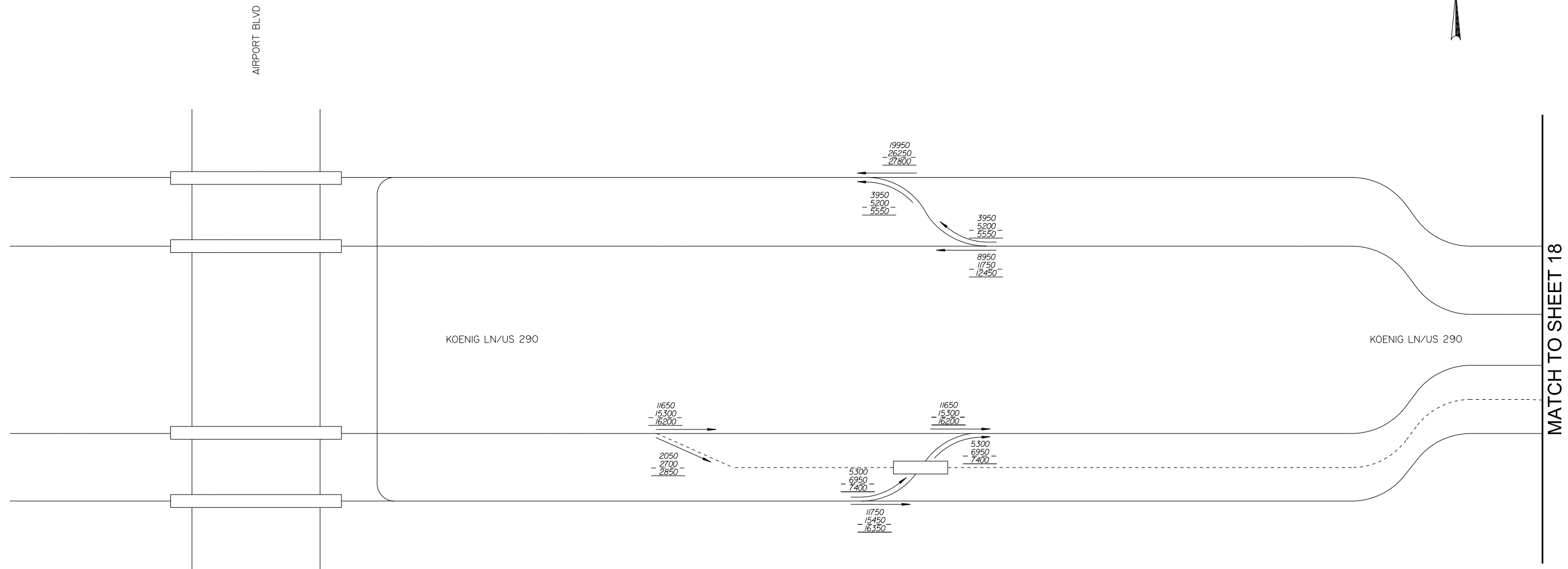


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 26 OF 28)

| | | | | |
|------------------|----------------|---------------|------------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | WILLIAMSON | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 26 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE

ATG ALLIANCE
TRANSPORTATION GROUP

Texas Department of Transportation

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 27 OF 28)

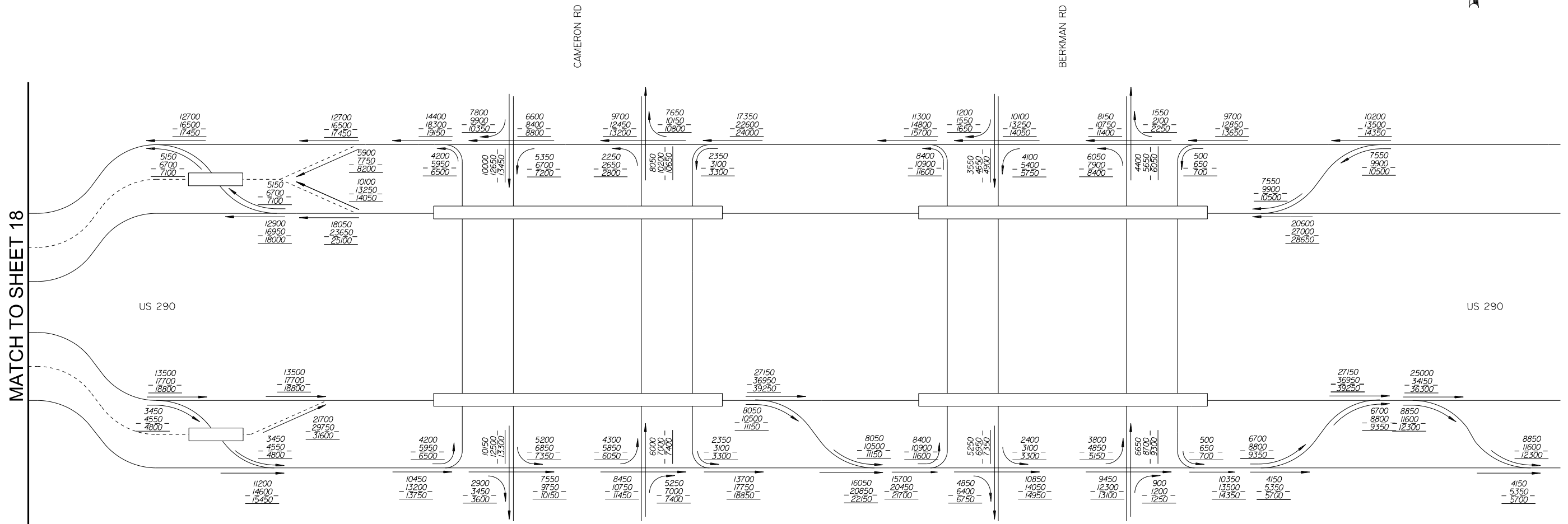
| | | | |
|------------------|----------------|---------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 27 |

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1/25/2019

NO-BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 28 OF 28)

| | | | |
|------------------|----------------|---------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 28 |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Mainlanes & Managed Lanes) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From William Cannon Drive To MLK Blvd | 203,000 | 251,450 | 51 - 49 | 6.0 | 9.5 | 4.3 | 13,500 | 20 | 76,923,500 | 3 | 108,024,000 | 8" |
| Travis County | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| Base Year | | | | | | | | | | | | |
| % of ADT | | | | | | | | | | | | |
| % of DHV | | | | | | | | | | | | |
| Light Duty | | | | | | | | | | | | |
| 90.5 | | | | | | | | | | | | |
| Medium Duty | | | | | | | | | | | | |
| 2.5 | | | | | | | | | | | | |
| Heavy Duty | | | | | | | | | | | | |
| 7.0 | | | | | | | | | | | | |
| 3.2 | | | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Mainlanes & Managed Lanes) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From William Cannon Drive To MLK Blvd | 203,000 | 268,950 | 51 - 49 | 6.0 | 9.5 | 4.3 | 13,600 | 20 | 119,828,500 | 3 | 168,275,500 | 8" |
| Travis County | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Mainlanes & Managed Lanes)</u></p> <p align="center"><u>Section 2</u></p> <p>From MLK Blvd To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 234,700 | 293,200 | 51 - 49 | 6.0 | 8.9 | 4.0 | 13,600 | 20 | 83,750,500 | 3 | 117,583,000 | 8" |
| <p align="center">Data for Use in Air & Noise Analysis</p> | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 91.1 | | 96.0 | | | | | | | | | |
| Medium Duty | 2.3 | | 1.0 | | | | | | | | | |
| Heavy Duty | 6.6 | | 3.0 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Mainlanes & Managed Lanes)</u></p> <p align="center"><u>Section 2</u></p> <p>From MLK Blvd To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 234,700 | 312,150 | 51 - 49 | 6.0 | 8.9 | 4.0 | 13,700 | 20 | 130,136,000 | 3 | 182,706,000 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|-----------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Frontage Roads) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From William Cannon Drive To Ben White Blvd/SH 71 | | | | | | | | | | | | |
| Travis County | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | |
| Light Duty | 97.2 | | 97.9 | | | | | | | | | |
| Medium Duty | 1.7 | | 1.3 | | | | | | | | | |
| Heavy Duty | 1.1 | | 0.8 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| I-35 (Build Frontage Roads) | | | | | | | | | | | | |
| Section 1 | | | | | | | | | | | | |
| From William Cannon Drive To Ben White Blvd/SH 71 | | | | | | | | | | | | |
| Travis County | | | | | | | | | | | | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Ben White Blvd/SH 71 To Oltorf Street</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 48,600 | 59,250 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 5,525,500 | 3 | 6,811,000 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 95.9 | | 96.9 | | | | | | | | | |
| Medium Duty | 2.4 | | 1.8 | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.3 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 2</u></p> <p>From Ben White Blvd/SH 71 To Oltorf Street</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 48,600 | 63,450 | 51 - 49 | 6.0 | 4.1 | 3.1 | 11,900 | 30 | 8,611,500 | 3 | 10,614,500 | 8" |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|---|--|----------|------------|----------|----------------|--------|--------|--------------------------------|---|------------|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 3</u></p> <p>From Oltorf Street To MLK Blvd</p> <p>Travis County</p> | | | | | | | | | | | |
| 113,700 | 143,450 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,200 | 30 | 9,090,500 | 3 | 11,152,500 | 8" | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | |
| Light Duty | 97.2 | 97.9 | | | | | | | | | | |
| Medium Duty | 1.7 | 1.3 | | | | | | | | | | |
| Heavy Duty | 1.1 | 0.8 | | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 3</u></p> <p>From Oltorf Street To MLK Blvd</p> <p>Travis County</p> | | | | | | | | | | | |
| 113,700 | 151,650 | 51 - 49 | 6.0 | 2.8 | 2.1 | 12,200 | 30 | 14,071,000 | 3 | 17,262,500 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|--------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 4</u></p> <p>From MLK Blvd To 38 1/2th Street</p> <p>Travis County</p> | | | | | | | | | | | | | |
| | 47,300 | 60,750 | 51 - 49 | 6.0 | 4.2 | 3.2 | 11,900 | 30 | 5,668,000 | 3 | 6,988,000 | 8" | |
| <p align="center">Data for Use in Air & Noise Analysis</p> | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | |
| Light Duty | 95.8 | | 96.8 | | | | | | | | | | |
| Medium Duty | 2.5 | | 1.9 | | | | | | | | | | |
| Heavy Duty | 1.7 | | 1.3 | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 4</u></p> <p>From MLK Blvd To 38 1/2th Street</p> <p>Travis County</p> | | | | | | | | | | | | | |
| | 47,300 | 65,400 | 51 - 49 | 6.0 | 4.2 | 3.2 | 11,900 | 30 | 8,868,000 | 3 | 10,933,500 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | |
|--|-----------------------|---------|------------|----------|----------------|-----|--------|--------------------------------|---|-----|----------------|------|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 5</u></p> <p>From 38 1/2th Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 132,050 | 166,000 | 51 - 49 | 6.0 | 2.7 | 2.0 | 12,200 | 30 | 10,172,500 | 3 | 12,472,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 97.3 | | 98.0 | | | | | | | | | |
| Medium Duty | 1.6 | | 1.2 | | | | | | | | | |
| Heavy Duty | 1.1 | | 0.8 | | | | | | | | | |
| | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | | | | |
| | Base Year | | | | Base Year | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 5</u></p> <p>From 38 1/2th Street To US 290</p> <p>Travis County</p> | | | | | | | | | | | | |
| | 132,050 | 177,800 | 51 - 49 | 6.0 | 2.7 | 2.0 | 12,300 | 30 | 15,863,000 | 3 | 19,450,000 | 8" |

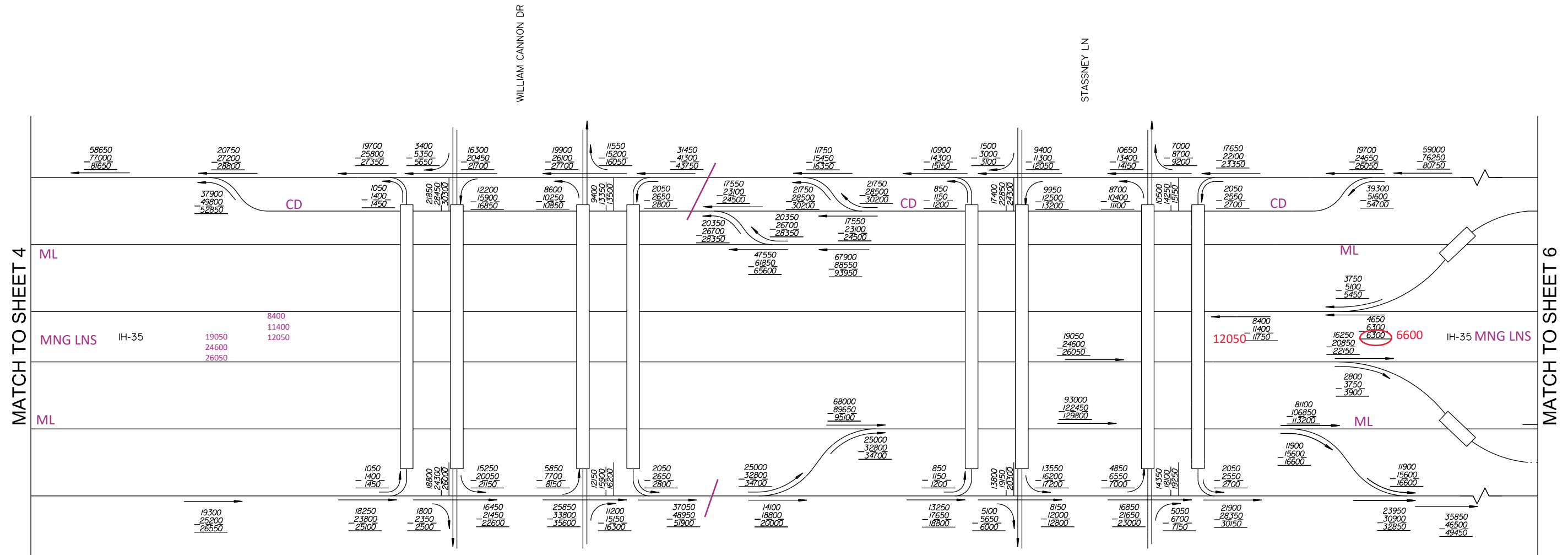
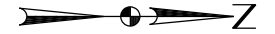
TRAFFIC ANALYSIS FOR HIGHWAY DESIGN (OPTION C)

Austin District

March 1, 2023

| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | | | |
|--|-----------------------|------|------------|----------|----------------|-----|--------|--------------------------------|-------------------|---|----------------|------|--------|---------|---------|-----|-----|-----|--------|----|------------|---|------------|----|
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2050 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From US 290 To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | | 74,050 | 91,600 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 6,868,000 | 3 | 8,444,500 | 8" |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | | | | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | | | | | | | | | | | | | |
| Light Duty | 96.7 | | 97.5 | | | | | | | | | | | | | | | | | | | | | |
| Medium Duty | 2.0 | | 1.5 | | | | | | | | | | | | | | | | | | | | | |
| Heavy Duty | 1.3 | | 1.0 | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | | | |
| Description of Location | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | S N | Rigid Pavement | SLAB | | | | | | | | | | | | |
| | 2030 | 2060 | | | ADT | DHV | | | | | | | | | | | | | | | | | | |
| | Base Year | | | | Base Year | | | | | | | | | | | | | | | | | | | |
| <p align="center"><u>I-35 (Build Frontage Roads)</u></p> <p align="center"><u>Section 6</u></p> <p>From US 290 To St. Johns Ave</p> <p>Travis County</p> | | | | | | | | | | | | | 74,050 | 100,350 | 51 - 49 | 6.0 | 3.3 | 2.5 | 12,000 | 30 | 10,846,000 | 3 | 13,336,000 | 8" |

BUILD CONFIGURATION



BUILD SECTION 1:
 From William Cannon Dr
 To Ben White Blvd/SH 71
 Frontage Roads (Collector Distributor Lanes included)
 110500
 145350
 154100

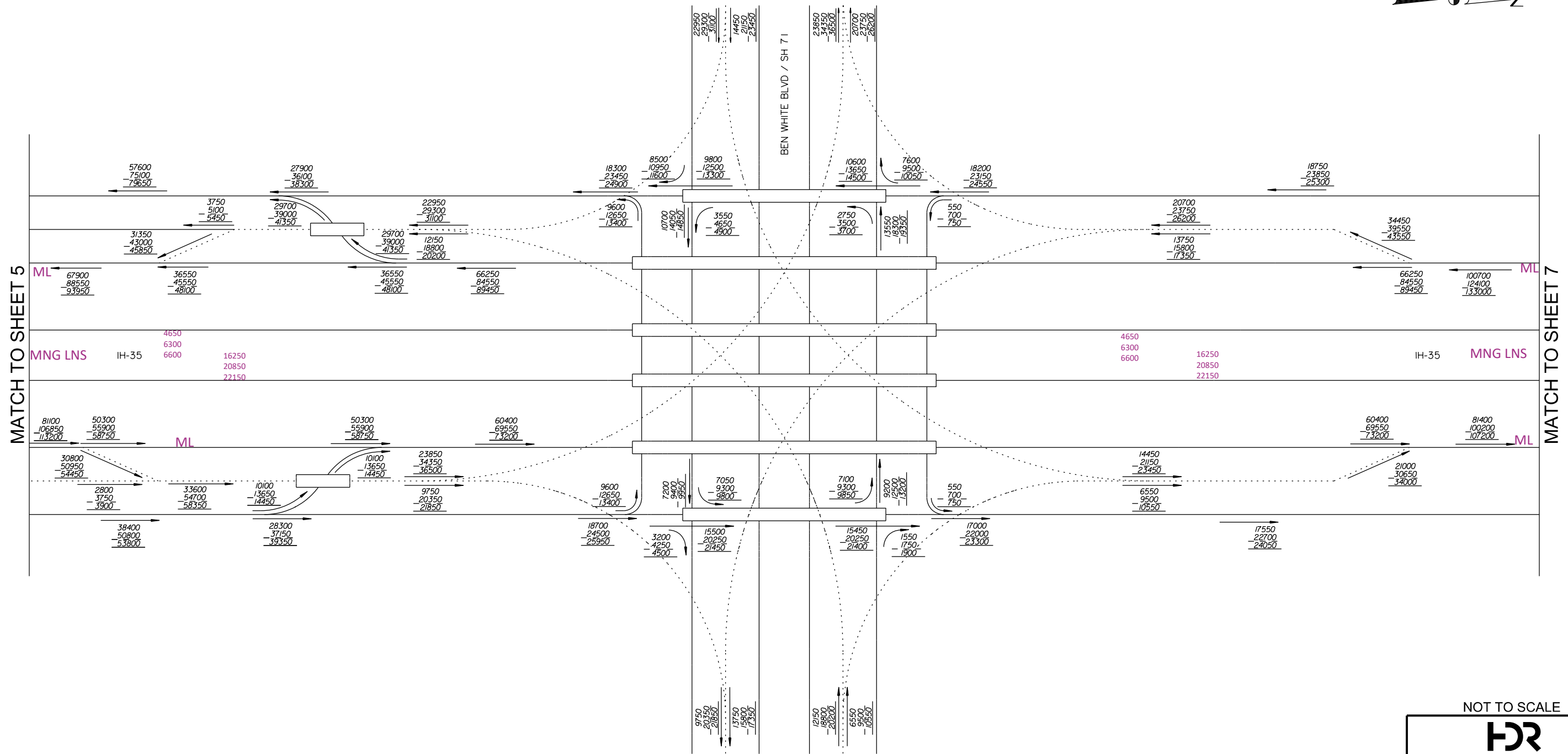
2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|------------------------------------|---------|-------------|-------------------|-----------|
| HR | | | | |
| Texas Department of Transportation | | | | |
| CAPITAL EXPRESS | | | | |
| BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES | | | | |
| (SHEET 5 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | STATE | CKD: HH | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |


BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



Texas Department of Transportation

CAPITAL EXPRESS

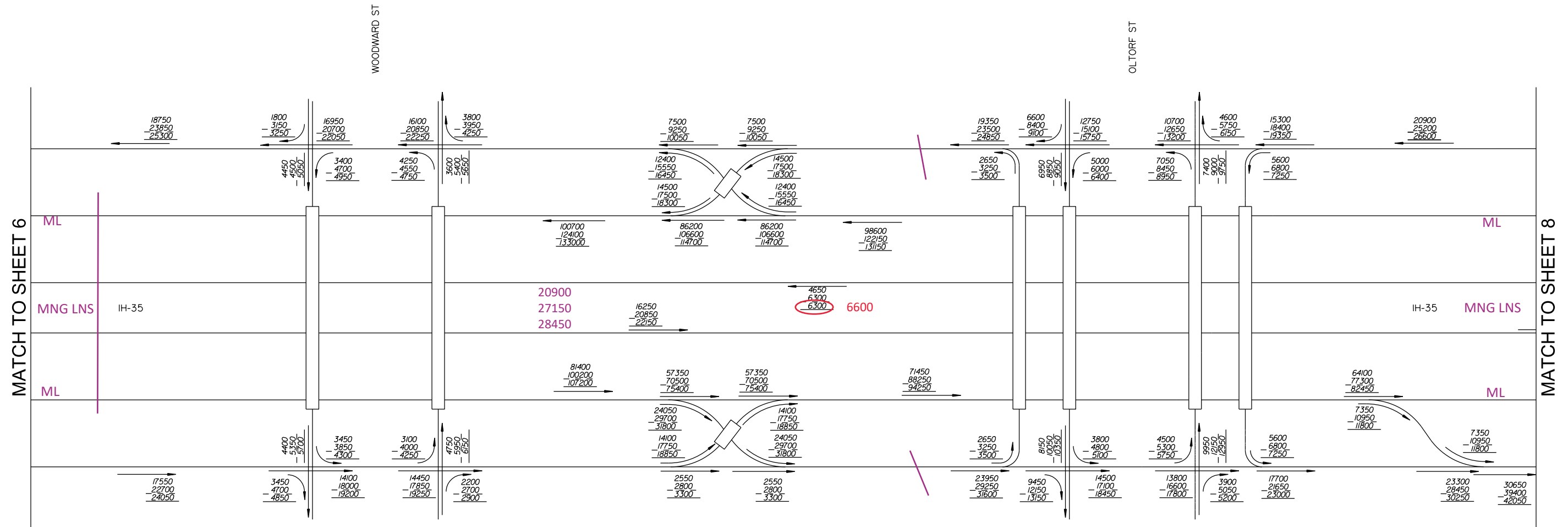
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 6 OF 28)

SCALE: N. T. S. PROJECT NO.

| | | | | |
|---------|----------------|---------|-------------------|-----------|
| DWN: TH | STATE DISTRICT | CKD: HH | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 6 |

BUILD CONFIGURATION



BUILD SECTION 1:
From William Cannon Dr
To MLK Blvd

ML+Managed Lanes
203000
251450
268950

BUILD SECTION 2:
From Ben White Blvd/SH 71
To Oltorf Street

Frontage Roads
48600
59250
63450

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
→ TRAVEL DIRECTION

NOT TO SCALE

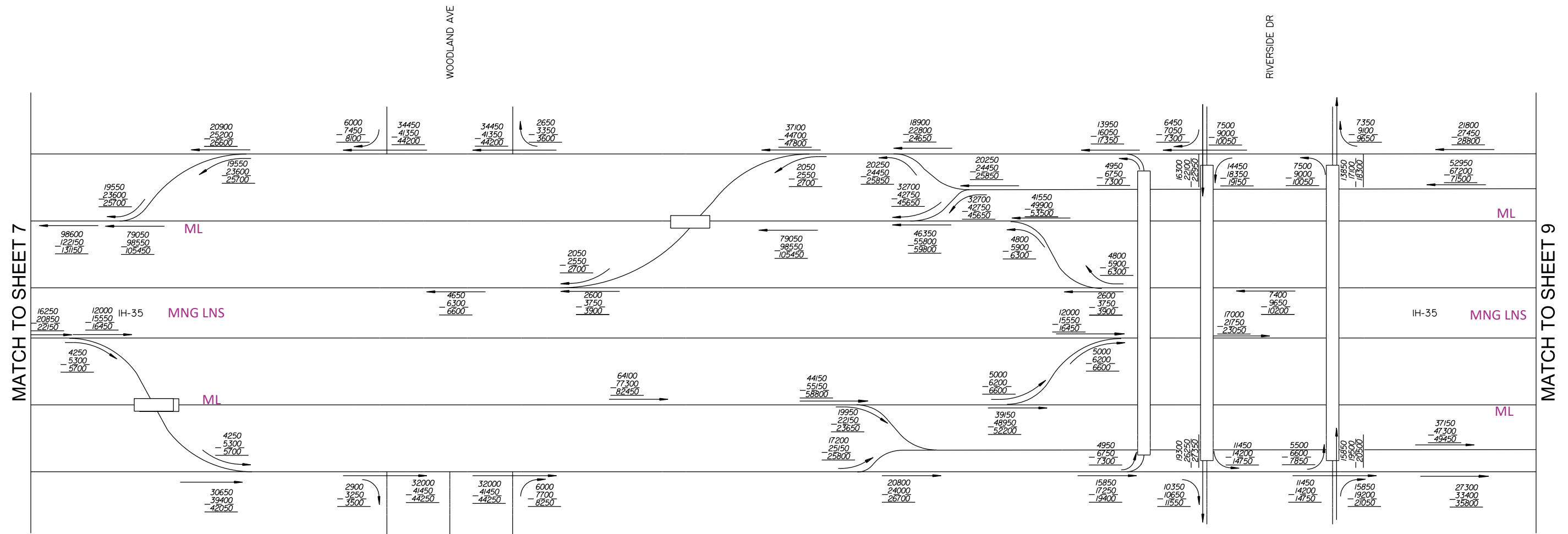
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 7 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 7 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



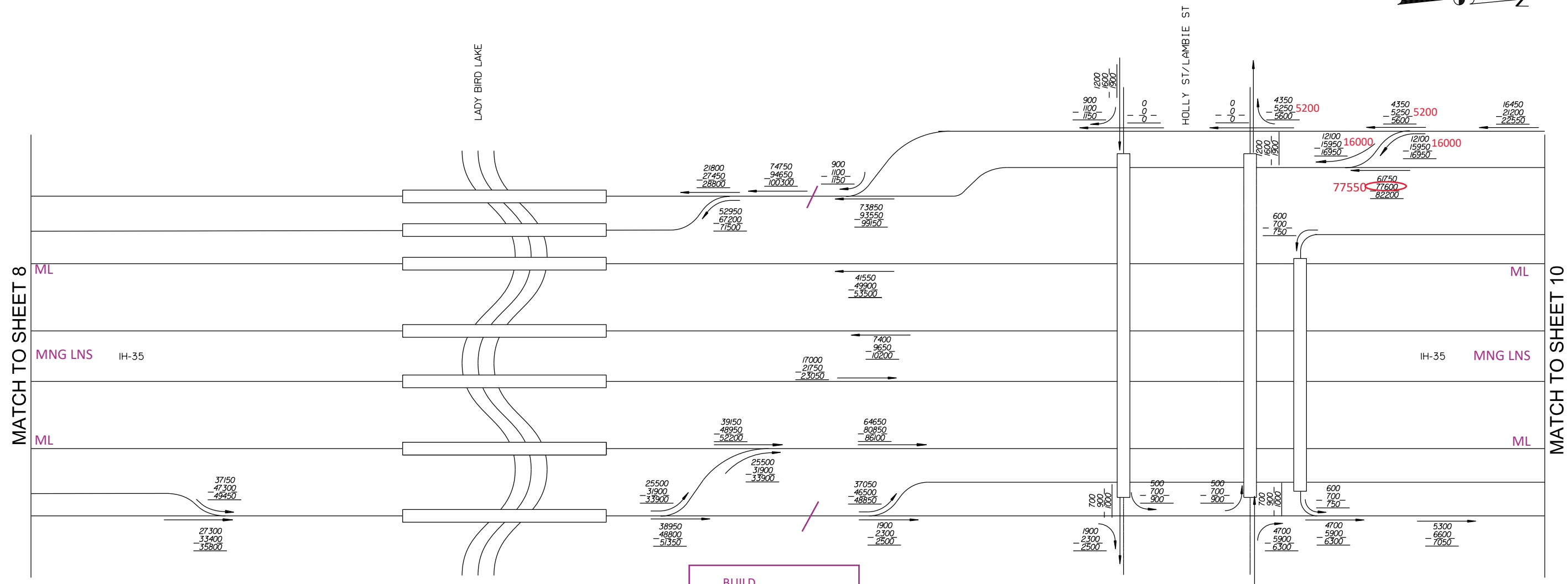
Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION

24 HOUR VOLUMES
 (SHEET 8 OF 28)

| | | | | |
|------------------|----------------|---------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 8 |

BUILD CONFIGURATION



BUILD SECTION 3:
 From Oltorf Street
 To MLK Blvd
 Frontage Roads
 113700
 143450
 151650

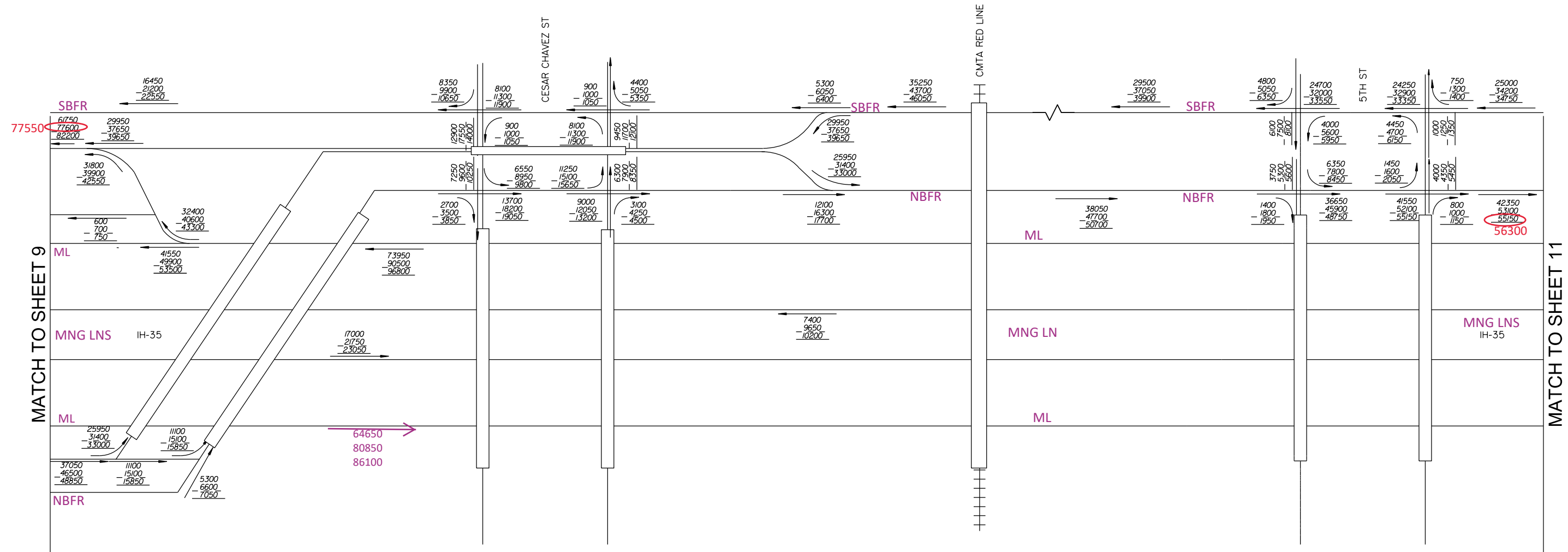
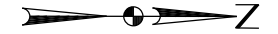
2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|------------------------------------|---------|---------|-------------------|-----------|
| HR | | | | |
| Texas Department of Transportation | | | | |
| CAPITAL EXPRESS | | | | |
| BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES (SHEET 9 OF 28) | | | | |
| SCALE: N. T. S. | | | PROJECT NO. | |
| DWN: TH | STATE | CKD: HH | FED. RD. DISTRICT | COUNTY |
| | TEXAS | | 14 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 9 |

BUILD CONFIGURATION



MATCH TO SHEET 9

MATCH TO SHEET 11

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE

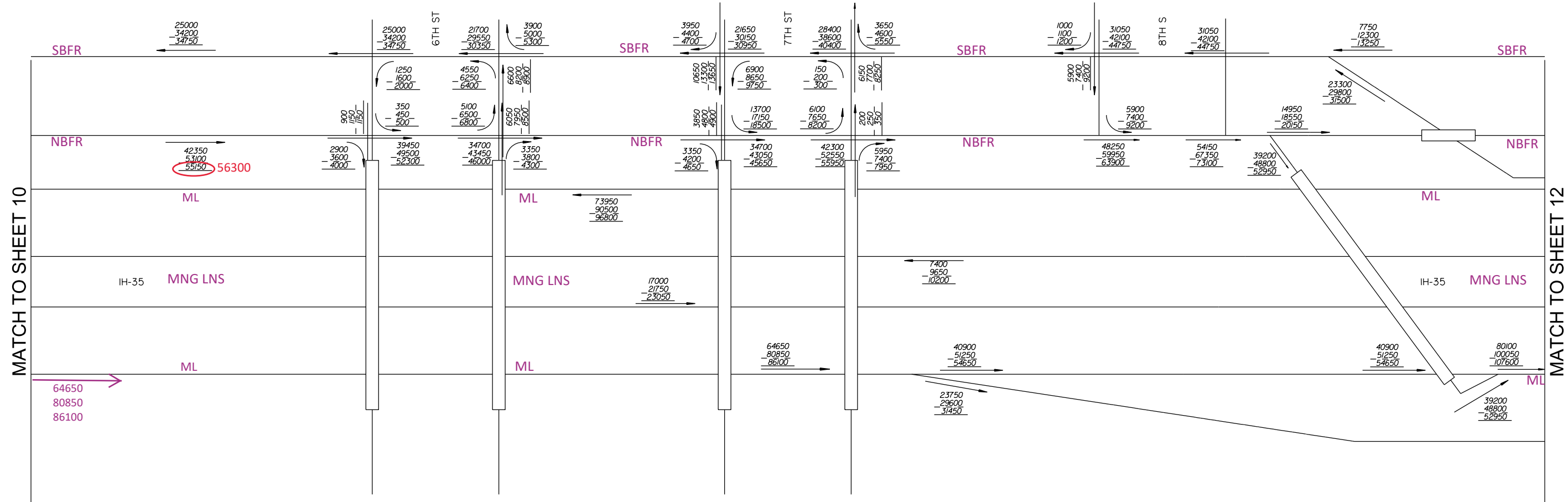
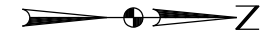


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 10 OF 28)

| | | | | |
|-----------------|----------------|-------------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 10 |

BUILD CONFIGURATION



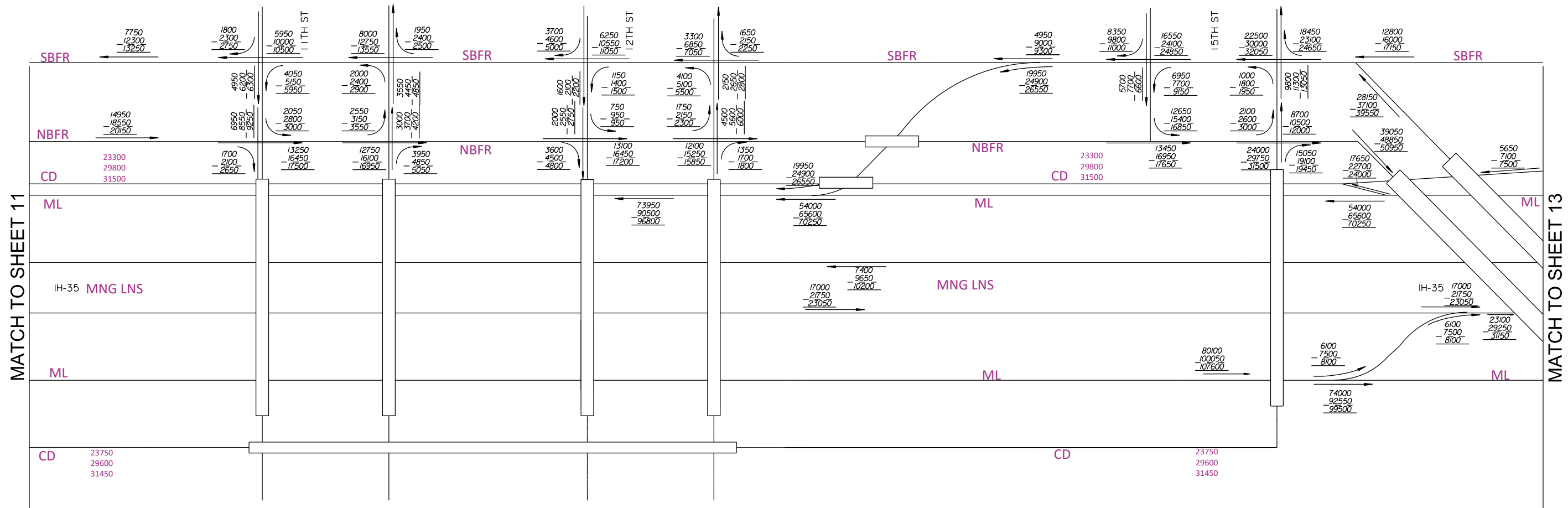
2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|------------------------------------|----------------|-------------------|-------------|-----------|
| HR | | | | |
| Texas Department of Transportation | | | | |
| CAPITAL EXPRESS | | | | |
| BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES | | | | |
| (SHEET 11 OF 28) | | | | |
| SCALE : N. T. S. | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 11 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE

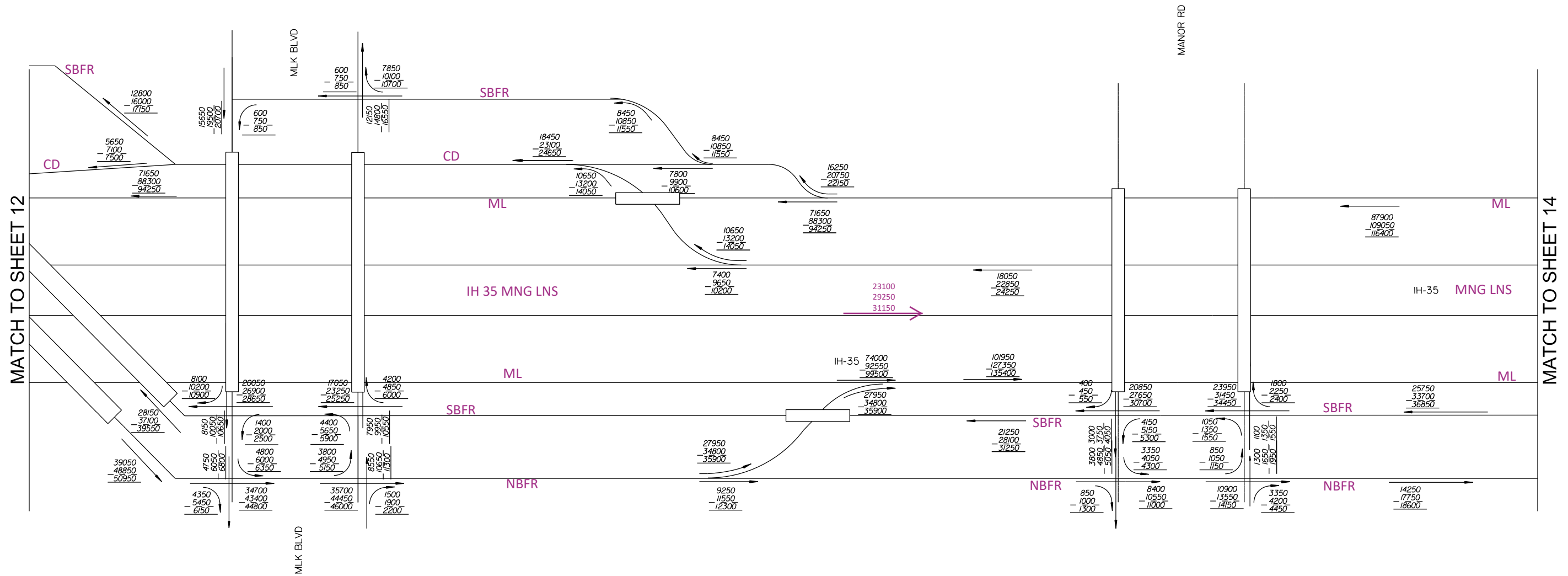
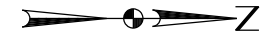


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 12 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 12 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE

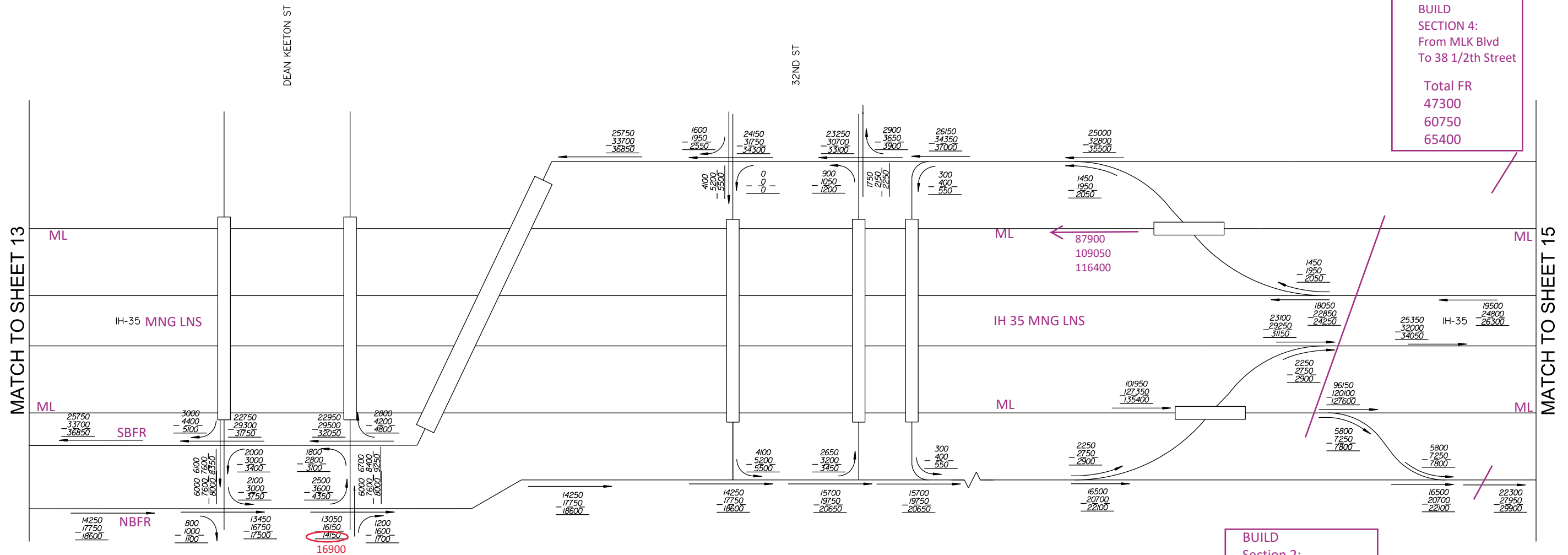
| | | | | |
|------------------------------------|----------------|---------------|----------|-----------|
| HR | | | | |
| Texas Department of Transportation | | | | |
| CAPITAL EXPRESS | | | | |
| BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES | | | | |
| (SHEET 13 OF 28) | | | | |
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 13 |

BUILD CONFIGURATION



BUILD SECTION 4:
From MLK Blvd
To 38 1/2th Street

Total FR
47300
60750
65400



BUILD Section 2:
From MLK Blvd
To St. Johns Ave

ML+Managed Lanes
234700
293200
312150

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
→ TRAVEL DIRECTION

NOT TO SCALE



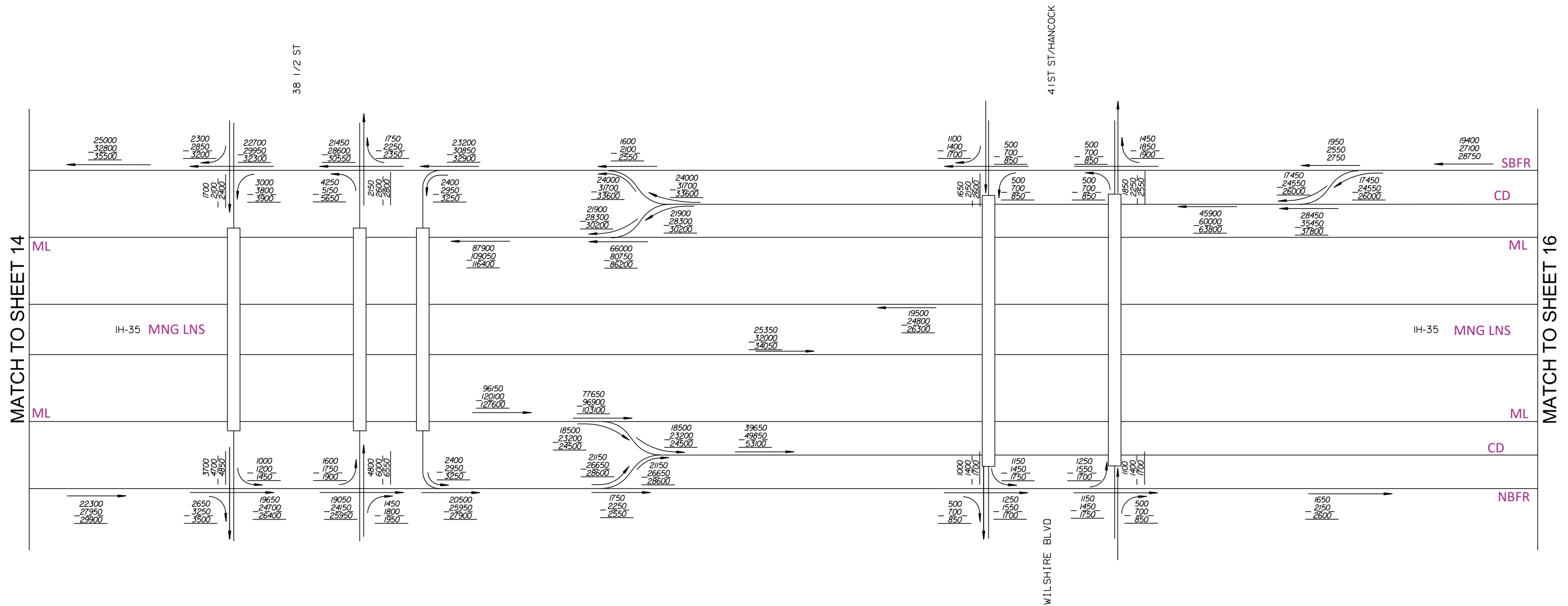
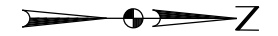
Texas Department of Transportation

CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 14 OF 28)

| | | | |
|-----------------|----------------|-------------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 14 |


BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE



Texas Department of Transportation

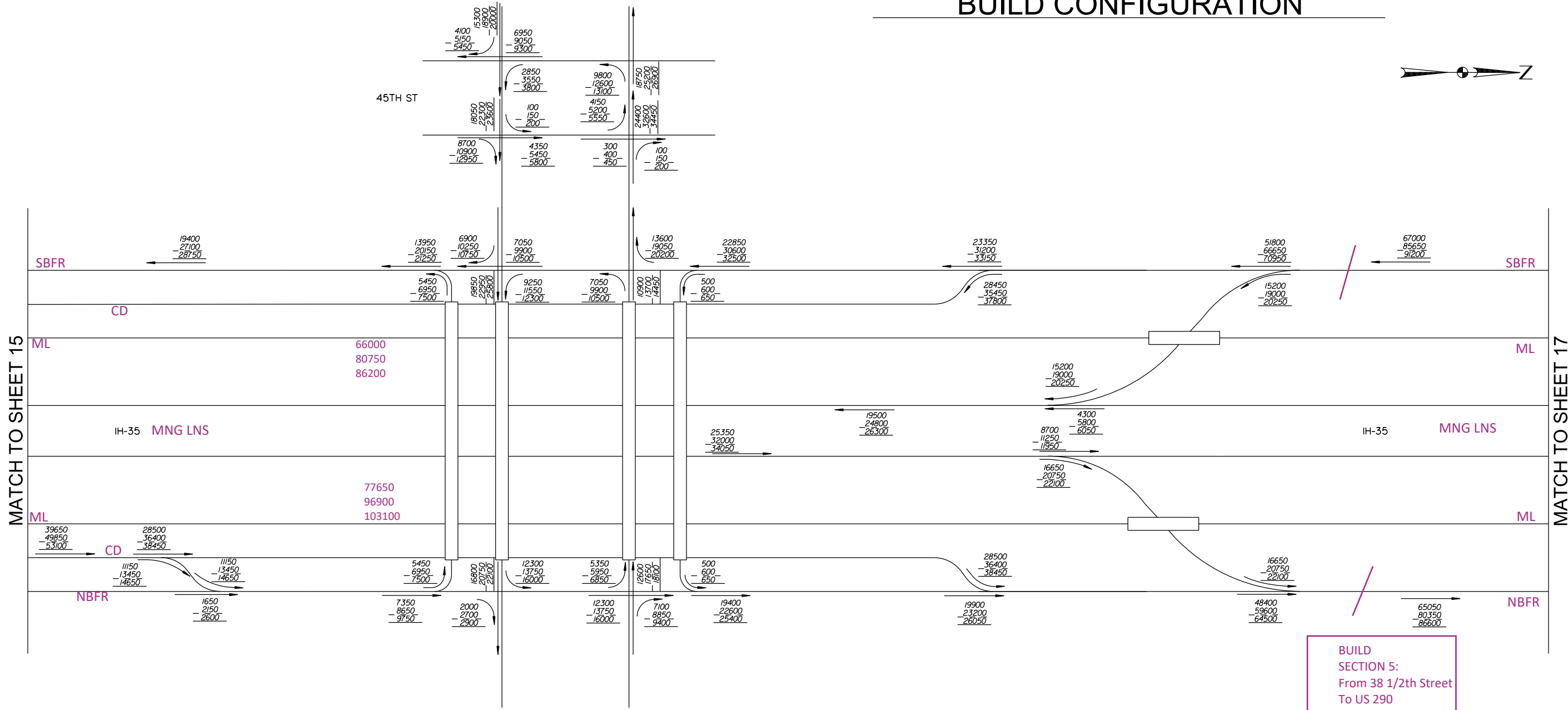
CAPITAL EXPRESS
BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 15 OF 28)

SCALE: N. T. S. PROJECT NO.

| | | | |
|---------|----------------|-------------------|--------------------|
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 15 |

BUILD CONFIGURATION



MATCH TO SHEET 15

MATCH TO SHEET 17

AIRPORT BLVD

BUILD SECTION 5:
From 38 1/2th Street
To US 290

Total FR
132050
166000
177800

NOT TO SCALE



Texas Department of Transportation

CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 16 OF 28)

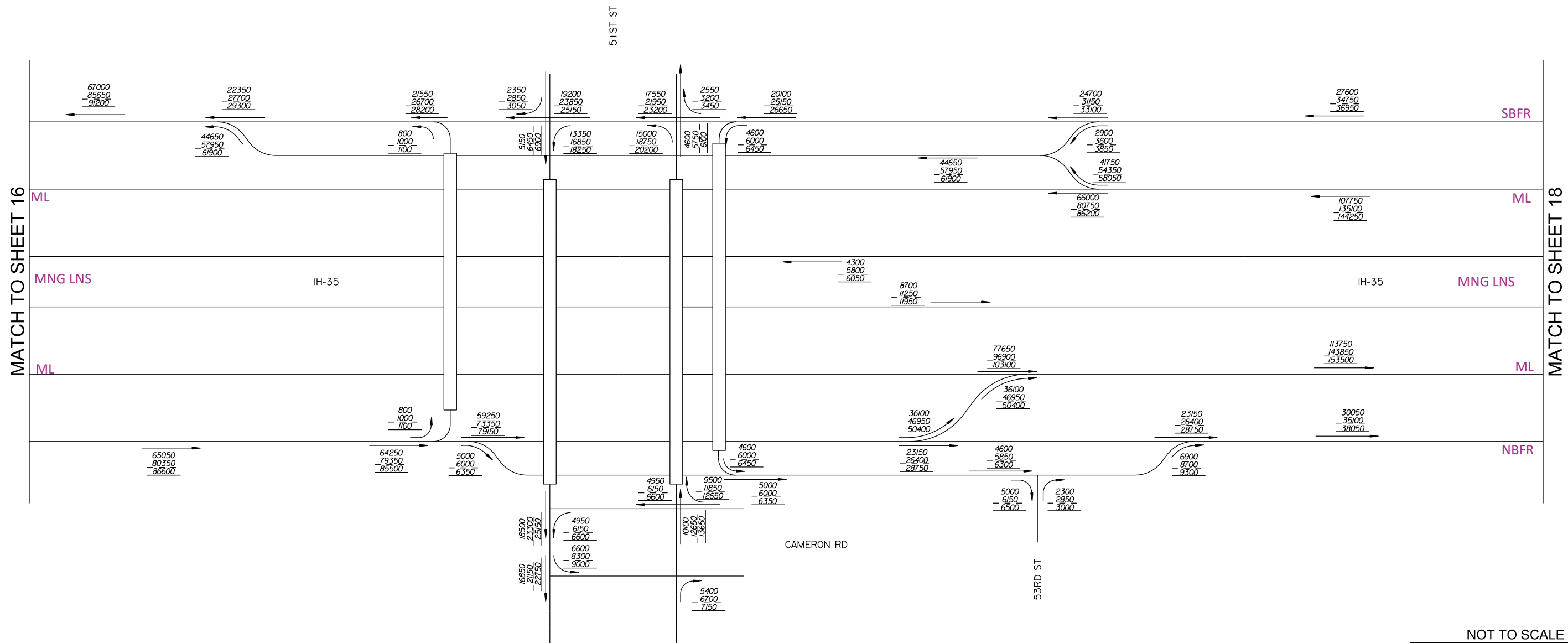
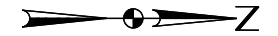
| | | | |
|------------------|---------|----------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE DISTRICT | FED. RD. DIV. NO. |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

NOT TO SCALE

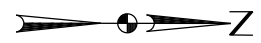
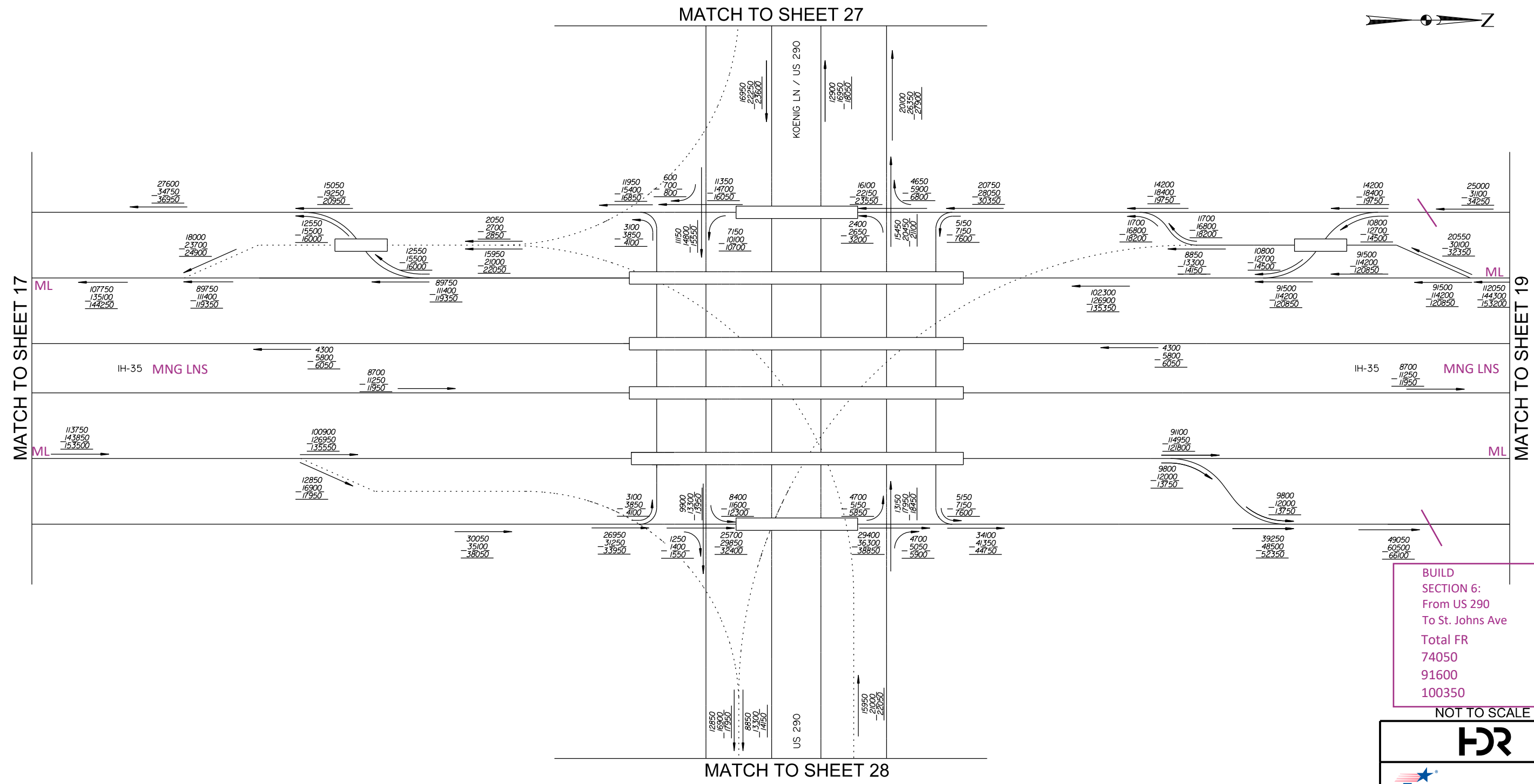


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 17 OF 28)

| | | | | | |
|------------------|----------------|---------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 17 | |

BUILD CONFIGURATION




BUILD SECTION 6:
 From US 290
 To St. Johns Ave
 Total FR
 74050
 91600
 100350


NOT TO SCALE

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION



HR

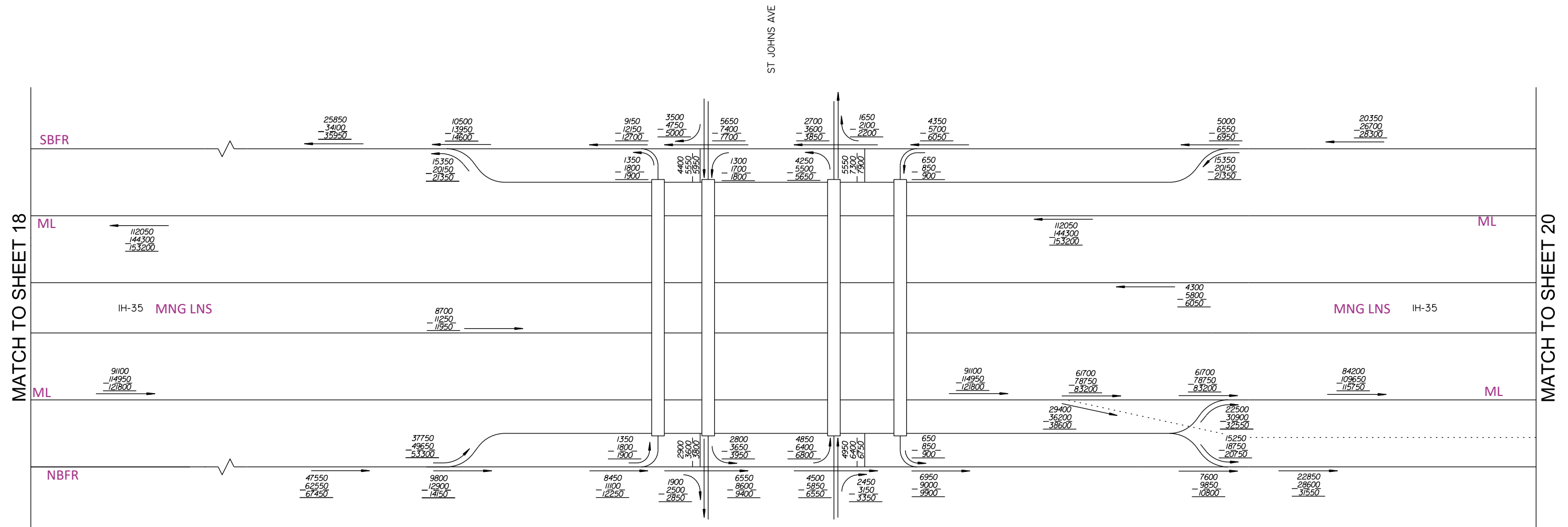


CAPITAL EXPRESS
 BUILD CONFIGURATION

24 HOUR VOLUMES
 (SHEET 18 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

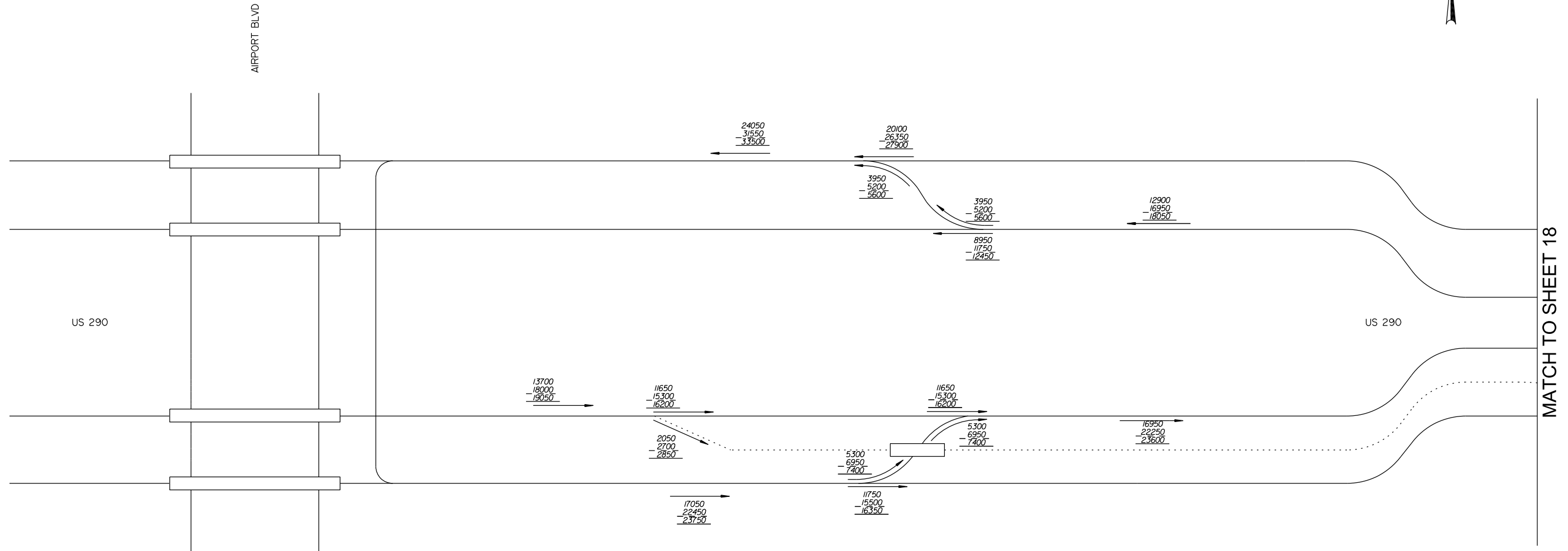


CAPITAL EXPRESS
 BUILD CONFIGURATION

24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | | |
|-----------------|----------------|-------------------|-------------|-----------|
| SCALE: N. T. S. | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 19 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE

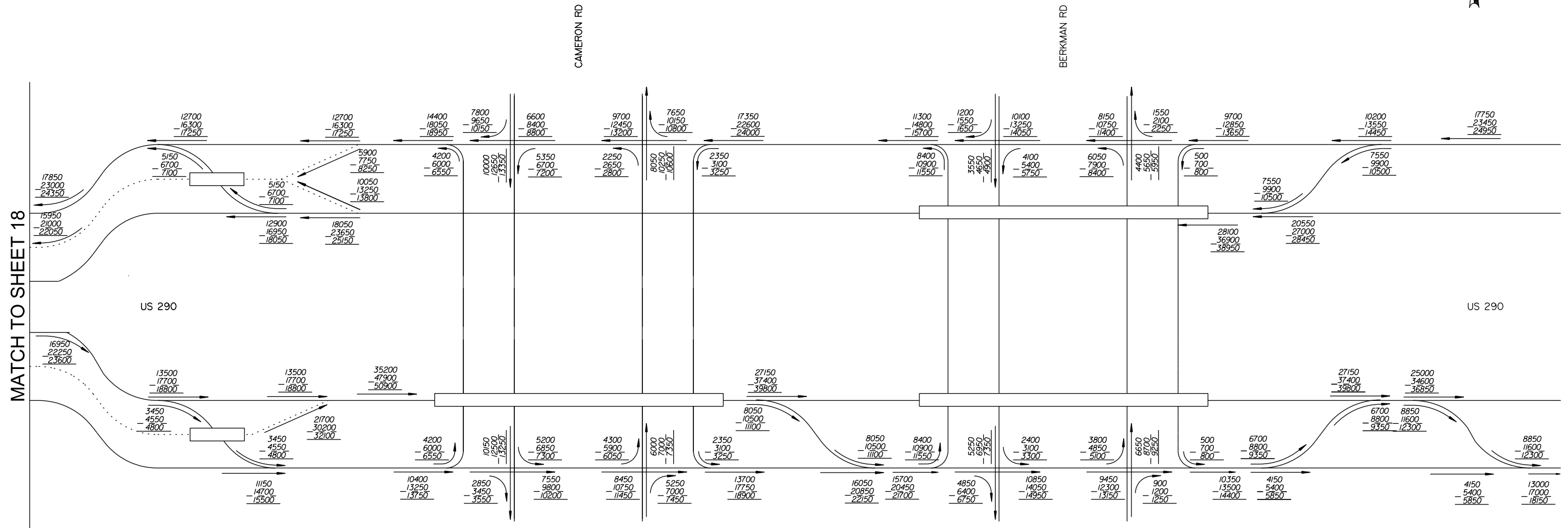


CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 27 OF 28)

| | | | | |
|-----------------|----------------|-------------------|----------|-----------|
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 27 |

BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- TRAVEL DIRECTION

NOT TO SCALE



CAPITAL EXPRESS BUILD CONFIGURATION

24 HOUR VOLUMES
(SHEET 28 OF 28)

| | | | | | |
|------------------|----------------|-------------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 28 | |

APPENDIX D
Analysis Tables

| BASE - 2023 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | | | Inputs Peak | | | | | Rates Peak | | | | | Totals | | | | | | | | | |
|--------------|--------|----------------|----------------|---------------|-------------|---------------|---------|---------|---------|---------|---------|----------|---------|---------|----------|------------|----------|-------------|--------|---------|---------|--------|------------|---------|---------|--------|---------|---------|-------|------|-------|-------|-------|-------|--------|--------|------|
| Link Name | Length | 24 Hr ADT 2023 | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | |
| I35 ML NB 1 | 0.27 | 61369 | 16474 | 60 | 51141 | 13728 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 11 | 10228 | 2746 | 0.0024 | 0.00026 | 0.00014 | 0.0027 | 0.0017 | 0.00021 | 0.0018 | 0.014 | 0.00011 | 16.92 | 1.78 | 1.00 | 17.72 | 11.38 | 1.37 | 11.30 | 100.92 | 0.75 | |
| I35 ML NB 2 | 0.65 | 70683 | 45957 | 60 | 58903 | 38298 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 15 | 11781 | 7660 | 0.0020 | 0.00021 | 0.00012 | 0.0021 | 0.0014 | 0.00016 | 0.0018 | 0.013 | 0.00009 | 44.37 | 4.57 | 2.61 | 45.23 | 29.08 | 3.47 | 28.71 | 272.48 | 1.95 | |
| I35 ML NB 3 | 0.27 | 90049 | 24208 | 60 | 75040 | 20173 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 11 | 15008 | 4035 | 0.0024 | 0.00026 | 0.00014 | 0.0027 | 0.0017 | 0.00021 | 0.0018 | 0.014 | 0.00011 | 24.86 | 2.62 | 1.46 | 26.04 | 16.72 | 2.01 | 16.60 | 148.29 | 1.11 | |
| I35 ML NB 4 | 0.35 | 67871 | 23945 | 60 | 56559 | 19954 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 13 | 11312 | 3991 | 0.0022 | 0.00023 | 0.00013 | 0.0023 | 0.0015 | 0.00018 | 0.0016 | 0.013 | 0.00009 | 23.74 | 2.47 | 1.40 | 24.49 | 15.79 | 1.89 | 15.58 | 143.96 | 1.05 | |
| I35 ML NB 5 | 0.14 | 80873 | 11085 | 60 | 67394 | 9238 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 9 | 13479 | 1848 | 0.0027 | 0.00030 | 0.00016 | 0.0031 | 0.0020 | 0.00024 | 0.0021 | 0.015 | 0.00012 | 11.93 | 1.28 | 0.70 | 12.75 | 8.19 | 0.89 | 8.16 | 70.39 | 0.54 | |
| I35 ML NB 6 | 0.53 | 71974 | 37804 | 60 | 59979 | 31504 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 2.5 | 11996 | 6301 | 0.0067 | 0.00039 | 0.00019 | 0.0059 | 0.00091 | 0.00059 | 0.00074 | 0.0063 | 0.041 | 0.00035 | 66.14 | 7.90 | 3.89 | 81.11 | 52.61 | 6.47 | 54.44 | 402.87 | 3.29 |
| I35 ML NB 7 | 0.27 | 88020 | 24043 | 60 | 73350 | 20036 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 9 | 14670 | 4007 | 0.0027 | 0.00030 | 0.00016 | 0.0031 | 0.0020 | 0.00024 | 0.0021 | 0.015 | 0.00012 | 25.88 | 2.77 | 1.53 | 27.66 | 17.76 | 2.14 | 17.69 | 152.67 | 1.16 | |
| I35 ML NB 8 | 0.37 | 78060 | 29233 | 60 | 65050 | 24361 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 12 | 13010 | 4872 | 0.0022 | 0.00024 | 0.00013 | 0.0025 | 0.0016 | 0.00019 | 0.0017 | 0.013 | 0.00010 | 29.46 | 3.08 | 1.74 | 30.61 | 19.66 | 2.36 | 19.49 | 177.28 | 1.31 | |
| I35 ML NB 9 | 0.39 | 66626 | 26166 | 60 | 55521 | 21804 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 12 | 11104 | 4361 | 0.0022 | 0.00024 | 0.00013 | 0.0025 | 0.0016 | 0.00019 | 0.0017 | 0.013 | 0.00010 | 26.37 | 2.76 | 1.55 | 27.40 | 17.60 | 2.11 | 17.44 | 158.68 | 1.17 | |
| I35 ML NB 10 | 0.26 | 89726 | 23620 | 60 | 74771 | 19684 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 6 | 14954 | 3937 | 0.0035 | 0.00042 | 0.00020 | 0.0043 | 0.0028 | 0.00034 | 0.0029 | 0.020 | 0.00017 | 28.55 | 3.17 | 1.69 | 31.97 | 20.55 | 2.50 | 20.61 | 167.7 | 1.32 | |
| I35 ML NB 11 | 0.42 | 84977 | 35450 | 60 | 70814 | 29541 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 7 | 14163 | 5908 | 0.0031 | 0.00037 | 0.00018 | 0.0038 | 0.0025 | 0.00030 | 0.0026 | 0.018 | 0.00015 | 40.84 | 4.47 | 2.41 | 44.89 | 28.85 | 3.49 | 28.86 | 240.27 | 1.87 | |
| I35 ML NB 12 | 0.02 | 86203 | 1735 | 60 | 71836 | 1446 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 5 | 14367 | 289 | 0.0039 | 0.00049 | 0.00023 | 0.0051 | 0.0033 | 0.00040 | 0.0034 | 0.022 | 0.00019 | 2.23 | 0.25 | 0.13 | 2.56 | 1.65 | 0.20 | 1.66 | 13.10 | 0.10 | |
| I35 ML NB 13 | 0.46 | 90002 | 41179 | 60 | 75002 | 34316 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 7 | 15000 | 6863 | 0.0031 | 0.00037 | 0.00018 | 0.0038 | 0.0025 | 0.00030 | 0.0026 | 0.018 | 0.00015 | 47.44 | 5.20 | 2.80 | 52.15 | 33.51 | 4.06 | 33.52 | 279.09 | 2.17 | |
| I35 ML NB 14 | 0.11 | 106970 | 11490 | 60 | 89142 | 9575 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 6 | 17828 | 1915 | 0.0035 | 0.00042 | 0.00020 | 0.0043 | 0.0028 | 0.00034 | 0.0029 | 0.020 | 0.00017 | 13.89 | 1.54 | 0.82 | 15.55 | 10.00 | 1.21 | 10.03 | 81.56 | 0.64 | |
| I35 ML NB 15 | 0.31 | 94659 | 29128 | 60 | 78883 | 24273 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 9 | 15777 | 4855 | 0.0027 | 0.00030 | 0.00016 | 0.0031 | 0.0020 | 0.00024 | 0.0021 | 0.015 | 0.00012 | 31.36 | 3.36 | 1.85 | 33.51 | 21.52 | 2.59 | 21.43 | 184.95 | 1.41 | |
| I35 ML NB 16 | 0.18 | 105288 | 18736 | 60 | 87740 | 15614 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 8 | 17548 | 3123 | 0.0029 | 0.00033 | 0.00017 | 0.0034 | 0.0022 | 0.00027 | 0.0023 | 0.016 | 0.00013 | 20.79 | 2.25 | 1.23 | 22.51 | 14.46 | 1.75 | 14.43 | 122.48 | 0.94 | |
| I35 ML NB 17 | 0.29 | 40575 | 11704 | 60 | 33812 | 9754 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 5 | 6762 | 1951 | 0.0039 | 0.00049 | 0.00023 | 0.0051 | 0.0033 | 0.00040 | 0.0034 | 0.022 | 0.00019 | 15.08 | 1.71 | 0.89 | 17.26 | 11.10 | 1.35 | 11.17 | 88.34 | 0.71 | |
| I35 ML NB 18 | 0.24 | 63767 | 15443 | 60 | 53139 | 12869 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 33 | 10628 | 2574 | 0.0011 | 0.00011 | 0.00007 | 0.0011 | 0.0008 | 0.00009 | 0.0007 | 0.008 | 0.00005 | 12.68 | 1.29 | 0.75 | 12.73 | 8.16 | 0.97 | 7.90 | 80.50 | 0.56 | |
| I35 ML NB 19 | 0.26 | 61462 | 15984 | 60 | 51218 | 13320 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 28 | 10244 | 2664 | 0.0013 | 0.00013 | 0.00007 | 0.0013 | 0.0009 | 0.00010 | 0.0009 | 0.010 | 0.00006 | 13.48 | 1.38 | 0.80 | 13.56 | 8.72 | 1.04 | 8.46 | 87.38 | 0.60 | |
| I35 ML NB 20 | 1.37 | 54914 | 75208 | 60 | 45762 | 62674 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 8 | 9152 | 12534 | 0.0029 | 0.00033 | 0.00017 | 0.0034 | 0.0022 | 0.00027 | 0.0023 | 0.016 | 0.00013 | 83.45 | 9.03 | 4.92 | 90.34 | 58.03 | 7.01 | 57.91 | 491.62 | 3.78 | |
| I35 ML NB 21 | 0.49 | 54638 | 26539 | 60 | 45531 | 22116 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 19 | 9106 | 4423 | 0.0016 | 0.00016 | 0.00010 | 0.0017 | 0.0011 | 0.00013 | 0.0012 | 0.011 | 0.00007 | 24.05 | 2.47 | 1.42 | 24.38 | 15.67 | 1.87 | 15.38 | 156.68 | 1.06 | |
| I35 ML NB 22 | 0.37 | 64781 | 23714 | 60 | 53985 | 19762 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 22 | 10797 | 3952 | 0.0015 | 0.00015 | 0.00009 | 0.0015 | 0.0010 | 0.00012 | 0.0010 | 0.011 | 0.00007 | 20.83 | 2.13 | 1.23 | 21.05 | 13.53 | 1.61 | 13.22 | 132.94 | 0.92 | |
| I35 ML NB 23 | 0.50 | 61001 | 30325 | 60 | 50834 | 25271 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 23 | 10167 | 5954 | 0.0015 | 0.00015 | 0.00008 | 0.0015 | 0.0010 | 0.00011 | 0.0010 | 0.010 | 0.00006 | 26.41 | 2.70 | 1.56 | 26.68 | 17.14 | 2.05 | 16.73 | 169.09 | 1.17 | |
| I35 ML NB 24 | 0.19 | 47537 | 9206 | 60 | 39614 | 7671 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 14 | 16998 | 5070 | 0.0021 | 0.00022 | 0.00012 | 0.0022 | 0.0014 | 0.00017 | 0.0015 | 0.013 | 0.00009 | 29.73 | 3.08 | 1.76 | 30.49 | 19.59 | 2.34 | 19.37 | 181.53 | 1.31 | |
| I35 ML NB 25 | 0.09 | 108538 | 10131 | 60 | 90448 | 8443 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 18 | 18090 | 1689 | 0.0021 | 0.00022 | 0.00012 | 0.0022 | 0.0014 | 0.00017 | 0.0015 | 0.013 | 0.00009 | 9.90 | 1.03 | 0.58 | 10.15 | 6.53 | 0.78 | 6.45 | 60.46 | 0.44 | |
| I35 ML NB 26 | 0.30 | 101990 | 30420 | 60 | 84992 | 25350 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 14 | 16998 | 5070 | 0.0021 | 0.00022 | 0.00012 | 0.0022 | 0.0014 | 0.00017 | 0.0015 | 0.013 | 0.00009 | 29.73 | 3.08 | 1.76 | 30.49 | 19.59 | 2.34 | 19.37 | 181.53 | 1.31 | |
| I35 ML NB 27 | 0.25 | 121678 | 30495 | 60 | 101399 | 25413 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 14 | 20280 | 5083 | 0.0021 | 0.00022 | 0.00012 | 0.0022 | 0.0014 | 0.00017 | 0.0015 | 0.013 | 0.00009 | 29.81 | 3.09 | 1.76 | 30.56 | 19.64 | 2.35 | 19.42 | 181.98 | 1.32 | |
| I35 ML NB 28 | 0.46 | 112918 | 51633 | 60 | 94098 | 43027 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 18 | 18280 | 6065 | 0.0017 | 0.00018 | 0.00010 | 0.0018 | 0.0012 | 0.00014 | 0.0012 | 0.012 | 0.00007 | 47.43 | 4.87 | 2.80 | 48.14 | 30.93 | 3.69 | 30.41 | 297.41 | 2.04 | |
| I35 ML NB 29 | 0.41 | 101068 | 41381 | 60 | 84224 | 34484 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 13 | 16845 | 6897 | 0.0022 | 0.00023 | 0.00013 | 0.0023 | 0.0015 | 0.00018 | 0.0016 | 0.013 | 0.00009 | 41.03 | 4.27 | 2.42 | 42.33 | 27.20 | 3.26 | 26.92 | 248.79 | 1.82 | |
| I35 ML NB 30 | 0.51 | 92031 | 46568 | 60 | 76693 | 38807 | 0.00076 | 0.00078 | 0.00045 | 0.00076 | 0.00048 | 0.000058 | 0.00046 | 0.00046 | 0.000034 | 13 | 15339 | 7762 | 0.0022 | 0.00023 | 0.00013 | 0.0023 | 0.0015 | 0.00018 | 0.0016 | 0.013 | 0.00009 | 46.17 | 4.80 | 2.72 | 47.64 | 30.61 | 3. | | | | |

| INTERIM - 2032 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | | | Totals | | | | | | | | | | | |
|----------------|--------|--------------------|----------|----------------|-------------|-------------|---------------|----------|----------|---------|----------|----------|---------|---------|----------|------------|----------|----------|-------------|----------|----------|------------|---------|---------|---------|---------|----------|----------|-------|------|-------|-------|-------|--------|--------|--------|------|--|--|--|--|--|--|--|--|
| Link Name | Length | 24HR ADT 2032 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | | | | | | | | |
| I35_ML_NB_1 | 0.27 | 68030 | 18262 | 60 | 56692 | 15218 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 6 | 11338 | 3044 | 0.00017 | 0.000092 | 0.000007 | 0.00014 | 0.00014 | 0.00013 | 0.00019 | 0.00076 | 0.000036 | 10.76 | 0.58 | 0.04 | 7.79 | 7.43 | 0.72 | 9.92 | 49.60 | 0.24 | | | | | | | | | |
| I35_ML_NB_2 | 0.65 | 68030 | 44232 | 60 | 56692 | 36860 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 11 | 11338 | 7372 | 0.00017 | 0.000060 | 0.000004 | 0.00018 | 0.00008 | 0.00008 | 0.00011 | 0.00055 | 0.000027 | 21.80 | 1.16 | 0.08 | 15.04 | 13.94 | 1.36 | 18.17 | 104.50 | 0.49 | | | | | | | | | |
| I35_ML_NB_3 | 0.27 | 99822 | 26835 | 60 | 83185 | 22363 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 8 | 16637 | 4473 | 0.00014 | 0.000075 | 0.000006 | 0.00011 | 0.00011 | 0.00010 | 0.00015 | 0.00064 | 0.000029 | 14.40 | 0.77 | 0.05 | 10.17 | 9.56 | 0.93 | 12.62 | 67.40 | 0.32 | | | | | | | | | |
| I35_ML_NB_4 | 0.35 | 75237 | 26543 | 60 | 62697 | 22119 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 7 | 12539 | 4424 | 0.00015 | 0.000082 | 0.000006 | 0.00012 | 0.00012 | 0.00012 | 0.00015 | 0.00069 | 0.000032 | 14.84 | 0.79 | 0.05 | 10.60 | 10.03 | 0.98 | 13.23 | 68.99 | 0.33 | | | | | | | | | |
| I35_ML_NB_5 | 0.14 | 89651 | 12288 | 60 | 74709 | 10240 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 7 | 14942 | 2048 | 0.00015 | 0.000082 | 0.000006 | 0.00012 | 0.00012 | 0.00012 | 0.00017 | 0.00069 | 0.000032 | 6.87 | 0.37 | 0.03 | 4.91 | 4.64 | 0.45 | 6.17 | 31.94 | 0.15 | | | | | | | | | |
| I35_ML_NB_6 | 0.53 | 79786 | 41907 | 60 | 66488 | 34922 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 10 | 13298 | 6985 | 0.00012 | 0.000064 | 0.000005 | 0.00019 | 0.00019 | 0.00019 | 0.00012 | 0.00057 | 0.000025 | 21.17 | 1.13 | 0.07 | 14.69 | 13.65 | 1.33 | 17.89 | 100.13 | 0.47 | | | | | | | | | |
| I35_ML_NB_7 | 0.27 | 97573 | 26653 | 60 | 81311 | 22211 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 9 | 16262 | 4442 | 0.00013 | 0.000069 | 0.000005 | 0.00019 | 0.00019 | 0.00019 | 0.00012 | 0.00057 | 0.000027 | 13.84 | 0.74 | 0.05 | 9.68 | 9.04 | 0.88 | 11.89 | 65.13 | 0.31 | | | | | | | | | |
| I35_ML_NB_8 | 0.37 | 86533 | 32406 | 60 | 72111 | 27005 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 16 | 14422 | 5401 | 0.00009 | 0.000047 | 0.000003 | 0.00016 | 0.00016 | 0.00016 | 0.00006 | 0.00008 | 0.000049 | 0.000018 | 14.64 | 0.78 | 0.05 | 9.92 | 9.07 | 0.89 | 11.65 | 73.38 | 0.33 | | | | | | | | |
| I35_ML_NB_9 | 0.39 | 73857 | 29005 | 60 | 61547 | 24171 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 16 | 12309 | 4834 | 0.00009 | 0.000047 | 0.000003 | 0.00016 | 0.00016 | 0.00016 | 0.00006 | 0.00008 | 0.000049 | 0.000018 | 11.11 | 0.70 | 0.04 | 8.88 | 8.17 | 0.79 | 10.43 | 65.68 | 0.29 | | | | | | | | |
| I35_ML_NB_10 | 0.26 | 99464 | 26184 | 60 | 82887 | 21820 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 16 | 16577 | 4364 | 0.00009 | 0.000047 | 0.000003 | 0.00016 | 0.00016 | 0.00016 | 0.00006 | 0.00008 | 0.000049 | 0.000018 | 11.83 | 0.63 | 0.04 | 8.01 | 7.33 | 0.72 | 9.41 | 59.29 | 0.27 | | | | | | | | |
| I35_ML_NB_11 | 0.42 | 94200 | 39297 | 60 | 78500 | 32748 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 20 | 15700 | 6550 | 0.00007 | 0.000039 | 0.000003 | 0.00015 | 0.00015 | 0.00015 | 0.00005 | 0.00007 | 0.000044 | 0.000015 | 16.81 | 0.89 | 0.06 | 11.27 | 10.24 | 1.00 | 13.13 | 85.83 | 0.38 | | | | | | | | |
| I35_ML_NB_12 | 0.02 | 95559 | 1923 | 60 | 79633 | 1603 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 19 | 15927 | 321 | 0.00008 | 0.000040 | 0.000003 | 0.00015 | 0.00015 | 0.00015 | 0.00005 | 0.00007 | 0.000045 | 0.000016 | 0.83 | 0.04 | 0.00 | 0.56 | 0.51 | 0.05 | 0.65 | 4.23 | 0.02 | | | | | | | | |
| I35_ML_NB_13 | 0.46 | 99771 | 45648 | 60 | 83142 | 38040 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 26 | 16628 | 7608 | 0.00006 | 0.000033 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000041 | 0.000015 | 18.62 | 0.94 | 0.06 | 12.44 | 11.25 | 1.10 | 14.26 | 96.78 | 0.43 | | | | | | | | |
| I35_ML_NB_14 | 0.11 | 118580 | 12737 | 60 | 98817 | 10614 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 23 | 19763 | 2123 | 0.00007 | 0.000035 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000042 | 0.000014 | 5.30 | 0.28 | 0.02 | 3.55 | 3.21 | 0.31 | 4.10 | 27.35 | 0.12 | | | | | | | | |
| I35_ML_NB_15 | 0.31 | 104933 | 32289 | 60 | 87444 | 26908 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 31 | 17489 | 5382 | 0.00005 | 0.000029 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000037 | 0.000012 | 12.83 | 0.68 | 0.04 | 8.55 | 7.71 | 0.75 | 9.71 | 66.48 | 0.30 | | | | | | | | |
| I35_ML_NB_16 | 0.18 | 116715 | 20770 | 60 | 97263 | 17308 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 25 | 19453 | 3462 | 0.00006 | 0.000033 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000041 | 0.000014 | 8.52 | 0.45 | 0.03 | 5.69 | 5.15 | 0.50 | 6.54 | 44.20 | 0.19 | | | | | | | | |
| I35_ML_NB_17 | 0.29 | 44979 | 12975 | 60 | 37482 | 10812 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 21 | 7496 | 2162 | 0.00007 | 0.000038 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00005 | 0.00005 | 0.000044 | 0.000015 | 5.50 | 0.29 | 0.02 | 3.68 | 3.34 | 0.33 | 4.28 | 28.16 | 0.12 | | | | | | | | |
| I35_ML_NB_18 | 0.24 | 70688 | 17119 | 60 | 58907 | 14266 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 48 | 11781 | 2853 | 0.00004 | 0.000022 | 0.000001 | 0.00013 | 0.00013 | 0.00013 | 0.00003 | 0.00003 | 0.000023 | 0.000010 | 6.42 | 0.34 | 0.02 | 4.22 | 3.76 | 0.37 | 4.74 | 31.41 | 0.15 | | | | | | | | |
| I35_ML_NB_19 | 0.26 | 68132 | 17179 | 60 | 56777 | 14766 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 44 | 11355 | 2953 | 0.00004 | 0.000023 | 0.000001 | 0.00013 | 0.00013 | 0.00013 | 0.00003 | 0.00003 | 0.000026 | 0.000010 | 6.71 | 0.36 | 0.02 | 4.42 | 3.95 | 0.39 | 4.97 | 33.20 | 0.16 | | | | | | | | |
| I35_ML_NB_20 | 1.37 | 60874 | 83371 | 60 | 50729 | 69476 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 28 | 10146 | 13996 | 0.00006 | 0.000031 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000040 | 0.000013 | 33.64 | 1.79 | 0.11 | 22.47 | 20.33 | 1.99 | 25.63 | 175.67 | 0.77 | | | | | | | | |
| I35_ML_NB_21 | 0.49 | 60685 | 29419 | 60 | 50473 | 24516 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 32 | 10095 | 4903 | 0.00005 | 0.000029 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000035 | 0.000012 | 11.64 | 0.62 | 0.04 | 7.73 | 6.95 | 0.68 | 8.78 | 59.60 | 0.27 | | | | | | | | |
| I35_ML_NB_22 | 0.37 | 71812 | 26288 | 60 | 59844 | 21906 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 29 | 11969 | 4381 | 0.00006 | 0.000031 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000039 | 0.000013 | 10.55 | 0.56 | 0.03 | 7.05 | 6.38 | 0.62 | 8.02 | 55.21 | 0.24 | | | | | | | | |
| I35_ML_NB_23 | 0.50 | 67621 | 33617 | 60 | 56351 | 28014 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 28 | 11270 | 5603 | 0.00006 | 0.000031 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000040 | 0.000013 | 13.56 | 0.72 | 0.04 | 9.06 | 8.20 | 0.80 | 10.33 | 70.81 | 0.31 | | | | | | | | |
| I35_ML_NB_24 | 0.19 | 52697 | 10205 | 60 | 43914 | 8504 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 28 | 8783 | 1701 | 0.00006 | 0.000031 | 0.000002 | 0.00014 | 0.00014 | 0.00014 | 0.00004 | 0.00005 | 0.000040 | 0.000013 | 4.12 | 0.22 | 0.01 | 2.75 | 2.49 | 0.24 | 3.14 | 21.49 | 0.09 | | | | | | | | |
| I35_ML_NB_25 | 0.09 | 120318 | 11231 | 60 | 100265 | 9359 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 25 | 20053 | 1872 | 0.00006 | 0.000033 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000041 | 0.000014 | 4.61 | 0.24 | 0.02 | 3.08 | 2.79 | 0.27 | 3.54 | 23.90 | 0.11 | | | | | | | | |
| I35_ML_NB_26 | 0.30 | 113060 | 33722 | 60 | 94217 | 28102 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 25 | 18843 | 5620 | 0.00006 | 0.000033 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000041 | 0.000014 | 13.84 | 0.73 | 0.05 | 9.24 | 8.36 | 0.82 | 10.62 | 71.76 | 0.32 | | | | | | | | |
| I35_ML_NB_27 | 0.25 | 134885 | 33805 | 60 | 112404 | 28171 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 24 | 22481 | 5634 | 0.00006 | 0.000034 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000042 | 0.000014 | 13.97 | 0.74 | 0.05 | 9.34 | 8.45 | 0.83 | 10.76 | 72.25 | 0.32 | | | | | | | | |
| I35_ML_NB_28 | 0.46 | 125173 | 57236 | 60 | 104311 | 47697 | 0.00037 | 0.000019 | 0.000001 | 0.00024 | 0.000021 | 0.000021 | 0.00027 | 0.00017 | 0.000009 | 25 | 20862 | 9539 | 0.00006 | 0.000033 | 0.000002 | 0.00015 | 0.00015 | 0.00015 | 0.00004 | 0.00005 | 0.000041 | 0.000014 | 23.49 | 1.25 | 0.08 | 15.69 | 14.20 | 1.39 | 18.03 | 121.80 | 0.54 | | | | | | | | |
| I35_ML_NB_29 | 0.41 | 112038 | 45872 | 60 | 93365 | 38227 | 0.00037 | 0.000019 | 0.000001 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| INTERIM - 2032 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | Totals | | | | | | | |
|-----------------|--------|-----------------------|-------------|------------------|----------------|----------------|---------------|----------|----------|---------|---------|----------|---------|--------|----------|---------------|-------------|-------------|---------|-------------|----------|--------|------------|---------|---------|---------|----------|------|-------|------|--------|------|-------|------|-------|------|--|--|
| Link Name | Length | 24HR ADT 2032 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | |
| I35_Frmtg_NB_47 | 0.34 | 50584 | 17047 | 45 | 42153 | 14206 | 0.00048 | 0.000022 | 0.000001 | 0.00022 | 0.00016 | 0.000016 | 0.00034 | 0.0010 | 0.000010 | 16 | 8431 | 2841 | 0.00010 | 0.000044 | 0.000002 | 0.0005 | 0.0004 | 0.00004 | 0.00008 | 0.00020 | 0.000019 | 9.76 | 0.44 | 0.02 | 4.45 | 3.23 | 0.33 | 7.14 | 19.94 | 0.19 | | |
| I35_Rmp_NB_1 | 0.25 | 10325 | 2536 | 50 | 8604 | 2113 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 40 | 1721 | 423 | 0.0005 | 0.000025 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00008 | 0.00027 | 0.000010 | 1.05 | 0.06 | 0.00 | 0.72 | 0.66 | 0.06 | 0.81 | 5.84 | 0.02 | | |
| I35_Rmp_NB_2 | 0.49 | 14414 | 7074 | 50 | 12011 | 5895 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 10 | 2402 | 1179 | 0.00012 | 0.000064 | 0.000005 | 0.0009 | 0.0009 | 0.00009 | 0.00012 | 0.00057 | 0.000025 | 3.79 | 0.20 | 0.01 | 2.70 | 2.56 | 0.25 | 3.27 | 19.75 | 0.08 | | |
| I35_Rmp_NB_3 | 0.14 | 24585 | 3404 | 50 | 20487 | 2837 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 41 | 4097 | 567 | 0.0005 | 0.000024 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00008 | 0.00027 | 0.000010 | 1.40 | 0.08 | 0.00 | 0.96 | 0.89 | 0.09 | 1.09 | 7.81 | 0.03 | | |
| I35_Rmp_NB_4 | 0.22 | 9865 | 2172 | 50 | 8221 | 1810 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 26 | 1644 | 362 | 0.0006 | 0.000033 | 0.000002 | 0.0004 | 0.0004 | 0.00004 | 0.00005 | 0.00041 | 0.000013 | 0.95 | 0.05 | 0.00 | 0.66 | 0.61 | 0.06 | 0.76 | 5.48 | 0.02 | | |
| I35_Rmp_NB_5 | 0.17 | 17787 | 2959 | 50 | 14822 | 2466 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 7 | 2964 | 493 | 0.0015 | 0.000082 | 0.000006 | 0.0012 | 0.0012 | 0.00012 | 0.00017 | 0.00069 | 0.000032 | 1.74 | 0.09 | 0.01 | 1.27 | 1.22 | 0.12 | 1.59 | 8.88 | 0.04 | | |
| I35_Rmp_NB_6 | 0.13 | 11040 | 1383 | 50 | 9200 | 1152 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 14 | 1840 | 230 | 0.0010 | 0.000051 | 0.000004 | 0.0007 | 0.0007 | 0.00007 | 0.00007 | 0.00052 | 0.000020 | 0.69 | 0.04 | 0.00 | 0.48 | 0.45 | 0.04 | 0.57 | 3.74 | 0.02 | | |
| I35_Rmp_NB_7 | 0.10 | 8587 | 832 | 50 | 7156 | 694 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 15 | 1431 | 139 | 0.0009 | 0.000049 | 0.000003 | 0.0007 | 0.0007 | 0.00006 | 0.00009 | 0.00051 | 0.000019 | 0.41 | 0.02 | 0.00 | 0.29 | 0.27 | 0.03 | 0.34 | 2.24 | 0.01 | | |
| I35_Rmp_NB_8 | 0.12 | 21518 | 2519 | 50 | 17932 | 2099 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 38 | 3586 | 420 | 0.0005 | 0.000026 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00009 | 0.00004 | 0.00028 | 1.05 | 0.06 | 0.00 | 0.72 | 0.66 | 0.06 | 0.81 | 5.83 | 0.02 | | |
| I35_Rmp_NB_9 | 0.14 | 5265 | 727 | 50 | 4387 | 606 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 15 | 877 | 121 | 0.0009 | 0.000049 | 0.000003 | 0.0007 | 0.0007 | 0.00006 | 0.00009 | 0.00051 | 0.000019 | 0.36 | 0.02 | 0.00 | 0.25 | 0.23 | 0.02 | 0.29 | 1.96 | 0.01 | | |
| I35_Rmp_NB_10 | 0.18 | 13596 | 2438 | 50 | 11330 | 2031 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 23 | 2266 | 406 | 0.0007 | 0.000035 | 0.000002 | 0.0005 | 0.0005 | 0.00004 | 0.00006 | 0.00042 | 0.000014 | 1.09 | 0.06 | 0.00 | 0.76 | 0.70 | 0.07 | 0.87 | 6.22 | 0.02 | | |
| I35_Rmp_NB_11 | 0.11 | 8025 | 870 | 50 | 6687 | 725 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 13 | 1337 | 145 | 0.0010 | 0.000054 | 0.000004 | 0.0008 | 0.0007 | 0.00007 | 0.00010 | 0.00053 | 0.000021 | 0.44 | 0.02 | 0.00 | 0.31 | 0.29 | 0.03 | 0.37 | 2.37 | 0.01 | | |
| I35_Rmp_NB_12 | 0.13 | 18809 | 2391 | 50 | 15674 | 1992 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 37 | 3135 | 398 | 0.0005 | 0.000026 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00004 | 0.00029 | 0.000011 | 1.00 | 0.05 | 0.00 | 0.68 | 0.63 | 0.06 | 0.78 | 5.56 | 0.02 | | |
| I35_Rmp_NB_13 | 0.17 | 13647 | 2345 | 50 | 11372 | 1954 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 22 | 2274 | 391 | 0.0007 | 0.000036 | 0.000002 | 0.0005 | 0.0005 | 0.00005 | 0.00006 | 0.00043 | 0.000015 | 1.05 | 0.06 | 0.00 | 0.73 | 0.68 | 0.07 | 0.85 | 6.01 | 0.02 | | |
| I35_Rmp_NB_14 | 0.28 | 10734 | 2985 | 50 | 8945 | 2487 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 20 | 1789 | 497 | 0.0007 | 0.000039 | 0.000003 | 0.0005 | 0.0005 | 0.00005 | 0.00006 | 0.00044 | 0.000015 | 1.37 | 0.07 | 0.00 | 0.95 | 0.88 | 0.09 | 1.10 | 7.72 | 0.03 | | |
| I35_Rmp_NB_15 | 0.43 | 7922 | 3403 | 50 | 6602 | 2836 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 18 | 1320 | 567 | 0.0008 | 0.000042 | 0.000003 | 0.0006 | 0.0006 | 0.00005 | 0.00007 | 0.00046 | 0.000017 | 1.59 | 0.09 | 0.01 | 1.11 | 1.04 | 0.10 | 1.30 | 8.92 | 0.04 | | |
| I35_Rmp_NB_16 | 0.15 | 7973 | 1212 | 50 | 6645 | 1010 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 15 | 1329 | 202 | 0.0009 | 0.000049 | 0.000003 | 0.0007 | 0.0007 | 0.00006 | 0.00009 | 0.00051 | 0.000019 | 0.59 | 0.03 | 0.00 | 0.42 | 0.39 | 0.04 | 0.49 | 3.26 | 0.01 | | |
| I35_Rmp_NB_17 | 0.11 | 15896 | 1797 | 50 | 13247 | 1498 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 22 | 2649 | 299 | 0.0007 | 0.000036 | 0.000002 | 0.0005 | 0.0005 | 0.00005 | 0.00006 | 0.00043 | 0.000015 | 0.81 | 0.04 | 0.00 | 0.56 | 0.52 | 0.05 | 0.65 | 4.60 | 0.02 | | |
| I35_Rmp_NB_18 | 0.07 | 2556 | 181 | 50 | 2130 | 151 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 45 | 426 | 30 | 0.0004 | 0.000023 | 0.000001 | 0.0003 | 0.0003 | 0.00003 | 0.00003 | 0.00025 | 0.000010 | 0.07 | 0.00 | 0.00 | 0.05 | 0.05 | 0.00 | 0.06 | 0.41 | 0.00 | | |
| I35_Rmp_NB_19 | 0.06 | 7565 | 439 | 50 | 6304 | 366 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 48 | 1261 | 73 | 0.0004 | 0.000022 | 0.000001 | 0.0003 | 0.0003 | 0.00003 | 0.00003 | 0.00023 | 0.000010 | 0.18 | 0.01 | 0.00 | 0.12 | 0.11 | 0.01 | 0.14 | 0.98 | 0.00 | | |
| I35_Rmp_NB_20 | 0.05 | 11245 | 574 | 50 | 9371 | 478 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 20 | 1874 | 96 | 0.0007 | 0.000039 | 0.000003 | 0.0005 | 0.0005 | 0.00005 | 0.00007 | 0.00044 | 0.000015 | 0.26 | 0.01 | 0.00 | 0.18 | 0.17 | 0.02 | 0.21 | 1.49 | 0.01 | | |
| I35_Rmp_NB_21 | 0.08 | 4191 | 350 | 50 | 3493 | 292 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 40 | 699 | 58 | 0.0005 | 0.000025 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00004 | 0.00027 | 0.000010 | 0.14 | 0.01 | 0.00 | 0.10 | 0.09 | 0.01 | 0.11 | 0.81 | 0.00 | | |
| I35_Rmp_NB_22 | 0.15 | 8178 | 1242 | 50 | 6815 | 1035 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 40 | 1363 | 207 | 0.0005 | 0.000025 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.00004 | 0.00027 | 0.000010 | 0.51 | 0.03 | 0.00 | 0.35 | 0.32 | 0.03 | 0.40 | 2.86 | 0.01 | | |
| I35_Rmp_NB_23 | 0.10 | 7258 | 753 | 50 | 6048 | 628 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 43 | 1210 | 126 | 0.0004 | 0.000024 | 0.000001 | 0.0003 | 0.0003 | 0.00003 | 0.00004 | 0.00026 | 0.000010 | 0.31 | 0.02 | 0.00 | 0.21 | 0.20 | 0.02 | 0.24 | 1.72 | 0.01 | | |
| I35_Rmp_NB_24 | 0.10 | 21825 | 2100 | 50 | 18187 | 1750 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 20 | 3637 | 350 | 0.0007 | 0.000039 | 0.000003 | 0.0005 | 0.0005 | 0.00005 | 0.00007 | 0.00044 | 0.000015 | 0.96 | 0.05 | 0.00 | 0.67 | 0.62 | 0.06 | 0.78 | 5.43 | 0.02 | | |
| I35_Rmp_NB_25 | 0.14 | 9711 | 1352 | 50 | 8093 | 1127 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 45 | 1619 | 225 | 0.0004 | 0.000023 | 0.000001 | 0.0003 | 0.0003 | 0.00003 | 0.00003 | 0.00025 | 0.000010 | 0.55 | 0.03 | 0.00 | 0.38 | 0.35 | 0.03 | 0.43 | 3.07 | 0.01 | | |
| I35_Rmp_NB_26 | 0.17 | 10018 | 1740 | 50 | 8348 | 1450 | 0.00040 | 0.000022 | 0.000001 | 0.00028 | 0.00025 | 0.000025 | 0.00031 | 0.0022 | 0.000009 | 27 | 1670 | 290 | 0.0006 | 0.000032 | 0.000002 | 0.0004 | 0.0004 | 0.00004 | 0.00005 | 0.00040 | 0.000013 | 0.76 | 0.04 | 0.00 | 0.53 | 0.49 | 0.05 | 0.60 | 4.38 | 0.02 | | |
| I35_CB_NB_1 | 0.20 | 4958 | 994 | 55 | 4132 | 828 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0 | | | | | | | | | | | | | | | | | | | | | | | | |

| INTERIM - 2032 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | Totals | | | | | | | |
|-------------------|--------|-----------------------|-------------|------------------|----------------|----------------|---------------|----------|----------|---------|---------|----------|---------|--------|----------|---------------|-------------|-------------|--------|------------|----------|--------|--------|---------|--------|--------|----------|------|-------|--------|------|------|-------|------|-------|------|--|
| Link Name | Length | 24HR ADT 2032 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | |
| I35_Frmtg_SB_11 | 0.14 | 12009 | 1637 | 40 | 10008 | 1364 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 36 | 2002 | 273 | 0.0006 | 0.000026 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0004 | 0.0012 | 0.000011 | 0.88 | 0.04 | 0.00 | 0.40 | 0.28 | 0.03 | 0.62 | 1.79 | 0.02 | |
| I35_Frmtg_SB_12 | 0.24 | 14462 | 3431 | 40 | 12052 | 2859 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 23 | 2410 | 572 | 0.0008 | 0.000036 | 0.000002 | 0.0004 | 0.0003 | 0.00003 | 0.0006 | 0.0017 | 0.000015 | 1.99 | 0.09 | 0.00 | 0.90 | 0.64 | 0.07 | 1.42 | 4.05 | 0.04 | |
| I35_Frmtg_SB_13 | 0.04 | 13542 | 572 | 40 | 11285 | 477 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 21 | 2257 | 95 | 0.0009 | 0.000038 | 0.000002 | 0.0004 | 0.0003 | 0.00003 | 0.0007 | 0.0017 | 0.000016 | 0.34 | 0.01 | 0.00 | 0.15 | 0.11 | 0.01 | 0.24 | 0.68 | 0.01 | |
| I35_Frmtg_SB_14 | 0.17 | 16608 | 2830 | 40 | 13840 | 2358 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 8 | 2768 | 472 | 0.0015 | 0.000066 | 0.000004 | 0.0007 | 0.0006 | 0.00006 | 0.0015 | 0.0027 | 0.000027 | 1.98 | 0.09 | 0.00 | 0.91 | 0.68 | 0.07 | 1.58 | 3.80 | 0.04 | |
| I35_Frmtg_SB_15 | 0.18 | 18139 | 3241 | 40 | 15116 | 2701 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 14 | 3023 | 540 | 0.0011 | 0.000047 | 0.000003 | 0.0005 | 0.0004 | 0.00004 | 0.0009 | 0.0021 | 0.000020 | 2.02 | 0.09 | 0.00 | 0.92 | 0.67 | 0.07 | 1.51 | 4.05 | 0.04 | |
| I35_Frmtg_SB_16 | 0.27 | 23402 | 6242 | 40 | 19502 | 5202 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 4 | 3900 | 1040 | 0.0026 | 0.000108 | 0.000008 | 0.0013 | 0.0010 | 0.00010 | 0.0028 | 0.0042 | 0.000044 | 5.45 | 0.24 | 0.01 | 2.55 | 1.97 | 0.20 | 4.83 | 10.00 | 0.10 | |
| I35_Frmtg_SB_17 | 0.08 | 21921 | 1721 | 40 | 18267 | 1434 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 7 | 3653 | 287 | 0.0017 | 0.000072 | 0.000005 | 0.0018 | 0.0006 | 0.00007 | 0.0017 | 0.0029 | 0.000030 | 1.25 | 0.05 | 0.00 | 0.58 | 0.43 | 0.04 | 1.01 | 2.37 | 0.02 | |
| I35_Frmtg_SB_18 | 0.25 | 12979 | 3224 | 40 | 10815 | 2686 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 3 | 2163 | 537 | 0.0033 | 0.000136 | 0.000010 | 0.0016 | 0.0013 | 0.00013 | 0.0036 | 0.0053 | 0.000056 | 3.19 | 0.14 | 0.01 | 1.50 | 1.18 | 0.12 | 2.96 | 5.75 | 0.06 | |
| I35_Frmtg_SB_19 | 0.17 | 15482 | 2596 | 40 | 12902 | 2164 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 2.5 | 2580 | 433 | 0.0038 | 0.000158 | 0.000012 | 0.0019 | 0.0016 | 0.00016 | 0.0043 | 0.0062 | 0.000065 | 2.81 | 0.12 | 0.01 | 1.32 | 1.05 | 0.11 | 2.68 | 5.00 | 0.05 | |
| I35_Frmtg_SB_20 | 0.14 | 11599 | 1608 | 40 | 9666 | 1340 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 25 | 1933 | 268 | 0.0008 | 0.000034 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.0006 | 0.0016 | 0.000014 | 0.92 | 0.04 | 0.00 | 0.42 | 0.30 | 0.03 | 0.66 | 1.88 | 0.02 | |
| I35_Frmtg_SB_21 | 0.14 | 15022 | 2078 | 40 | 12519 | 1732 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 20 | 2504 | 346 | 0.0009 | 0.000039 | 0.000002 | 0.0004 | 0.0003 | 0.00003 | 0.0007 | 0.0018 | 0.000017 | 1.23 | 0.05 | 0.00 | 0.56 | 0.40 | 0.04 | 0.89 | 2.49 | 0.02 | |
| I35_Frmtg_SB_22 | 0.09 | 20643 | 1774 | 40 | 17203 | 1479 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 3 | 3441 | 296 | 0.0033 | 0.000136 | 0.000010 | 0.0016 | 0.0013 | 0.00013 | 0.0036 | 0.0053 | 0.000056 | 1.75 | 0.08 | 0.00 | 0.83 | 0.65 | 0.07 | 1.63 | 3.16 | 0.03 | |
| I35_Frmtg_SB_23 | 0.17 | 24526 | 4120 | 40 | 20439 | 3434 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 10 | 4088 | 687 | 0.0013 | 0.000057 | 0.000003 | 0.0006 | 0.0005 | 0.00005 | 0.0012 | 0.0024 | 0.000024 | 2.74 | 0.12 | 0.01 | 1.26 | 0.93 | 0.09 | 2.12 | 5.33 | 0.05 | |
| I35_Frmtg_SB_24 | 0.10 | 31629 | 3262 | 40 | 26357 | 2718 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 3 | 5271 | 544 | 0.0033 | 0.000136 | 0.000010 | 0.0016 | 0.0013 | 0.00013 | 0.0036 | 0.0053 | 0.000056 | 3.22 | 0.14 | 0.01 | 1.52 | 1.19 | 0.12 | 2.99 | 5.81 | 0.06 | |
| I35_Frmtg_SB_25 | 0.02 | 27030 | 669 | 40 | 22525 | 558 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 7 | 4505 | 112 | 0.0017 | 0.000072 | 0.000005 | 0.0008 | 0.0006 | 0.00007 | 0.0017 | 0.0029 | 0.000030 | 0.49 | 0.02 | 0.00 | 0.22 | 0.17 | 0.02 | 0.39 | 0.92 | 0.01 | |
| I35_Frmtg_SB_26 | 0.15 | 12161 | 1785 | 40 | 10134 | 1488 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 13 | 2027 | 298 | 0.0011 | 0.000049 | 0.000003 | 0.0005 | 0.0004 | 0.00004 | 0.0010 | 0.0021 | 0.000021 | 1.13 | 0.05 | 0.00 | 0.51 | 0.38 | 0.04 | 0.85 | 2.25 | 0.02 | |
| I35_Frmtg_SB_27 | 0.04 | 23045 | 953 | 40 | 19204 | 794 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 5 | 3841 | 159 | 0.0022 | 0.000092 | 0.000006 | 0.0010 | 0.0009 | 0.00009 | 0.0023 | 0.0036 | 0.000038 | 0.77 | 0.03 | 0.00 | 0.36 | 0.27 | 0.03 | 0.66 | 1.42 | 0.01 | |
| I35_Frmtg_SB_28 | 0.09 | 27439 | 2506 | 40 | 22866 | 2088 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 7 | 4573 | 418 | 0.0017 | 0.000072 | 0.000005 | 0.0008 | 0.0006 | 0.00007 | 0.0017 | 0.0029 | 0.000030 | 1.82 | 0.08 | 0.00 | 0.84 | 0.63 | 0.06 | 1.48 | 3.45 | 0.03 | |
| I35_Frmtg_SB_29 | 0.14 | 24373 | 3443 | 40 | 20311 | 2869 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 13 | 4062 | 574 | 0.0011 | 0.000049 | 0.000003 | 0.0005 | 0.0004 | 0.00004 | 0.0010 | 0.0021 | 0.000021 | 2.18 | 0.10 | 0.00 | 0.99 | 0.73 | 0.07 | 1.64 | 4.33 | 0.04 | |
| I35_Frmtg_SB_30 | 0.06 | 35870 | 2276 | 40 | 29892 | 1896 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 4 | 5978 | 379 | 0.0026 | 0.000108 | 0.000008 | 0.0013 | 0.0010 | 0.00010 | 0.0028 | 0.0042 | 0.000044 | 1.99 | 0.09 | 0.01 | 0.93 | 0.72 | 0.07 | 1.76 | 3.64 | 0.04 | |
| I35_Frmtg_SB_31 | 0.07 | 25906 | 1700 | 40 | 21588 | 1417 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 4 | 4318 | 283 | 0.0026 | 0.000108 | 0.000008 | 0.0013 | 0.0010 | 0.00010 | 0.0028 | 0.0042 | 0.000044 | 1.99 | 0.09 | 0.00 | 0.69 | 0.54 | 0.05 | 1.32 | 2.72 | 0.03 | |
| I35_Frmtg_SB_32 | 0.08 | 28870 | 2232 | 40 | 24058 | 1860 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 3 | 4812 | 372 | 0.0033 | 0.000136 | 0.000010 | 0.0016 | 0.0013 | 0.00013 | 0.0036 | 0.0053 | 0.000056 | 2.21 | 0.09 | 0.01 | 1.04 | 0.81 | 0.08 | 2.05 | 3.98 | 0.04 | |
| I35_Frmtg_SB_33 | 0.12 | 9759 | 1215 | 40 | 8133 | 1012 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 5 | 1627 | 202 | 0.0022 | 0.000092 | 0.000006 | 0.0010 | 0.0009 | 0.00009 | 0.0023 | 0.0036 | 0.000038 | 0.98 | 0.04 | 0.00 | 0.46 | 0.35 | 0.04 | 0.84 | 1.81 | 0.02 | |
| I35_Frmtg_SB_34 | 0.17 | 5314 | 911 | 40 | 4428 | 760 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 5 | 886 | 152 | 0.0022 | 0.000092 | 0.000006 | 0.0010 | 0.0009 | 0.00009 | 0.0023 | 0.0036 | 0.000038 | 0.73 | 0.03 | 0.00 | 0.34 | 0.26 | 0.03 | 0.63 | 1.36 | 0.01 | |
| I35_Frmtg_SB_35 | 0.03 | 13745 | 442 | 40 | 11454 | 368 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 2.5 | 2291 | 74 | 0.0038 | 0.000158 | 0.000012 | 0.0019 | 0.0016 | 0.00016 | 0.0043 | 0.0062 | 0.000065 | 4.48 | 0.02 | 0.00 | 0.23 | 0.18 | 0.02 | 0.46 | 0.85 | 0.01 | |
| I35_Frmtg_SB_36 | 0.10 | 21972 | 2202 | 40 | 18310 | 1835 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 8 | 3662 | 367 | 0.0015 | 0.000066 | 0.000004 | 0.0007 | 0.0006 | 0.00006 | 0.0015 | 0.0027 | 0.000027 | 1.54 | 0.07 | 0.00 | 0.71 | 0.53 | 0.05 | 1.23 | 2.96 | 0.03 | |
| I35_Frmtg_SB_37 | 0.17 | 8124 | 1376 | 40 | 6770 | 1146 | 0.00053 | 0.000024 | 0.000001 | 0.00024 | 0.00017 | 0.000018 | 0.00037 | 0.0011 | 0.000010 | 8 | 1354 | 229 | 0.0015 | 0.000066 | 0.000004 | 0.0007 | 0.0006 | 0.00006 | 0.0015 | 0.0027 | 0.000027 | 0.96 | 0.04 | 0.00 | 0.44 | 0.33 | 0.03 | 0.77 | 1.85 | 0.02 | |
| I35_Frmtg_SB_38 | 0.17 | 10219 | 1741 | 45 | 8516 | 1450 | 0.00048 | 0.000022 | 0.000001 | 0.00022 | 0.00016 | 0.000016 | 0.00034 | 0.0010 | 0.000010 | 29 | 1703 | 290 | 0.0007 | 0.000031 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0005 | 0.0016 | 0.000016 | 0.90 | 0.04 | 0.00 | 0.41 | 0.29 | 0.03 | 0.64 | 1.91 | 0.02 | |
| I35_Frmtg_SB_39 | 0.49 | 27235 | 13270 | 45 | 22696 | 11059 | 0.00048 | 0.000022 | 0.000001 | 0.00022 | 0.00016 | 0.000016 | 0.00034 | 0.0010 | 0.000010 | 10 | 4539 | 2212 | 0.0013 | 0.000057 | 0.000003 | 0.0006 | 0.0005 | 0.00005 | 0.0012 | 0.0024 | 0.000024 | 8.31 | 0.37 | 0.02 | 3.82 | 2.82 | 0.29 | 6.42 | 16.32 | 0.16 | |
| I35_Frmtg_SB_40 | 0.21 | 19849 | 4162 | 45 | 16541 | 3468 | 0.00048 | 0.000022 | 0.000001 | 0.00022 | 0.00016 | 0.000016 | 0.00034 | 0.0010 | 0.000010 | 12 | 3308 | 694 | 0.0012 | 0.000051 | 0.000003 | 0.0006 | 0.0004 | 0.00004 | 0.0010 | 0.0022 | 0.000022 | 2.51 | 0.11 | 0.01 | 1.15 | 0.84 | 0.09 | 1.89 | 5.02 | 0.05 | |
| I35_Frmtg_SB_41</ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| INTERIM - 2032 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | Totals | | | | | | | | | |
|----------------|--------|--------------------|----------------|---------------|-------------|---------------|---------|----------|----------|---------|---------|----------|---------|--------|-------------|------------|----------|------------|--------|----------|----------|--------|--------|---------|--------|--------|----------|------|-------|------|------|------|-------|------|-------|------|
| Link Name | Length | 24HR ADT 2032 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM |
| I35_DC_SB_5 | 0.25 | 14056 | 3534 | 55 | 11713 | 2945 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 2343 | 589 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 1.35 | 0.07 | 0.00 | 0.89 | 0.80 | 0.08 | 1.01 | 6.61 | 0.03 |
| I35_DC_SB_6 | 0.22 | 21160 | 4689 | 55 | 17634 | 3908 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 3527 | 782 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 1.79 | 0.10 | 0.01 | 1.18 | 1.06 | 0.10 | 1.34 | 8.77 | 0.04 |
| I35_DC_SB_7 | 0.19 | 24994 | 4761 | 55 | 20828 | 3967 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 4166 | 794 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 1.82 | 0.10 | 0.01 | 1.20 | 1.07 | 0.11 | 1.36 | 8.90 | 0.04 |
| I35_DC_SB_8 | 0.42 | 13238 | 5586 | 55 | 11032 | 4655 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 2206 | 931 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 2.14 | 0.11 | 0.01 | 1.41 | 1.26 | 0.12 | 1.60 | 10.45 | 0.05 |
| I35_DC_SB_9 | 0.22 | 38232 | 8458 | 55 | 31860 | 7048 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 46 | 6372 | 1410 | 0.0004 | 0.000023 | 0.000001 | 0.0003 | 0.0003 | 0.00003 | 0.0003 | 0.0025 | 0.000010 | 3.29 | 0.18 | 0.01 | 2.20 | 1.98 | 0.19 | 2.48 | 16.66 | 0.08 |
| I35_DC_EB_1 | 0.25 | 24023 | 6067 | 55 | 20019 | 5056 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 4004 | 1011 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 2.32 | 0.12 | 0.01 | 1.53 | 1.37 | 0.13 | 1.73 | 11.34 | 0.05 |
| I35_DC_EB_2 | 0.30 | 39765 | 12000 | 55 | 33138 | 10000 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 6628 | 2000 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 4.59 | 0.24 | 0.02 | 3.03 | 2.71 | 0.27 | 3.43 | 22.44 | 0.11 |
| I35_DC_EB_3 | 0.34 | 22183 | 7562 | 55 | 18486 | 6302 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 40 | 3697 | 1260 | 0.0005 | 0.000025 | 0.000002 | 0.0003 | 0.0003 | 0.00003 | 0.0004 | 0.0027 | 0.000010 | 2.99 | 0.16 | 0.01 | 2.00 | 1.80 | 0.18 | 2.27 | 15.21 | 0.07 |
| I35_DC_WB_1 | 0.19 | 19934 | 3812 | 55 | 16611 | 3177 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 3322 | 635 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 1.46 | 0.08 | 0.00 | 0.96 | 0.86 | 0.08 | 1.09 | 7.13 | 0.03 |
| I35_DC_WB_2 | 0.32 | 45541 | 14713 | 55 | 37951 | 12261 | 0.00038 | 0.000020 | 0.000001 | 0.00025 | 0.00023 | 0.000022 | 0.00029 | 0.0019 | 0.000009 | 55 | 7590 | 2452 | 0.0004 | 0.000020 | 0.000001 | 0.0003 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000009 | 5.63 | 0.30 | 0.02 | 3.72 | 3.32 | 0.33 | 4.21 | 27.51 | 0.13 |

| DESIGN - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | | Rates Peak | | | | | | | | | | Totals | | | | | | | |
|---------------|--------|-----------------------|----------|------------------|----------------|----------------|---------------|---------|------|---------|---------|---------|---------|---------|---------|---------------|-------------|-------------|--------|----------|------------|---------|---------|---------|---------|---------|----------|-------|-------|------|--------|-------|-------|-------|--------|------|--|--|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | |
| I35_ML_NB_1 | 0.27 | 76750 | 20602 | 60 | 63958 | 17169 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 5 | 12792 | 3434 | 0.0015 | 0.000058 | 0.00 | 0.00011 | 0.00014 | 0.00012 | 0.00019 | 0.00062 | 0.000023 | 9.98 | 0.40 | 0.00 | 6.45 | 7.40 | 0.66 | 10.09 | 42.58 | 0.17 | | |
| I35_ML_NB_2 | 0.65 | 90400 | 58777 | 60 | 75333 | 48980 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 9 | 15067 | 9796 | 0.0010 | 0.000039 | 0.00 | 0.00007 | 0.00008 | 0.00007 | 0.00011 | 0.00044 | 0.000015 | 23.27 | 0.94 | 0.00 | 14.33 | 15.80 | 1.42 | 21.20 | 103.54 | 0.10 | | |
| I35_ML_NB_3 | 0.27 | 121050 | 32542 | 60 | 100875 | 27118 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 7 | 20175 | 5424 | 0.0012 | 0.000045 | 0.00 | 0.00008 | 0.00010 | 0.00009 | 0.00014 | 0.00051 | 0.000018 | 13.91 | 0.56 | 0.00 | 8.74 | 9.80 | 0.88 | 13.24 | 60.87 | 0.23 | | |
| I35_ML_NB_4 | 0.35 | 91350 | 32228 | 60 | 76125 | 26857 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 7 | 15225 | 5371 | 0.0012 | 0.000045 | 0.00 | 0.00008 | 0.00010 | 0.00009 | 0.00014 | 0.00051 | 0.000018 | 13.77 | 0.56 | 0.00 | 8.65 | 9.71 | 0.87 | 13.11 | 60.28 | 0.23 | | |
| I35_ML_NB_5 | 0.14 | 109100 | 14954 | 60 | 90917 | 12462 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 6 | 18183 | 2492 | 0.0013 | 0.000051 | 0.00 | 0.00009 | 0.00012 | 0.00010 | 0.00016 | 0.00055 | 0.000020 | 6.75 | 0.27 | 0.00 | 4.29 | 4.87 | 0.43 | 6.60 | 29.19 | 0.11 | | |
| I35_ML_NB_6 | 0.53 | 97150 | 51027 | 60 | 80958 | 42523 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 13 | 16192 | 8505 | 0.0008 | 0.000031 | 0.00 | 0.00005 | 0.00006 | 0.00005 | 0.00008 | 0.00039 | 0.000012 | 18.38 | 0.75 | 0.00 | 11.10 | 12.01 | 1.08 | 15.87 | 85.50 | 0.32 | | |
| I35_ML_NB_7 | 0.27 | 118950 | 32492 | 60 | 99125 | 27077 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 11 | 19825 | 5415 | 0.0009 | 0.000034 | 0.00 | 0.00006 | 0.00007 | 0.00006 | 0.00009 | 0.00041 | 0.000013 | 12.19 | 0.50 | 0.00 | 7.41 | 8.08 | 0.73 | 10.77 | 55.38 | 0.21 | | |
| I35_ML_NB_8 | 0.37 | 106560 | 39566 | 60 | 88042 | 32971 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 15 | 17608 | 6594 | 0.0007 | 0.000028 | 0.00 | 0.00005 | 0.00006 | 0.00005 | 0.00007 | 0.00038 | 0.000011 | 13.82 | 0.57 | 0.00 | 8.29 | 8.92 | 0.80 | 11.71 | 65.45 | 0.24 | | |
| I35_ML_NB_9 | 0.39 | 95150 | 37368 | 60 | 79292 | 31140 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 15 | 15858 | 6228 | 0.0007 | 0.000028 | 0.00 | 0.00005 | 0.00006 | 0.00005 | 0.00007 | 0.00038 | 0.000011 | 13.05 | 0.54 | 0.00 | 7.83 | 8.42 | 0.76 | 11.06 | 61.81 | 0.23 | | |
| I35_ML_NB_10 | 0.26 | 121400 | 31959 | 60 | 101167 | 26632 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 15 | 20233 | 5326 | 0.0007 | 0.000028 | 0.00 | 0.00005 | 0.00006 | 0.00005 | 0.00007 | 0.00038 | 0.000011 | 11.16 | 0.46 | 0.00 | 6.70 | 7.20 | 0.65 | 9.46 | 52.87 | 0.19 | | |
| I35_ML_NB_11 | 0.42 | 115000 | 47974 | 60 | 95833 | 39979 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 19 | 19167 | 7996 | 0.0006 | 0.000023 | 0.00 | 0.00004 | 0.00004 | 0.00004 | 0.00006 | 0.00033 | 0.000009 | 15.79 | 0.65 | 0.00 | 9.33 | 9.91 | 0.89 | 13.07 | 76.00 | 0.28 | | |
| I35_ML_NB_12 | 0.02 | 131600 | 2649 | 60 | 109667 | 2207 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 16 | 21933 | 441 | 0.0007 | 0.000027 | 0.00 | 0.00004 | 0.00005 | 0.00005 | 0.00007 | 0.00036 | 0.000010 | 0.91 | 0.04 | 0.00 | 0.54 | 0.58 | 0.05 | 0.77 | 4.33 | 0.02 | | |
| I35_ML_NB_13 | 0.46 | 121800 | 55727 | 60 | 101500 | 46439 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 24 | 20000 | 9288 | 0.0005 | 0.000020 | 0.00 | 0.00003 | 0.00004 | 0.00003 | 0.00005 | 0.00030 | 0.000008 | 17.51 | 0.72 | 0.00 | 10.27 | 10.84 | 0.98 | 14.22 | 85.65 | 0.31 | | |
| I35_ML_NB_14 | 0.11 | 144750 | 15548 | 60 | 120625 | 12957 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 22 | 24125 | 2591 | 0.0005 | 0.000021 | 0.00 | 0.00003 | 0.00004 | 0.00003 | 0.00005 | 0.00031 | 0.000008 | 4.96 | 0.20 | 0.00 | 2.92 | 3.09 | 0.28 | 4.06 | 24.14 | 0.09 | | |
| I35_ML_NB_15 | 0.31 | 128150 | 39433 | 60 | 106792 | 32861 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 34 | 21358 | 6572 | 0.0004 | 0.000016 | 0.00 | 0.00002 | 0.00003 | 0.00002 | 0.00003 | 0.00023 | 0.000007 | 11.76 | 0.49 | 0.00 | 6.77 | 7.05 | 0.64 | 9.28 | 55.50 | 0.21 | | |
| I35_ML_NB_16 | 0.18 | 141100 | 25109 | 60 | 117583 | 20924 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 32 | 23517 | 4185 | 0.0004 | 0.000017 | 0.00 | 0.00003 | 0.00003 | 0.00003 | 0.00004 | 0.00025 | 0.000007 | 7.55 | 0.31 | 0.00 | 4.39 | 4.60 | 0.41 | 6.00 | 36.50 | 0.13 | | |
| I35_ML_NB_17 | 0.29 | 54900 | 15837 | 60 | 45750 | 13197 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 20 | 9150 | 2639 | 0.0006 | 0.000023 | 0.00 | 0.00004 | 0.00004 | 0.00004 | 0.00005 | 0.00033 | 0.000009 | 5.15 | 0.21 | 0.00 | 3.03 | 3.22 | 0.29 | 4.25 | 24.88 | 0.09 | | |
| I35_ML_NB_18 | 0.24 | 86200 | 20875 | 60 | 71833 | 17396 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 54 | 14367 | 3479 | 0.0003 | 0.000012 | 0.00 | 0.00002 | 0.00002 | 0.00002 | 0.00002 | 0.00014 | 0.000005 | 5.89 | 0.24 | 0.00 | 3.33 | 3.41 | 0.31 | 4.53 | 26.28 | 0.11 | | |
| I35_ML_NB_19 | 0.26 | 83100 | 21612 | 60 | 69250 | 18010 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 35 | 13850 | 3602 | 0.0004 | 0.000016 | 0.00 | 0.00002 | 0.00003 | 0.00002 | 0.00003 | 0.00021 | 0.000007 | 6.42 | 0.27 | 0.00 | 3.68 | 3.82 | 0.35 | 5.05 | 29.96 | 0.11 | | |
| I35_ML_NB_20 | 1.37 | 74300 | 101758 | 60 | 61917 | 84799 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 6 | 12383 | 16959 | 0.0003 | 0.000051 | 0.00 | 0.00009 | 0.00012 | 0.00010 | 0.00016 | 0.00055 | 0.000020 | 45.90 | 1.84 | 0.00 | 3.21 | 33.11 | 2.96 | 44.92 | 198.66 | 0.77 | | |
| I35_ML_NB_21 | 0.49 | 73900 | 35895 | 60 | 61583 | 29912 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 33 | 12317 | 5983 | 0.0004 | 0.000017 | 0.00 | 0.00003 | 0.00003 | 0.00003 | 0.00004 | 0.00024 | 0.000007 | 10.75 | 0.45 | 0.00 | 6.22 | 6.49 | 0.59 | 8.51 | 51.32 | 0.19 | | |
| I35_ML_NB_22 | 0.37 | 87650 | 23085 | 60 | 73042 | 26738 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 19 | 14608 | 5347 | 0.0006 | 0.000023 | 0.00 | 0.00004 | 0.00004 | 0.00004 | 0.00006 | 0.00033 | 0.000009 | 10.56 | 0.43 | 0.00 | 6.24 | 6.63 | 0.60 | 8.74 | 50.83 | 0.18 | | |
| I35_ML_NB_23 | 0.50 | 82500 | 41013 | 60 | 68750 | 34178 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 9 | 13750 | 6836 | 0.0010 | 0.000039 | 0.00 | 0.00007 | 0.00008 | 0.00007 | 0.00011 | 0.00044 | 0.000015 | 16.23 | 0.66 | 0.00 | 10.00 | 11.03 | 0.99 | 14.80 | 72.25 | 0.28 | | |
| I35_ML_NB_24 | 0.19 | 64350 | 12462 | 60 | 53625 | 10385 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 6 | 10725 | 2077 | 0.0013 | 0.000051 | 0.00 | 0.00009 | 0.00012 | 0.00010 | 0.00016 | 0.00055 | 0.000020 | 5.62 | 0.23 | 0.00 | 3.58 | 4.05 | 0.36 | 5.50 | 24.33 | 0.09 | | |
| I35_ML_NB_25 | 0.09 | 146850 | 13707 | 60 | 122375 | 11423 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 24475 | 2285 | 0.0018 | 0.000069 | 0.00 | 0.00013 | 0.00017 | 0.00015 | 0.00023 | 0.00073 | 0.000027 | 7.30 | 0.29 | 0.00 | 4.81 | 5.60 | 0.50 | 7.70 | 30.88 | 0.12 | | |
| I35_ML_NB_26 | 0.30 | 138000 | 41161 | 60 | 115000 | 34300 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 23000 | 6860 | 0.0018 | 0.000069 | 0.00 | 0.00013 | 0.00017 | 0.00015 | 0.00023 | 0.00073 | 0.000027 | 21.93 | 0.87 | 0.00 | 14.44 | 16.82 | 1.50 | 23.12 | 92.72 | 0.36 | | |
| I35_ML_NB_27 | 0.25 | 164650 | 41265 | 60 | 137208 | 34387 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 27442 | 6878 | 0.0018 | 0.000069 | 0.00 | 0.00013 | 0.00017 | 0.00015 | 0.00023 | 0.00073 | 0.000027 | 21.99 | 0.87 | 0.00 | 14.48 | 16.86 | 1.50 | 23.18 | 92.95 | 0.36 | | |
| I35_ML_NB_28 | 0.46 | 152800 | 69869 | 60 | 127333 | 58224 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 5 | 25467 | 11645 | 0.0015 | 0.000058 | 0.00 | 0.00011 | 0.00014 | 0.00012 | 0.00019 | 0.00062 | 0.000023 | 33.83 | 1.35 | 0.00 | 21.88 | 25.11 | 2.24 | 34.23 | 144.40 | 0.56 | | |
| I35_ML_NB_29 | 0.41 | 137000 | 56092 | 60 | 114167 | 46744 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 22833 | 9349 | 0.0018 | 0.000069 | 0.00 | 0.00013 | 0.00017 | 0.00015 | 0.00023 | 0.00073 | 0.000027 | 29.89 | 1.18 | 0.00 | 19.68 | 22.92 | 2.04 | 31.51 | 126.35 | 0.49 | | |
| I35_ML_NB_30 | 0.51 | 125000 | 63250 | 60 | 104167 | 52709 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 20833 | 10541 | 0.0018 | 0.000069 | 0.00 | 0.00013 | 0.00017 | 0.00015 | 0.00023 | 0.00073 | 0.000027 | 33.70 | 1.33 | 0.00 | 22.19 | 25.85 | 2.30 | 35.53 | 142.47 | 0.55 | | |

| DESIGN - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | | Inputs Peak | | | | Rates Peak | | | | | | | | | | | Totals | | | | | | | |
|-----------------|--------|-----------------------|----------|------------------|----------------|----------------|---------------|----------|------|---------|---------|----------|---------|--------|----------|---------------|-------------|-------------|--------|----------|------|------------|--------|---------|--------|--------|----------|-------|-------|------|------|------|--------|-------|-------|------|--|--|--|--|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | | | |
| I35_Frtmg_NB_45 | 0.71 | 38300 | 27329 | 45 | 31917 | 22774 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 2.5 | 6383 | 4555 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 22.30 | 0.74 | 0.00 | 9.16 | 8.64 | 0.79 | 22.42 | 34.31 | 0.31 | | | | |
| I35_Frtmg_NB_46 | 0.19 | 51650 | 9747 | 45 | 43042 | 8122 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 2.5 | 8608 | 1624 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 79.50 | 0.26 | 0.00 | 3.27 | 3.08 | 0.28 | 8.00 | 12.24 | 0.11 | | | | |
| I35_Rmp_NB_47 | 0.34 | 63650 | 21450 | 45 | 53042 | 17875 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 2.5 | 10608 | 3575 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 17.50 | 0.58 | 0.00 | 7.19 | 6.78 | 0.62 | 17.60 | 26.93 | 0.24 | | | | |
| I35_Rmp_NB_1 | 0.25 | 13650 | 3353 | 50 | 11375 | 2794 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 3 | 2275 | 559 | 0.0023 | 0.000086 | 0.00 | 0.0017 | 0.0021 | 0.00019 | 0.0030 | 0.0092 | 0.000034 | 2.13 | 0.08 | 0.00 | 1.47 | 1.76 | 0.16 | 2.39 | 9.60 | 0.03 | | | | |
| I35_Rmp_NB_2 | 0.49 | 17750 | 8712 | 50 | 14792 | 7260 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 4 | 2958 | 1452 | 0.0018 | 0.000069 | 0.00 | 0.0013 | 0.0017 | 0.00015 | 0.0023 | 0.0073 | 0.000027 | 4.84 | 0.19 | 0.00 | 3.27 | 3.85 | 0.34 | 5.16 | 22.24 | 0.08 | | | | |
| I35_Rmp_NB_3 | 0.14 | 29700 | 4113 | 50 | 24750 | 3427 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 41 | 4950 | 685 | 0.0003 | 0.000014 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000006 | 1.29 | 0.05 | 0.00 | 0.79 | 0.85 | 0.08 | 1.06 | 6.79 | 0.02 | | | | |
| I35_Rmp_NB_4 | 0.22 | 11950 | 2631 | 50 | 9958 | 2193 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 14 | 1992 | 439 | 0.0007 | 0.000029 | 0.00 | 0.0005 | 0.0002 | 0.00005 | 0.0007 | 0.0038 | 0.000011 | 0.99 | 0.04 | 0.00 | 0.63 | 0.69 | 0.06 | 0.88 | 5.17 | 0.02 | | | | |
| I35_Rmp_NB_5 | 0.17 | 21800 | 3627 | 50 | 18167 | 3022 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 14 | 3633 | 604 | 0.0007 | 0.000029 | 0.00 | 0.0005 | 0.0006 | 0.00005 | 0.0007 | 0.0038 | 0.000011 | 1.37 | 0.06 | 0.00 | 0.86 | 0.95 | 0.09 | 1.21 | 7.12 | 0.02 | | | | |
| I35_Rmp_NB_6 | 0.13 | 13300 | 1665 | 50 | 11083 | 1388 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 12 | 2217 | 278 | 0.0008 | 0.000032 | 0.00 | 0.0005 | 0.0006 | 0.00006 | 0.0009 | 0.0040 | 0.000013 | 0.65 | 0.03 | 0.00 | 0.41 | 0.46 | 0.04 | 0.58 | 3.31 | 0.01 | | | | |
| I35_Rmp_NB_7 | 0.10 | 10500 | 1018 | 50 | 8750 | 848 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 11 | 1750 | 170 | 0.0009 | 0.000034 | 0.00 | 0.0006 | 0.0007 | 0.00006 | 0.0009 | 0.0041 | 0.000013 | 0.40 | 0.02 | 0.00 | 0.26 | 0.29 | 0.03 | 0.37 | 2.04 | 0.01 | | | | |
| I35_Rmp_NB_8 | 0.12 | 26250 | 3072 | 50 | 21875 | 2560 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 34 | 4375 | 512 | 0.0004 | 0.000016 | 0.00 | 0.0002 | 0.0003 | 0.00002 | 0.0003 | 0.0023 | 0.000007 | 0.98 | 0.04 | 0.00 | 0.60 | 0.65 | 0.06 | 0.82 | 5.25 | 0.02 | | | | |
| I35_Rmp_NB_9 | 0.14 | 6400 | 884 | 50 | 5333 | 737 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 34 | 1067 | 147 | 0.0004 | 0.000016 | 0.00 | 0.0002 | 0.0003 | 0.00002 | 0.0003 | 0.0023 | 0.000007 | 0.28 | 0.01 | 0.00 | 0.17 | 0.19 | 0.02 | 0.23 | 1.51 | 0.01 | | | | |
| I35_Rmp_NB_10 | 0.18 | 16600 | 2976 | 50 | 13833 | 2480 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 20 | 2767 | 496 | 0.0006 | 0.000023 | 0.00 | 0.0004 | 0.0004 | 0.00004 | 0.0005 | 0.0033 | 0.000009 | 1.03 | 0.04 | 0.00 | 0.64 | 0.70 | 0.06 | 0.89 | 5.57 | 0.02 | | | | |
| I35_Rmp_NB_11 | 0.11 | 9800 | 1062 | 50 | 8167 | 885 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 2.5 | 1633 | 177 | 0.0027 | 0.000100 | 0.00 | 0.0020 | 0.0025 | 0.00022 | 0.0036 | 0.0107 | 0.000039 | 0.74 | 0.03 | 0.00 | 0.52 | 0.63 | 0.06 | 0.86 | 3.30 | 0.01 | | | | |
| I35_Rmp_NB_12 | 0.13 | 22950 | 2917 | 50 | 19125 | 2431 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 26 | 3825 | 486 | 0.0005 | 0.000019 | 0.00 | 0.0003 | 0.0003 | 0.00003 | 0.0004 | 0.0030 | 0.000008 | 0.97 | 0.04 | 0.00 | 0.60 | 0.66 | 0.06 | 0.82 | 5.32 | 0.02 | | | | |
| I35_Rmp_NB_13 | 0.17 | 16600 | 2853 | 50 | 13833 | 2377 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 24 | 2767 | 476 | 0.0005 | 0.000020 | 0.00 | 0.0003 | 0.0004 | 0.00003 | 0.0005 | 0.0030 | 0.000008 | 0.96 | 0.04 | 0.00 | 0.60 | 0.65 | 0.06 | 0.81 | 5.24 | 0.02 | | | | |
| I35_Rmp_NB_14 | 0.28 | 12950 | 3601 | 50 | 10792 | 3001 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 29 | 2158 | 600 | 0.0004 | 0.000018 | 0.00 | 0.0003 | 0.0003 | 0.00003 | 0.0004 | 0.0029 | 0.000007 | 1.18 | 0.05 | 0.00 | 0.73 | 0.80 | 0.07 | 0.99 | 6.52 | 0.02 | | | | |
| I35_Rmp_NB_15 | 0.43 | 9650 | 4145 | 50 | 8042 | 3454 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 20 | 1608 | 691 | 0.0006 | 0.000023 | 0.00 | 0.0004 | 0.0003 | 0.00004 | 0.0005 | 0.0033 | 0.000009 | 1.44 | 0.06 | 0.00 | 0.90 | 0.98 | 0.09 | 1.24 | 7.76 | 0.03 | | | | |
| I35_Rmp_NB_16 | 0.15 | 9750 | 1482 | 50 | 8125 | 1235 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 15 | 1625 | 247 | 0.0007 | 0.000028 | 0.00 | 0.0005 | 0.0006 | 0.00005 | 0.0007 | 0.0038 | 0.000011 | 0.55 | 0.02 | 0.00 | 0.35 | 0.38 | 0.03 | 0.48 | 2.90 | 0.01 | | | | |
| I35_Rmp_NB_17 | 0.11 | 19400 | 2193 | 50 | 16167 | 1828 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 18 | 3233 | 365 | 0.0006 | 0.000024 | 0.00 | 0.0004 | 0.0005 | 0.00004 | 0.0006 | 0.0034 | 0.000010 | 0.78 | 0.03 | 0.00 | 0.49 | 0.53 | 0.05 | 0.67 | 4.16 | 0.01 | | | | |
| I35_Rmp_NB_18 | 0.07 | 3100 | 220 | 50 | 2583 | 183 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 45 | 517 | 37 | 0.0003 | 0.000014 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0018 | 0.000006 | 0.07 | 0.00 | 0.00 | 0.04 | 0.04 | 0.00 | 0.06 | 0.36 | 0.00 | | | | |
| I35_Rmp_NB_19 | 0.06 | 9200 | 534 | 50 | 7667 | 445 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 45 | 1533 | 89 | 0.0003 | 0.000014 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0018 | 0.000006 | 0.17 | 0.01 | 0.00 | 0.10 | 0.11 | 0.01 | 0.14 | 0.87 | 0.00 | | | | |
| I35_Rmp_NB_20 | 0.05 | 13750 | 702 | 50 | 11458 | 585 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 14 | 2292 | 117 | 0.0007 | 0.000029 | 0.00 | 0.0005 | 0.0006 | 0.00005 | 0.0007 | 0.0038 | 0.000011 | 0.26 | 0.01 | 0.00 | 0.17 | 0.18 | 0.02 | 0.23 | 1.38 | 0.00 | | | | |
| I35_Rmp_NB_21 | 0.08 | 5150 | 430 | 50 | 4292 | 358 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 10 | 858 | 72 | 0.0009 | 0.000036 | 0.00 | 0.0006 | 0.0007 | 0.00007 | 0.0010 | 0.0042 | 0.000014 | 0.17 | 0.01 | 0.00 | 0.11 | 0.12 | 0.01 | 0.16 | 0.87 | 0.00 | | | | |
| I35_Rmp_NB_22 | 0.15 | 9950 | 1511 | 50 | 8292 | 1260 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 40 | 1658 | 252 | 0.0004 | 0.000015 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0020 | 0.000006 | 0.47 | 0.02 | 0.00 | 0.29 | 0.31 | 0.03 | 0.39 | 2.50 | 0.01 | | | | |
| I35_Rmp_NB_23 | 0.10 | 8850 | 918 | 50 | 7375 | 765 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 29 | 1475 | 153 | 0.0004 | 0.000018 | 0.00 | 0.0003 | 0.0003 | 0.00003 | 0.0004 | 0.0029 | 0.000007 | 0.30 | 0.01 | 0.00 | 0.19 | 0.20 | 0.02 | 0.25 | 1.66 | 0.01 | | | | |
| I35_Rmp_NB_24 | 0.10 | 26650 | 2565 | 50 | 22208 | 2137 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 25 | 4442 | 427 | 0.0005 | 0.000020 | 0.00 | 0.0003 | 0.0004 | 0.00003 | 0.0004 | 0.0030 | 0.000008 | 0.86 | 0.04 | 0.00 | 0.53 | 0.58 | 0.05 | 0.73 | 4.69 | 0.02 | | | | |
| I35_Rmp_NB_25 | 0.14 | 11850 | 1650 | 50 | 9875 | 1375 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 32 | 1975 | 275 | 0.0004 | 0.000017 | 0.00 | 0.0003 | 0.0003 | 0.00003 | 0.0004 | 0.0025 | 0.000007 | 0.53 | 0.02 | 0.00 | 0.33 | 0.36 | 0.03 | 0.44 | 2.89 | 0.01 | | | | |
| I35_Rmp_NB_26 | 0.17 | 12000 | 2084 | 50 | 10000 | 1737 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 2.5 | 2000 | 347 | 0.0027 | 0.000100 | 0.00 | 0.0020 | 0.0025 | 0.00022 | 0.0036 | 0.0107 | 0.000039 | 1.44 | 0.06 | 0.00 | 1.02 | 1.23 | 0.11 | 1.68 | 6.48 | 0.02 | | | | |
| I35_CD_NB_1 | 0.20 | 6050 | 1213 | 55 | 5042 | 1011 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 4 | 1008 | 202 | 0.0018 | 0.000069 | 0.00 | 0.0013 | 0.0017 | 0.00015 | 0.0023 | 0.0073 | 0.000027 | 0.66 | 0.03 | 0.00 | 0.44 | 0.51 | 0.05 | 0.70 | 2.83 | 0.01 | | | | |
| I35_CD_NB_2 | 0.21 | 20650 | 4428 | 55 | 17208 | 3690 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 5 | 3442 | 738 | 0.0015 | 0.000058 | 0.00 | 0.0011 | 0.0014 | 0.00012 | 0.0019 | 0.0062 | 0.000023 | 2.19 | | | | | | | | | | | | |

| DESIGN - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | Totals | | | | | | | |
|-----------------|--------|-----------------------|----------|------------------|----------------|----------------|---------------|----------|------|---------|---------|----------|---------|--------|----------|---------------|-------------|-------------|--------|------------|------|--------|--------|---------|--------|--------|----------|------|-------|--------|------|------|-------|------|------|------|--|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | |
| I35 Frrtg_SB_7 | 0.15 | 27700 | 4219 | 45 | 23083 | 3516 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 11 | 4617 | 703 | 0.0010 | 0.000033 | 0.00 | 0.0004 | 0.0004 | 0.00003 | 0.0009 | 0.0016 | 0.000014 | 1.99 | 0.07 | 0.00 | 0.81 | 0.69 | 0.06 | 1.60 | 3.63 | 0.03 | |
| I35 Frrtg_SB_8 | 0.19 | 54700 | 10271 | 45 | 45583 | 8559 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 8 | 9117 | 1712 | 0.0012 | 0.000040 | 0.00 | 0.0005 | 0.0005 | 0.00004 | 0.0012 | 0.0018 | 0.000016 | 5.24 | 0.19 | 0.00 | 2.13 | 1.86 | 0.17 | 4.39 | 9.24 | 0.08 | |
| I35 Frrtg_SB_9 | 0.18 | 34600 | 6390 | 45 | 28833 | 5325 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 13 | 5767 | 1065 | 0.0009 | 0.000031 | 0.00 | 0.0004 | 0.0003 | 0.00003 | 0.0008 | 0.0015 | 0.000013 | 2.91 | 0.11 | 0.00 | 1.18 | 1.00 | 0.09 | 2.29 | 5.41 | 0.05 | |
| I35 Frrtg_SB_10 | 0.09 | 31550 | 2714 | 45 | 26292 | 2262 | 0.00037 | 0.000014 | 0.00 | 0.00015 | 0.00012 | 0.000011 | 0.00027 | 0.0007 | 0.000006 | 3 | 5258 | 452 | 0.0026 | 0.000080 | 0.00 | 0.0011 | 0.0011 | 0.00010 | 0.0030 | 0.0035 | 0.000033 | 2.01 | 0.07 | 0.00 | 0.83 | 0.77 | 0.07 | 1.97 | 3.17 | 0.03 | |
| I35 Frrtg_SB_11 | 0.14 | 14650 | 1997 | 40 | 12208 | 1664 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 36 | 2442 | 333 | 0.0004 | 0.000016 | 0.00 | 0.0002 | 0.0011 | 0.00001 | 0.0003 | 0.0008 | 0.000007 | 0.82 | 0.03 | 0.00 | 0.33 | 0.27 | 0.03 | 0.61 | 1.54 | 0.01 | |
| I35 Frrtg_SB_12 | 0.24 | 17700 | 4199 | 40 | 14750 | 3500 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 22 | 2950 | 700 | 0.0006 | 0.000023 | 0.00 | 0.0003 | 0.0002 | 0.00002 | 0.0005 | 0.0012 | 0.000010 | 1.87 | 0.07 | 0.00 | 0.75 | 0.63 | 0.06 | 1.41 | 3.53 | 0.03 | |
| I35 Frrtg_SB_13 | 0.04 | 16550 | 699 | 40 | 13792 | 583 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 27 | 2758 | 117 | 0.0006 | 0.000020 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0004 | 0.0011 | 0.000009 | 0.30 | 0.01 | 0.00 | 0.12 | 0.10 | 0.01 | 0.21 | 0.58 | 0.00 | |
| I35 Frrtg_SB_14 | 0.17 | 20350 | 3467 | 40 | 16958 | 2889 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 7 | 3392 | 578 | 0.0013 | 0.000044 | 0.00 | 0.0005 | 0.0005 | 0.00005 | 0.0014 | 0.0020 | 0.000018 | 1.94 | 0.07 | 0.00 | 0.79 | 0.69 | 0.06 | 1.66 | 3.35 | 0.03 | |
| I35 Frrtg_SB_15 | 0.18 | 22100 | 3949 | 40 | 18417 | 3291 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 10 | 3683 | 658 | 0.0010 | 0.000035 | 0.00 | 0.0004 | 0.0004 | 0.00004 | 0.0010 | 0.0017 | 0.000015 | 2.02 | 0.07 | 0.00 | 0.82 | 0.70 | 0.07 | 1.64 | 3.61 | 0.03 | |
| I35 Frrtg_SB_16 | 0.27 | 28500 | 7602 | 40 | 23750 | 6335 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 4750 | 1267 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 6.42 | 0.21 | 0.00 | 2.64 | 2.48 | 0.23 | 6.42 | 9.89 | 0.09 | |
| I35 Frrtg_SB_17 | 0.08 | 26800 | 2104 | 40 | 22333 | 1754 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 21 | 4467 | 351 | 0.0007 | 0.000024 | 0.00 | 0.0003 | 0.0003 | 0.00002 | 0.0005 | 0.0013 | 0.000010 | 0.94 | 0.03 | 0.00 | 0.38 | 0.32 | 0.03 | 0.71 | 1.78 | 0.01 | |
| I35 Frrtg_SB_18 | 0.25 | 15850 | 3937 | 40 | 13208 | 3281 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 17 | 2642 | 656 | 0.0007 | 0.000027 | 0.00 | 0.0003 | 0.0003 | 0.00003 | 0.0006 | 0.0014 | 0.000011 | 1.82 | 0.07 | 0.00 | 0.74 | 0.62 | 0.06 | 1.40 | 3.42 | 0.03 | |
| I35 Frrtg_SB_19 | 0.17 | 18950 | 3178 | 40 | 15792 | 2648 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 3 | 3158 | 530 | 0.0026 | 0.000080 | 0.00 | 0.0011 | 0.0011 | 0.00010 | 0.0030 | 0.0035 | 0.000033 | 2.45 | 0.08 | 0.00 | 1.00 | 0.93 | 0.09 | 2.38 | 3.86 | 0.03 | |
| I35 Frrtg_SB_20 | 0.14 | 14200 | 1968 | 40 | 11833 | 1640 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 2367 | 328 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.66 | 0.06 | 0.00 | 0.68 | 0.64 | 0.06 | 1.66 | 2.56 | 0.02 | |
| I35 Frrtg_SB_21 | 0.14 | 18350 | 2538 | 40 | 15292 | 2115 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 3058 | 423 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.24 | 0.07 | 0.00 | 0.88 | 0.83 | 0.06 | 2.14 | 3.30 | 0.03 | |
| I35 Frrtg_SB_22 | 0.09 | 25200 | 2166 | 40 | 21000 | 1805 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 4200 | 361 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.83 | 0.06 | 0.00 | 0.75 | 0.71 | 0.06 | 1.83 | 2.82 | 0.03 | |
| I35 Frrtg_SB_23 | 0.17 | 29950 | 5031 | 40 | 24958 | 4193 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 4992 | 839 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 4.25 | 0.14 | 0.00 | 1.74 | 1.64 | 0.15 | 4.25 | 6.55 | 0.06 | |
| I35 Frrtg_SB_24 | 0.10 | 38650 | 3986 | 40 | 32208 | 3322 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 6442 | 664 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 3.37 | 0.11 | 0.00 | 1.38 | 1.30 | 0.12 | 3.37 | 5.19 | 0.05 | |
| I35 Frrtg_SB_25 | 0.02 | 33000 | 817 | 40 | 27500 | 681 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 3 | 5500 | 136 | 0.0026 | 0.000080 | 0.00 | 0.0011 | 0.0011 | 0.00010 | 0.0030 | 0.0035 | 0.000033 | 0.63 | 0.02 | 0.00 | 0.26 | 0.24 | 0.02 | 0.61 | 0.99 | 0.01 | |
| I35 Frrtg_SB_26 | 0.15 | 14800 | 2172 | 40 | 12333 | 1810 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 2467 | 362 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.83 | 0.06 | 0.00 | 0.75 | 0.71 | 0.06 | 1.84 | 2.83 | 0.03 | |
| I35 Frrtg_SB_27 | 0.04 | 28100 | 1162 | 40 | 23417 | 968 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 4683 | 194 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 0.98 | 0.03 | 0.00 | 0.40 | 0.38 | 0.03 | 0.98 | 1.51 | 0.01 | |
| I35 Frrtg_SB_28 | 0.09 | 33500 | 3059 | 40 | 27917 | 2550 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 5583 | 510 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 2.58 | 0.09 | 0.00 | 1.06 | 1.00 | 0.09 | 2.58 | 3.98 | 0.04 | |
| I35 Frrtg_SB_29 | 0.14 | 29750 | 4203 | 40 | 24792 | 3502 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 4958 | 700 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 3.55 | 0.12 | 0.00 | 1.46 | 1.37 | 0.13 | 3.55 | 5.47 | 0.05 | |
| I35 Frrtg_SB_30 | 0.06 | 43800 | 2779 | 40 | 36500 | 2316 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 7300 | 463 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 2.35 | 0.08 | 0.00 | 0.96 | 0.91 | 0.08 | 2.35 | 3.61 | 0.03 | |
| I35 Frrtg_SB_31 | 0.07 | 31650 | 2077 | 40 | 26375 | 1731 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 5275 | 346 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.75 | 0.06 | 0.00 | 0.72 | 0.68 | 0.06 | 1.76 | 2.70 | 0.02 | |
| I35 Frrtg_SB_32 | 0.08 | 35300 | 2729 | 40 | 29417 | 2274 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 5883 | 455 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 2.30 | 0.08 | 0.00 | 0.95 | 0.89 | 0.08 | 2.31 | 3.55 | 0.03 | |
| I35 Frrtg_SB_33 | 0.12 | 11950 | 1487 | 40 | 9958 | 1239 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 1992 | 248 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 1.26 | 0.04 | 0.00 | 0.52 | 0.49 | 0.04 | 1.26 | 1.93 | 0.02 | |
| I35 Frrtg_SB_34 | 0.17 | 6500 | 1115 | 40 | 5417 | 929 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 1083 | 186 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 0.94 | 0.03 | 0.00 | 0.39 | 0.36 | 0.03 | 0.94 | 1.45 | 0.01 | |
| I35 Frrtg_SB_35 | 0.03 | 16750 | 538 | 40 | 13958 | 448 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 2.5 | 2792 | 90 | 0.0030 | 0.000093 | 0.00 | 0.0013 | 0.0013 | 0.00012 | 0.0036 | 0.0040 | 0.000038 | 0.45 | 0.02 | 0.00 | 0.19 | 0.18 | 0.02 | 0.45 | 0.70 | 0.01 | |
| I35 Frrtg_SB_36 | 0.10 | 26800 | 2685 | 40 | 22333 | 2238 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 4 | 4467 | 448 | 0.0020 | 0.000064 | 0.00 | 0.0008 | 0.0008 | 0.00008 | 0.0023 | 0.0028 | 0.000026 | 1.82 | 0.06 | 0.00 | 0.75 | 0.68 | 0.06 | 1.69 | 2.96 | 0.03 | |
| I35 Frrtg_SB_37 | 0.17 | 9900 | 1676 | 40 | 8250 | 1397 | 0.00041 | 0.000015 | 0.00 | 0.00016 | 0.00013 | 0.000013 | 0.00030 | 0.0008 | 0.000007 | 4 | 1650 | 279 | 0.0020 | 0.000064 | 0.00 | 0.0008 | 0.0008 | | | | | | | | | | | | | | |

| DESIGN - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | Totals | | | | | | | |
|---------------|--------|-----------------------|----------|------------------|----------------|----------------|---------------|----------|------|---------|---------|----------|---------|--------|----------|---------------|-------------|-------------|--------|------------|------|--------|--------|---------|--------|--------|----------|------|-------|--------|------|------|-------|------|-------|------|--|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | |
| I35_Rmp_SB_28 | 0.32 | 19650 | 6336 | 50 | 16375 | 5280 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 6 | 3275 | 1056 | 0.0013 | 0.000051 | 0.00 | 0.0009 | 0.0012 | 0.00010 | 0.0016 | 0.0055 | 0.000020 | 3.00 | 0.12 | 0.00 | 1.97 | 2.27 | 0.20 | 2.99 | 14.27 | 0.05 | |
| I35_Rmp_SB_29 | 0.23 | 14450 | 3346 | 50 | 12042 | 2789 | 0.00031 | 0.000013 | 0.00 | 0.00019 | 0.00020 | 0.000018 | 0.00025 | 0.0016 | 0.000006 | 2.5 | 2408 | 558 | 0.0027 | 0.000100 | 0.00 | 0.0020 | 0.0025 | 0.00022 | 0.0036 | 0.0107 | 0.000039 | 2.34 | 0.09 | 0.00 | 1.63 | 1.97 | 0.17 | 2.70 | 10.41 | 0.04 | |
| I35_DC_SB_1 | 0.48 | 13950 | 6644 | 55 | 11625 | 5537 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 36 | 2325 | 1107 | 0.0004 | 0.000016 | 0.00 | 0.0002 | 0.0003 | 0.00002 | 0.0003 | 0.0021 | 0.000006 | 2.03 | 0.08 | 0.00 | 1.18 | 1.24 | 0.11 | 1.63 | 9.72 | 0.04 | |
| I35_DC_SB_2 | 0.59 | 21000 | 12398 | 55 | 17500 | 10332 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 3 | 3500 | 2066 | 0.0023 | 0.000086 | 0.00 | 0.0017 | 0.0021 | 0.00019 | 0.0030 | 0.0092 | 0.000034 | 7.73 | 0.30 | 0.00 | 5.24 | 6.23 | 0.55 | 8.61 | 32.80 | 0.12 | |
| I35_DC_SB_3 | 0.42 | 2700 | 1130 | 55 | 2250 | 941 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 25 | 450 | 188 | 0.0005 | 0.000020 | 0.00 | 0.0003 | 0.0004 | 0.00003 | 0.0004 | 0.0030 | 0.000008 | 0.36 | 0.02 | 0.00 | 0.22 | 0.23 | 0.02 | 0.30 | 1.82 | 0.01 | |
| I35_DC_SB_4 | 0.35 | 39550 | 13899 | 55 | 32958 | 11582 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 57 | 6592 | 2317 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 4.04 | 0.17 | 0.00 | 2.32 | 2.40 | 0.22 | 3.17 | 18.45 | 0.07 | |
| I35_DC_SB_5 | 0.25 | 15800 | 3972 | 55 | 13167 | 3310 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 2633 | 662 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 1.16 | 0.05 | 0.00 | 0.67 | 0.69 | 0.06 | 0.91 | 5.30 | 0.02 | |
| I35_DC_SB_6 | 0.22 | 23750 | 5263 | 55 | 19792 | 4386 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 3958 | 877 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 1.53 | 0.06 | 0.00 | 0.88 | 0.92 | 0.08 | 1.20 | 7.02 | 0.03 | |
| I35_DC_SB_7 | 0.19 | 31100 | 5924 | 55 | 25917 | 4936 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 5183 | 987 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 1.72 | 0.07 | 0.00 | 0.99 | 1.03 | 0.09 | 1.36 | 7.90 | 0.03 | |
| I35_DC_SB_8 | 0.42 | 20000 | 8440 | 55 | 16667 | 7033 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 3333 | 1406 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 2.46 | 0.10 | 0.00 | 1.41 | 1.47 | 0.13 | 1.93 | 11.26 | 0.04 | |
| I35_DC_SB_9 | 0.22 | 51100 | 11304 | 55 | 42583 | 9420 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 38 | 8517 | 1884 | 0.0004 | 0.000015 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0020 | 0.000006 | 3.42 | 0.14 | 0.00 | 2.00 | 2.10 | 0.19 | 2.74 | 16.40 | 0.06 | |
| I35_DC_EB_1 | 0.25 | 36150 | 9130 | 55 | 30125 | 7608 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 6025 | 1522 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 2.66 | 0.11 | 0.00 | 1.53 | 1.59 | 0.14 | 2.09 | 12.18 | 0.05 | |
| I35_DC_EB_2 | 0.30 | 52250 | 15767 | 55 | 43542 | 13139 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 8708 | 2628 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 4.59 | 0.19 | 0.00 | 2.64 | 2.74 | 0.25 | 3.61 | 21.04 | 0.08 | |
| I35_DC_EB_3 | 0.34 | 29750 | 10141 | 55 | 24792 | 8451 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 43 | 4958 | 1690 | 0.0003 | 0.000014 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0003 | 0.0019 | 0.000006 | 3.03 | 0.13 | 0.00 | 1.77 | 1.86 | 0.17 | 2.41 | 14.46 | 0.05 | |
| I35_DC_WB_1 | 0.19 | 29500 | 5642 | 55 | 24583 | 4702 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 4917 | 940 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 1.64 | 0.07 | 0.00 | 0.94 | 0.98 | 0.09 | 1.29 | 7.53 | 0.03 | |
| I35_DC_WB_2 | 0.32 | 58100 | 18771 | 55 | 48417 | 15642 | 0.00029 | 0.000012 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00023 | 0.0013 | 0.000005 | 55 | 9683 | 3128 | 0.0003 | 0.000012 | 0.00 | 0.0002 | 0.0002 | 0.00002 | 0.0002 | 0.0013 | 0.000005 | 5.47 | 0.23 | 0.00 | 3.14 | 3.26 | 0.30 | 4.29 | 25.04 | 0.10 | |

| INTERIM - 2032 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | | | Totals | | | | | | | | | | | | | | | |
|-------------------|--------|---------------|----------------|---------------|-------------|---------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|------------|----------|-------------|---------|---------|------------|---------|---------|---------|---------|---------|---------|------|-------|------|---------|---------|---------|---------|---------|---------|---------|---------|---------|------|------|------|------|-------|------|------|-------|------|
| Link Name | Length | 24HR ADT BASE | VMT NonPeak | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | | | | | | | | | | | |
| Northbound_DC_1 | 0.25 | 34323 | 8734 | 50 | 28603 | 7278 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 5721 | 1456 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 5721 | 1456 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 3.52 | 0.19 | 0.01 | 2.41 | 2.21 | 0.22 | 2.71 | 19.37 | 0.08 |
| Northbound_DC_2 | 0.25 | 9960 | 2502 | 50 | 8300 | 2060 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 1660 | 417 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 1660 | 417 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 1.01 | 0.05 | 0.00 | 0.69 | 0.63 | 0.06 | 0.78 | 5.55 | 0.07 |
| Northbound_DC_3 | 0.25 | 24363 | 6176 | 50 | 20303 | 5146 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 4061 | 1029 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 4061 | 1029 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 2.49 | 0.13 | 0.01 | 1.71 | 1.57 | 0.15 | 1.97 | 13.69 | 0.06 |
| Northbound_DC_4 | 0.41 | 14671 | 6023 | 50 | 12301 | 5019 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 2460 | 1004 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 2460 | 1004 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 2.43 | 0.13 | 0.01 | 1.66 | 1.53 | 0.15 | 1.82 | 13.35 | 0.06 |
| Northbound_DC_5 | 0.25 | 6691 | 1701 | 50 | 5576 | 1417 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 1115 | 283 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 1115 | 283 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 0.69 | 0.04 | 0.00 | 0.47 | 0.43 | 0.04 | 0.53 | 3.77 | 0.02 |
| Northbound_DC_6 | 0.28 | 21470 | 5900 | 50 | 17892 | 4925 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 3878 | 985 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 3878 | 985 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 2.38 | 0.13 | 0.01 | 1.63 | 1.50 | 0.15 | 1.84 | 13.10 | 0.06 |
| Northbound_DC_7 | 0.47 | 13138 | 6153 | 50 | 10948 | 5128 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 2199 | 1016 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 50 | 2199 | 1016 | 0.00040 | 0.00002 | 0.00001 | 0.00028 | 0.00025 | 0.00025 | 0.00031 | 0.00022 | 0.00009 | 2.48 | 0.13 | 0.01 | 1.70 | 1.56 | 0.15 | 1.91 | 13.64 | 0.06 |
| Northbound_RMP_1 | 0.25 | 10317 | 2534 | 40 | 8598 | 2112 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 21 | 1720 | 422 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 21 | 1720 | 422 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 1.27 | 0.07 | 0.00 | 0.89 | 0.84 | 0.08 | 1.05 | 7.59 | 0.03 |
| Northbound_RMP_2 | 0.49 | 14403 | 7069 | 40 | 12003 | 5891 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 48 | 2401 | 1178 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 48 | 2401 | 1178 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 2.23 | 0.17 | 0.01 | 2.23 | 2.07 | 0.20 | 2.57 | 17.88 | 0.07 |
| Northbound_RMP_3 | 0.14 | 24568 | 3402 | 40 | 20473 | 2835 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 48 | 4095 | 567 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 48 | 4095 | 567 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 1.07 | 0.08 | 0.01 | 1.07 | 1.00 | 0.10 | 1.24 | 9.04 | 0.04 |
| Northbound_RMP_4 | 0.27 | 7508 | 2015 | 40 | 6257 | 1679 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 39 | 1251 | 336 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 39 | 1251 | 336 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.54 | 0.05 | 0.00 | 0.65 | 0.60 | 0.06 | 0.75 | 5.50 | 0.02 |
| Northbound_RMP_5 | 0.18 | 4341 | 787 | 40 | 3618 | 656 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 42 | 724 | 131 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 42 | 724 | 131 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.36 | 0.02 | 0.00 | 0.25 | 0.23 | 0.02 | 0.29 | 2.13 | 0.01 |
| Northbound_RMP_7 | 0.16 | 17570 | 2804 | 40 | 14642 | 2337 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 10 | 2928 | 467 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 10 | 2928 | 467 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 1.18 | 0.12 | 0.01 | 1.18 | 1.12 | 0.11 | 1.44 | 9.00 | 0.04 |
| Northbound_RMP_8 | 0.06 | 5108 | 294 | 40 | 4256 | 245 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 19 | 851 | 49 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 19 | 851 | 49 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.15 | 0.01 | 0.00 | 0.11 | 0.10 | 0.01 | 0.13 | 0.89 | 0.00 |
| Northbound_RMP_9 | 0.08 | 20379 | 1683 | 40 | 16983 | 1403 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 35 | 3397 | 281 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 35 | 3397 | 281 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.79 | 0.04 | 0.00 | 0.55 | 0.51 | 0.05 | 0.64 | 4.65 | 0.02 |
| Northbound_RMP_10 | 0.11 | 26049 | 2803 | 40 | 21707 | 2336 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 36 | 4341 | 467 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 36 | 4341 | 467 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 1.31 | 0.07 | 0.00 | 0.91 | 0.85 | 0.08 | 1.06 | 7.71 | 0.03 |
| Northbound_RMP_11 | 0.26 | 40044 | 10458 | 40 | 33370 | 8715 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 49 | 6674 | 1743 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 49 | 6674 | 1743 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 3.29 | 0.36 | 0.30 | 3.79 | 27.68 | 0.11 | | | |
| Northbound_RMP_12 | 0.37 | 6231 | 2334 | 40 | 5193 | 1945 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 44 | 1039 | 389 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 44 | 1039 | 389 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 1.07 | 0.06 | 0.00 | 0.74 | 0.69 | 0.07 | 0.86 | 6.29 | 0.03 |
| Northbound_RMP_13 | 0.27 | 28575 | 7780 | 40 | 23813 | 6484 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 12 | 4763 | 1297 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 12 | 4763 | 1297 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 3.12 | 0.29 | 0.29 | 3.77 | 24.61 | 0.10 | | | |
| Northbound_RMP_14 | 0.38 | 5930 | 2272 | 40 | 4941 | 1893 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 20 | 988 | 379 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 20 | 988 | 379 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.81 | 0.76 | 0.07 | 0.96 | 6.83 | 0.03 | | | |
| Northbound_RMP_15 | 0.32 | 2300 | 732 | 40 | 1917 | 613 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 46 | 383 | 122 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 46 | 383 | 122 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.23 | 0.22 | 0.02 | 0.27 | 1.97 | 0.01 | | | |
| Northbound_RMP_16 | 0.08 | 21623 | 1688 | 40 | 18019 | 1406 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 15 | 3604 | 281 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 15 | 3604 | 281 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.91 | 0.05 | 0.00 | 0.64 | 0.61 | 0.06 | 0.77 | 5.25 | 0.02 |
| Northbound_RMP_17 | 0.09 | 11400 | 2009 | 40 | 9500 | 841 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 19 | 1900 | 168 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 19 | 1900 | 168 | 0.00046 | 0.00002 | 0.00002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.00027 | 0.00010 | 0.52 | 0.03 | 0.00 | 0.36 | 0.34 | 0.03 | 0.43 | 3.05 | 0.01 |
| Northbound_RMP_18 | 0.18 | 17023 | 3119 | 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| INTERIM - 2032 | | | | | | | Inputs NonPeak | | | | | | | | | | | | | | Rates NonPeak | | | | | | | | | | | | | | Inputs Peak | | | | | | | | | | | | | | Rates Peak | | | | | | | | | | | | | | Totals | | | | | | | | | | | | | |
|------------------|--------|---------------|----------|---------------|-------------|-------------|----------------|---------|----------|---------|---------|---------|---------|--------|----------|------------|----------|----------|---------|---------|---------------|---------|---------|----------|---------|---------|----------|-------|-------|------|-------|-------|-------|-------|-------------|------|------|-------|------|------|------|-------|------|-----|-----|--|--|--|------------|--|--|--|--|--|--|--|--|--|--|--|--|--|--------|--|--|--|--|--|--|--|--|--|--|--|--|--|
| Link Name | Length | 24HR ADT Base | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_ML_4 | 2.60 | 17366 | 45190 | 60 | 14472 | 37660 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 5 | 2894 | 7531 | 0.00343 | 0.00019 | 0.00016 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_ML_5 | 0.94 | 23617 | 22160 | 60 | 19681 | 18466 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 54 | 3936 | 3693 | 0.00039 | 0.00019 | 0.00001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_ML_6 | 0.87 | 25917 | 22461 | 60 | 21598 | 18718 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 54 | 4320 | 3744 | 0.00039 | 0.00019 | 0.00001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_ML_7 | 1.91 | 8895 | 16949 | 60 | 7412 | 14124 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 21 | 1482 | 2824 | 0.00071 | 0.00002 | 0.000002 | 0.00051 | 0.00049 | 0.00047 | 0.00064 | 0.00015 | 0.000015 | 7.18 | 0.38 | 0.02 | 4.81 | 4.36 | 0.43 | 5.58 | 36.70 | 0.19 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_1 | 0.27 | 51382 | 11393 | 60 | 42819 | 11494 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 67 | 8564 | 2299 | 0.00037 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_2 | 0.65 | 61700 | 40176 | 60 | 51416 | 33430 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 63 | 10283 | 6286 | 0.00037 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_3 | 0.27 | 83132 | 22354 | 60 | 69293 | 18628 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 56 | 13859 | 3726 | 0.00038 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_4 | 0.35 | 95844 | 20687 | 60 | 48920 | 17224 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 21 | 9764 | 3445 | 0.00071 | 0.00002 | 0.000002 | 0.00051 | 0.00049 | 0.00047 | 0.00064 | 0.00015 | 0.000015 | 7.28 | 0.44 | 0.03 | 5.38 | 4.76 | 0.47 | 6.04 | 39.16 | 0.19 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_5 | 0.28 | 72988 | 20232 | 60 | 60823 | 18680 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 43 | 12165 | 3772 | 0.00044 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_6 | 0.67 | 65479 | 43951 | 60 | 54566 | 36626 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 21 | 10913 | 7325 | 0.00071 | 0.00004 | 0.000002 | 0.00051 | 0.00049 | 0.00047 | 0.00064 | 0.00015 | 0.000015 | 18.62 | 0.99 | 0.06 | 12.47 | 11.32 | 1.11 | 14.48 | 95.41 | 0.42 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_7 | 0.05 | 60372 | 2760 | 60 | 50310 | 2300 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 35 | 10062 | 460 | 0.00051 | 0.00003 | 0.000002 | 0.00035 | 0.00032 | 0.00031 | 0.00041 | 0.00040 | 0.00015 | 1.08 | 0.06 | 0.00 | 1.71 | 1.63 | 0.06 | 0.81 | 5.35 | 0.02 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_8 | 0.70 | 39992 | 28142 | 60 | 33327 | 23451 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 8 | 6665 | 4690 | 0.00138 | 0.00007 | 0.000006 | 0.00108 | 0.00108 | 0.00104 | 0.00148 | 0.00064 | 0.000029 | 15.10 | 0.81 | 0.05 | 10.66 | 10.02 | 0.98 | 13.43 | 70.68 | 0.34 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_9 | 0.86 | 66641 | 56983 | 60 | 55034 | 47486 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 55 | 11007 | 9497 | 0.00038 | 0.00007 | 0.000002 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_10 | 0.33 | 41780 | 13983 | 60 | 34817 | 11652 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 2.5 | 6963 | 2330 | 0.00343 | 0.00019 | 0.00016 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_11 | 0.33 | 41824 | 13983 | 60 | 34817 | 11652 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 40 | 13637 | 4548 | 0.00046 | 0.00019 | 0.00016 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_12 | 0.51 | 76566 | 38262 | 60 | 63047 | 31885 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 2.5 | 12609 | 6377 | 0.00343 | 0.00019 | 0.00016 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_13 | 0.84 | 104232 | 87886 | 60 | 86860 | 73239 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 4 | 17372 | 14648 | 0.00232 | 0.00013 | 0.00011 | 0.00192 | 0.00198 | 0.00190 | 0.00279 | 0.0102 | 0.000049 | 60.88 | 3.28 | 0.24 | 45.56 | 44.48 | 4.41 | 60.49 | 276.93 | 1.35 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_14 | 1.51 | 79388 | 120242 | 60 | 66156 | 100201 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 56 | 13231 | 2040 | 0.00038 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_15 | 0.26 | 116296 | 30152 | 60 | 96913 | 25126 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 55 | 19383 | 5025 | 0.00038 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_16 | 0.46 | 100318 | 46958 | 60 | 85965 | 39131 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 55 | 17193 | 7826 | 0.00038 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_17 | 0.43 | 93139 | 40933 | 60 | 77616 | 33495 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 33 | 15523 | 6829 | 0.00053 | 0.00003 | 0.000002 | 0.00037 | 0.00035 | 0.00034 | 0.00044 | 0.00033 | 0.000012 | 15.82 | 0.84 | 0.05 | 10.48 | 9.41 | 0.92 | 11.70 | 80.18 | 0.36 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Northbound_GP_18 | 0.28 | 18339 | 5987 | 60 | 77616 | 33495 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 54 | 15523 | 3164 | 0.00039 | 0.00004 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_1 | 0.11 | 2965 | 458 | 45 | 2471 | 381 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 10 | 494 | 76 | 0.00096 | 0.00005 | 0.000004 | 0.00071 | 0.00070 | 0.00067 | 0.00092 | 0.00052 | 0.00020 | 0.24 | 0.01 | 0.00 | 0.17 | 0.16 | 0.02 | 0.70 | 1.36 | 0.01 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_2 | 0.28 | 28218 | 7964 | 45 | 23515 | 6636 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 10 | 4703 | 1327 | 0.00120 | 0.00005 | 0.000005 | 0.00091 | 0.00090 | 0.00087 | 0.00122 | 0.00057 | 0.00025 | 4.43 | 0.24 | 0.02 | 3.20 | 3.05 | 0.30 | 3.87 | 24.35 | 0.10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_3 | 0.46 | 29087 | 13269 | 45 | 24239 | 11057 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 4 | 4848 | 2212 | 0.00232 | 0.00013 | 0.00011 | 0.00192 | 0.00198 | 0.00190 | 0.00279 | 0.0102 | 0.000049 | 9.87 | 0.53 | 0.04 | 7.56 | 7.48 | 7.32 | 9.92 | 50.68 | 0.22 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_4 | 0.22 | 46927 | 10421 | 45 | 39106 | 8684 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 18 | 7821 | 1737 | 0.00079 | 0.00004 | 0.000003 | 0.00098 | 0.00098 | 0.00094 | 0.00122 | 0.00057 | 0.00025 | 4.43 | 0.24 | 0.02 | 3.20 | 3.05 | 0.30 | 3.87 | 24.35 | 0.10 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_5 | 0.31 | 18863 | 5914 | 45 | 15719 | 4928 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 51 | 3144 | 986 | 0.00040 | 0.00002 | 0.000001 | 0.00028 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 39.63 | 2.13 | 0.17 | 30.76 | 30.81 | 2.97 | 42.83 | 179.25 | 0.87 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_6 | 0.25 | 5772 | 1440 | 45 | 4810 | 1200 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 3 | 962 | 240 | 0.00293 | 0.00016 | 0.00014 | 0.00246 | 0.00257 | 0.000246 | 0.00366 | 0.0030 | 0.00062 | 1.22 | 0.07 | 0.01 | 0.95 | 0.95 | 0.09 | 1.28 | 6.15 | 0.03 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_7 | 0.42 | 23801 | 10115 | 45 | 19834 | 8429 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 4 | 3967 | 1686 | 0.00232 | 0.00013 | 0.00011 | 0.00192 | 0.00198 | 0.00190 | 0.00279 | 0.0102 | 0.000049 | 7.52 | 0.41 | 0.03 | 5.76 | 5.70 | 5.57 | 7.57 | 38.64 | 0.17 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Southbound_CD_8 | 0.33 | 54089 | 17955 | 45 | 45075 | 14825 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.00010 | 21 | 9015 | 2965 | 0.00071 | 0.00004 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

| INTERIM - 2032 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | | Totals | | | | | | | | |
|-------------------|--------|---------------|----------------|-------------|-------------|---------------|---------|---------|----------|---------|---------|---------|---------|--------|------------|-------------|----------|-------|------------|---------|----------|---------|---------|----------|---------|--------|----------|----------|--------|------|-------|-------|------|-------|--------|-------|------|
| Link Name | Length | 24HR ADT BASE | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | | |
| Southbound_GP_2 | 0.22 | 104589 | 22676 | 60 | 87158 | 18897 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 16 | 17432 | 3779 | 0.00088 | 0.00005 | 0.000003 | 0.00064 | 0.00063 | 0.00060 | 0.00082 | 0.0049 | 0.000018 | 10.25 | 0.54 | 0.03 | 6.94 | 6.35 | 0.62 | 8.15 | 51.35 | 0.23 | |
| Southbound_GP_3 | 0.73 | 110161 | 80482 | 60 | 91801 | 67068 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 10 | 18360 | 13413 | 0.00120 | 0.00006 | 0.000005 | 0.00091 | 0.00090 | 0.00087 | 0.00122 | 0.0057 | 0.000025 | 40.66 | 2.17 | 0.14 | 28.20 | 26.22 | 2.55 | 34.35 | 192.30 | 0.91 | |
| Southbound_GP_4 | 0.70 | 67477 | 47145 | 60 | 56231 | 39288 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 29 | 11246 | 7857 | 0.00057 | 0.00003 | 0.000002 | 0.00042 | 0.00040 | 0.00039 | 0.00049 | 0.0039 | 0.000013 | 18.93 | 1.01 | 0.06 | 12.64 | 11.44 | 1.12 | 14.39 | 99.01 | 0.43 | |
| Southbound_GP_5 | 0.76 | 67477 | 51564 | 60 | 56231 | 42970 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 4 | 11246 | 8594 | 0.00232 | 0.00013 | 0.000011 | 0.00192 | 0.00198 | 0.000190 | 0.00279 | 0.0102 | 0.000049 | 35.72 | 1.92 | 0.14 | 26.73 | 26.10 | 2.53 | 35.49 | 162.48 | 0.79 | |
| Southbound_GP_6 | 0.83 | 89867 | 74355 | 60 | 74889 | 61945 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 10 | 14978 | 12389 | 0.00120 | 0.00006 | 0.000005 | 0.00091 | 0.00090 | 0.00087 | 0.00122 | 0.0057 | 0.000025 | 37.56 | 2.00 | 0.13 | 26.05 | 24.22 | 2.36 | 31.73 | 177.61 | 0.84 | |
| Southbound_GP_7 | 0.36 | 73253 | 26238 | 60 | 61045 | 21865 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 8 | 12209 | 4373 | 0.00138 | 0.00007 | 0.000006 | 0.00108 | 0.00108 | 0.00104 | 0.00148 | 0.0064 | 0.000029 | 14.08 | 0.75 | 0.05 | 9.94 | 9.35 | 0.91 | 12.35 | 65.90 | 0.31 | |
| Southbound_GP_8 | 0.57 | 55162 | 31489 | 60 | 45968 | 26241 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 56 | 9194 | 5248 | 0.00038 | 0.00002 | 0.000001 | 0.00025 | 0.00023 | 0.00021 | 0.00028 | 0.0018 | 0.000028 | 11.63 | 0.62 | 0.04 | 7.57 | 6.78 | 0.66 | 8.51 | 55.17 | 0.27 | |
| Southbound_GP_9 | 0.66 | 75541 | 49681 | 60 | 62951 | 41401 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 57 | 12590 | 8280 | 0.00038 | 0.00002 | 0.000001 | 0.00025 | 0.00023 | 0.00021 | 0.00028 | 0.0018 | 0.000028 | 18.32 | 0.97 | 0.06 | 11.93 | 10.55 | 1.04 | 13.59 | 86.81 | 0.43 | |
| Southbound_GP_10 | 1.07 | 42444 | 45429 | 60 | 35270 | 37858 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 8 | 7074 | 7572 | 0.00138 | 0.00007 | 0.000006 | 0.00108 | 0.00108 | 0.00104 | 0.00148 | 0.0064 | 0.000029 | 18.38 | 1.30 | 0.09 | 17.21 | 16.18 | 1.57 | 21.38 | 114.11 | 0.54 | |
| Southbound_GP_11 | 0.75 | 80751 | 60689 | 60 | 67293 | 50575 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 3 | 13459 | 10115 | 0.00293 | 0.00016 | 0.000014 | 0.00246 | 0.00257 | 0.000246 | 0.00366 | 0.0130 | 0.000062 | 48.26 | 2.60 | 0.20 | 36.94 | 36.65 | 3.54 | 50.52 | 218.74 | 1.06 | |
| Southbound_GP_12 | 0.35 | 107222 | 34938 | 60 | 83935 | 29115 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 56 | 16787 | 5823 | 0.00038 | 0.00002 | 0.000001 | 0.00025 | 0.00022 | 0.00022 | 0.00028 | 0.0130 | 0.000028 | 12.90 | 0.68 | 0.04 | 8.40 | 7.43 | 0.73 | 9.44 | 61.28 | 0.31 | |
| Southbound_GP_13 | 0.49 | 88055 | 43508 | 60 | 73379 | 36257 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 53 | 14676 | 7251 | 0.00039 | 0.00002 | 0.000001 | 0.00026 | 0.00024 | 0.00023 | 0.00030 | 0.0020 | 0.000009 | 16.15 | 0.86 | 0.05 | 10.55 | 9.36 | 0.92 | 11.85 | 77.39 | 0.37 | |
| Southbound_GP_14 | 0.17 | 102867 | 17153 | 60 | 85722 | 14294 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 55 | 17144 | 2859 | 0.00038 | 0.00002 | 0.000001 | 0.00025 | 0.00023 | 0.00022 | 0.00022 | 0.0029 | 0.0029 | 0.000009 | 6.34 | 0.34 | 0.02 | 4.13 | 3.66 | 0.36 | 4.65 | 30.14 | 0.15 |
| Southbound_GP_15 | 0.62 | 67676 | 42198 | 60 | 56396 | 35164 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 65 | 11279 | 7033 | 0.00036 | 0.00002 | 0.000001 | 0.00024 | 0.00022 | 0.00021 | 0.00026 | 0.0018 | 0.000009 | 15.47 | 0.82 | 0.05 | 10.09 | 8.95 | 0.88 | 11.25 | 73.69 | 0.36 | |
| Southbound_GP_16 | 0.28 | 37337 | 10541 | 60 | 31114 | 8784 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00021 | 0.00021 | 0.00027 | 0.0017 | 0.000009 | 63 | 6223 | 1757 | 0.00037 | 0.00002 | 0.000001 | 0.00024 | 0.00022 | 0.00021 | 0.00026 | 0.0018 | 0.000009 | 3.87 | 0.21 | 0.01 | 2.52 | 2.23 | 0.22 | 2.82 | 18.36 | 0.09 | |
| Southbound_RMP_1 | 0.14 | 21010 | 2936 | 40 | 17508 | 2446 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 49 | 3502 | 489 | 0.00041 | 0.00002 | 0.000001 | 0.00028 | 0.00026 | 0.00025 | 0.00032 | 0.0023 | 0.000009 | 1.33 | 0.07 | 0.00 | 0.92 | 0.86 | 0.08 | 1.06 | 7.77 | 0.03 | |
| Southbound_RMP_2 | 0.21 | 11042 | 2314 | 40 | 9201 | 1928 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 52 | 1840 | 386 | 0.00039 | 0.00002 | 0.000001 | 0.00027 | 0.00024 | 0.00024 | 0.00030 | 0.0020 | 0.000009 | 1.04 | 0.06 | 0.00 | 0.72 | 0.67 | 0.07 | 0.83 | 6.05 | 0.02 | |
| Southbound_RMP_3 | 0.30 | 11962 | 3563 | 40 | 9968 | 2969 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 49 | 1994 | 594 | 0.00041 | 0.00002 | 0.000001 | 0.00028 | 0.00026 | 0.00025 | 0.00032 | 0.0023 | 0.000009 | 1.61 | 0.09 | 0.01 | 1.12 | 1.04 | 0.10 | 1.29 | 9.43 | 0.04 | |
| Southbound_RMP_4 | 0.31 | 12831 | 4003 | 40 | 10692 | 3335 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 9 | 2138 | 667 | 0.00128 | 0.00007 | 0.000005 | 0.00099 | 0.00098 | 0.00095 | 0.00134 | 0.0060 | 0.000027 | 2.39 | 0.13 | 0.01 | 1.73 | 1.65 | 0.16 | 2.13 | 13.07 | 0.05 | |
| Southbound_RMP_5 | 0.28 | 18403 | 5164 | 40 | 15336 | 4303 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 40 | 3067 | 861 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 2.39 | 0.13 | 0.01 | 1.66 | 1.54 | 0.15 | 1.92 | 14.05 | 0.05 | |
| Southbound_RMP_6 | 0.18 | 42684 | 7502 | 40 | 35570 | 6252 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 29 | 7114 | 1250 | 0.00057 | 0.00003 | 0.000002 | 0.00042 | 0.00040 | 0.00039 | 0.00049 | 0.0039 | 0.000013 | 3.60 | 0.19 | 0.01 | 2.53 | 2.37 | 0.23 | 2.94 | 21.92 | 0.08 | |
| Southbound_RMP_7 | 0.18 | 15540 | 2818 | 40 | 12950 | 2348 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 37 | 2590 | 470 | 0.00049 | 0.00003 | 0.000002 | 0.00044 | 0.00041 | 0.00039 | 0.00040 | 0.0029 | 0.000011 | 1.31 | 0.07 | 0.00 | 0.91 | 0.85 | 0.08 | 1.06 | 7.73 | 0.03 | |
| Southbound_RMP_8 | 0.04 | 17841 | 632 | 40 | 14887 | 527 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 9 | 2973 | 105 | 0.00128 | 0.00007 | 0.000005 | 0.00099 | 0.00098 | 0.00095 | 0.00134 | 0.0060 | 0.000027 | 0.38 | 0.02 | 0.00 | 0.27 | 0.26 | 0.03 | 0.34 | 2.06 | 0.01 | |
| Southbound_RMP_9 | 0.27 | 22390 | 6049 | 40 | 18658 | 5040 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 11 | 3732 | 1008 | 0.00112 | 0.00006 | 0.000004 | 0.00085 | 0.00084 | 0.00081 | 0.00113 | 0.0055 | 0.000024 | 2.46 | 0.19 | 0.01 | 2.47 | 2.35 | 0.23 | 3.01 | 19.26 | 0.08 | |
| Southbound_RMP_10 | 0.09 | 24537 | 2106 | 40 | 20448 | 1755 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 16 | 4090 | 351 | 0.00088 | 0.00005 | 0.000003 | 0.00064 | 0.00063 | 0.00060 | 0.00082 | 0.0049 | 0.000018 | 1.12 | 0.06 | 0.00 | 0.79 | 0.74 | 0.07 | 0.94 | 6.50 | 0.02 | |
| Southbound_RMP_11 | 0.15 | 1482 | 220 | 40 | 1235 | 184 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 3 | 247 | 37 | 0.00293 | 0.00016 | 0.000014 | 0.00246 | 0.00257 | 0.000246 | 0.00366 | 0.0130 | 0.000062 | 0.19 | 0.01 | 0.00 | 0.15 | 0.15 | 0.01 | 0.20 | 0.98 | 0.00 | |
| Southbound_RMP_12 | 0.08 | 16614 | 1379 | 40 | 13845 | 1149 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 45 | 2769 | 230 | 0.00043 | 0.00002 | 0.000001 | 0.00030 | 0.00028 | 0.00027 | 0.00034 | 0.0025 | 0.000010 | 0.63 | 0.03 | 0.00 | 0.44 | 0.41 | 0.04 | 0.51 | 3.71 | 0.01 | |
| Southbound_RMP_13 | 0.22 | 10888 | 2446 | 40 | 9074 | 2039 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 6 | 1815 | 408 | 0.00170 | 0.00005 | 0.000007 | 0.00136 | 0.00139 | 0.00133 | 0.00192 | 0.0076 | 0.000036 | 1.64 | 0.09 | 0.01 | 1.21 | 1.18 | 0.11 | 1.54 | 8.66 | 0.04 | |
| Southbound_RMP_14 | 0.13 | 18030 | 2294 | 40 | 15025 | 1912 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 2.5 | 3005 | 382 | 0.00343 | 0.00019 | 0.000016 | 0.00289 | 0.00304 | 0.000291 | 0.00435 | 0.0151 | 0.000073 | 2.19 | 0.12 | 0.01 | 1.72 | 1.73 | 0.17 | 2.37 | 10.99 | 0.05 | |
| Southbound_RMP_15 | 0.30 | 20379 | 6166 | 40 | 16983 | 5139 | 0.00046 | 0.00002 | 0.000002 | 0.00032 | 0.00030 | 0.00029 | 0.00037 | 0.0027 | 0.000010 | 42 | 3397 | 1028 | 0.00045 | 0.00002 | 0.000001 | 0.00031 | 0.00029 | 0.00028 | 0.00036 | 0.0026 | 0.000010 | 2.83 | 0.15 | 0.01 | 1.97 | 1.84 | 0.18 | 2.28 | | | |

| Design - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | Totals | | | | | | | | | |
|-------------------|--------|-----------------------|-------------|------------------|---------------|----------------|---------------|---------|------|---------|---------|---------|---------|--------|---------|---------------|-------------|-------------|---------|------------|------|---------|---------|----------|---------|---------|----------|-------|-------|------|------|-------|-------|-------|-------|------|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NoPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM |
| Northbound_DC_1 | 0.25 | 54700 | 13919 | 50 | 45583 | 11599 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 59 | 9117 | 2320 | 0.00028 | 0.00001 | 0.00 | 0.00016 | 0.00016 | 0.000015 | 0.00002 | 0.00013 | 0.000005 | 4.21 | 0.18 | 0.00 | 2.53 | 2.69 | 0.24 | 3.40 | 21.40 | 0.08 |
| Northbound_DC_2 | 0.25 | 20350 | 5112 | 50 | 16958 | 4260 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 55 | 3392 | 852 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00002 | 0.00013 | 0.000005 | 1.55 | 0.06 | 0.00 | 0.94 | 1.00 | 0.09 | 1.26 | 7.93 | 0.03 |
| Northbound_DC_3 | 0.25 | 34350 | 8707 | 50 | 28625 | 7256 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 55 | 5725 | 1451 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00002 | 0.00013 | 0.000005 | 2.65 | 0.11 | 0.00 | 1.50 | 1.60 | 0.15 | 2.15 | 13.51 | 0.05 |
| Northbound_DC_4 | 0.41 | 21150 | 8630 | 50 | 17625 | 7191 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 55 | 3525 | 1438 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00002 | 0.00013 | 0.000005 | 2.62 | 0.11 | 0.00 | 1.68 | 1.79 | 0.15 | 2.13 | 13.39 | 0.05 |
| Northbound_DC_5 | 0.25 | 9500 | 2415 | 50 | 7917 | 2012 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 55 | 1583 | 402 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.000016 | 0.00002 | 0.00013 | 0.000005 | 0.73 | 0.03 | 0.00 | 0.44 | 0.47 | 0.04 | 0.59 | 3.75 | 0.01 |
| Northbound_DC_6 | 0.28 | 30650 | 8436 | 50 | 25542 | 7030 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 55 | 5108 | 1406 | 0.00267 | 0.00010 | 0.00 | 0.00020 | 0.00024 | 0.000024 | 0.00006 | 0.0107 | 0.000039 | 5.91 | 0.23 | 0.00 | 4.12 | 4.97 | 0.44 | 6.81 | 26.24 | 0.09 |
| Northbound_DC_7 | 0.47 | 16900 | 7915 | 50 | 14083 | 6596 | 0.00031 | 0.00013 | 0.00 | 0.00019 | 0.00020 | 0.00018 | 0.00025 | 0.0016 | 0.00006 | 17 | 2817 | 1319 | 0.00063 | 0.00003 | 0.00 | 0.00042 | 0.00049 | 0.000043 | 0.00006 | 0.00035 | 0.000010 | 2.85 | 0.12 | 0.00 | 1.79 | 1.96 | 0.18 | 2.48 | 15.16 | 0.05 |
| Northbound_RMP_1 | 0.25 | 13650 | 3353 | 40 | 11375 | 2794 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 5 | 2275 | 559 | 0.00151 | 0.00006 | 0.00 | 0.00109 | 0.00135 | 0.00010 | 0.00019 | 0.00062 | 0.000023 | 1.82 | 0.07 | 0.00 | 1.22 | 1.42 | 0.13 | 1.88 | 9.98 | 0.03 |
| Northbound_RMP_2 | 0.49 | 17750 | 8712 | 40 | 14792 | 7260 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 2958 | 1452 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 6.42 | 0.25 | 0.00 | 4.49 | 5.42 | 0.48 | 7.40 | 29.82 | 0.10 |
| Northbound_RMP_3 | 0.14 | 29700 | 4113 | 40 | 24750 | 3427 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 3 | 4950 | 685 | 0.00228 | 0.00009 | 0.00 | 0.00170 | 0.00214 | 0.000189 | 0.00030 | 0.0092 | 0.000034 | 2.77 | 0.11 | 0.00 | 1.91 | 2.29 | 0.20 | 3.10 | 13.06 | 0.04 |
| Northbound_RMP_4 | 0.27 | 10950 | 2938 | 40 | 9125 | 2448 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 1825 | 490 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 2.17 | 0.08 | 0.00 | 1.51 | 1.83 | 0.16 | 2.50 | 10.06 | 0.03 |
| Northbound_RMP_6 | 0.18 | 5300 | 960 | 40 | 4417 | 800 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 883 | 160 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 0.71 | 0.03 | 0.00 | 0.49 | 0.60 | 0.05 | 0.82 | 3.29 | 0.01 |
| Northbound_RMP_7 | 0.16 | 25100 | 4013 | 40 | 20958 | 3344 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 3 | 4192 | 669 | 0.00228 | 0.00009 | 0.00 | 0.00170 | 0.00214 | 0.000189 | 0.00030 | 0.0092 | 0.000034 | 2.70 | 0.11 | 0.00 | 1.87 | 2.23 | 0.20 | 3.02 | 12.74 | 0.04 |
| Northbound_RMP_8 | 0.06 | 6200 | 357 | 40 | 5167 | 297 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 1033 | 59 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 0.26 | 0.01 | 0.00 | 0.18 | 0.22 | 0.02 | 0.30 | 1.22 | 0.00 |
| Northbound_RMP_9 | 0.08 | 22150 | 1829 | 40 | 18458 | 1524 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 3692 | 305 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 1.35 | 0.05 | 0.00 | 0.94 | 1.14 | 0.10 | 1.55 | 6.26 | 0.02 |
| Northbound_RMP_10 | 0.11 | 31900 | 3432 | 40 | 26583 | 2860 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 38 | 5317 | 372 | 0.00036 | 0.00002 | 0.00 | 0.00023 | 0.00025 | 0.000022 | 0.00003 | 0.0020 | 0.000006 | 1.21 | 0.05 | 0.00 | 0.75 | 0.82 | 0.07 | 1.04 | 6.80 | 0.02 |
| Northbound_RMP_11 | 0.26 | 48800 | 12745 | 40 | 40667 | 10621 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 8133 | 2124 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 9.40 | 0.37 | 0.00 | 6.57 | 7.93 | 0.70 | 10.82 | 43.63 | 0.15 |
| Northbound_RMP_12 | 0.37 | 7500 | 2810 | 40 | 6250 | 2341 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 1250 | 468 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 2.07 | 0.08 | 0.00 | 1.45 | 1.75 | 0.16 | 2.39 | 9.62 | 0.03 |
| Northbound_RMP_13 | 0.27 | 34800 | 9475 | 40 | 29000 | 7896 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 12 | 5800 | 1579 | 0.00080 | 0.00003 | 0.00 | 0.00055 | 0.00065 | 0.000058 | 0.00030 | 0.0040 | 0.000013 | 4.03 | 0.17 | 0.00 | 2.59 | 2.91 | 0.26 | 3.72 | 21.81 | 0.07 |
| Northbound_RMP_14 | 0.38 | 7250 | 2778 | 40 | 6042 | 2315 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 2.5 | 1208 | 463 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 2.05 | 0.08 | 0.00 | 1.43 | 1.73 | 0.15 | 2.36 | 9.51 | 0.03 |
| Northbound_RMP_15 | 0.32 | 2750 | 879 | 40 | 2292 | 733 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 38 | 458 | 146 | 0.00036 | 0.00002 | 0.00 | 0.00023 | 0.00025 | 0.000022 | 0.00003 | 0.0020 | 0.000006 | 0.31 | 0.01 | 0.00 | 0.19 | 0.21 | 0.02 | 0.27 | 1.74 | 0.01 |
| Northbound_RMP_16 | 0.08 | 26650 | 2080 | 40 | 22208 | 1733 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 13 | 4442 | 347 | 0.00076 | 0.00003 | 0.00 | 0.00052 | 0.00061 | 0.000054 | 0.00039 | 0.00012 | 0.000012 | 0.87 | 0.04 | 0.00 | 0.56 | 0.63 | 0.06 | 0.80 | 4.76 | 0.01 |
| Northbound_RMP_17 | 0.09 | 13450 | 1190 | 40 | 11208 | 992 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 8 | 2242 | 198 | 0.00106 | 0.00004 | 0.00 | 0.00074 | 0.00090 | 0.000080 | 0.00012 | 0.0047 | 0.000016 | 0.56 | 0.02 | 0.00 | 0.36 | 0.41 | 0.04 | 0.54 | 2.88 | 0.01 |
| Northbound_RMP_18 | 0.18 | 20750 | 3801 | 40 | 17292 | 3168 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 44 | 3458 | 634 | 0.00033 | 0.00001 | 0.00 | 0.00021 | 0.00023 | 0.000020 | 0.00003 | 0.0019 | 0.000006 | 1.32 | 0.06 | 0.00 | 0.82 | 0.90 | 0.08 | 1.13 | 7.42 | 0.02 |
| Northbound_RMP_19 | 0.18 | 46950 | 8620 | 40 | 39125 | 7183 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 38 | 7825 | 1437 | 0.00036 | 0.00002 | 0.00 | 0.00023 | 0.00025 | 0.000022 | 0.00003 | 0.0020 | 0.000006 | 3.04 | 0.13 | 0.00 | 1.89 | 2.07 | 0.19 | 2.60 | 17.08 | 0.05 |
| Northbound_RMP_20 | 0.17 | 12000 | 2080 | 40 | 10000 | 1734 | 0.00035 | 0.00015 | 0.00 | 0.00022 | 0.00024 | 0.00021 | 0.00030 | 0.0020 | 0.00006 | 21 | 2000 | 347 | 0.00053 | 0.00002 | 0.00 | 0.00035 | 0.00040 | 0.000036 | 0.00003 | 0.00009 | 0.000009 | 0.79 | 0.03 | 0.00 | 0.50 | 0.55 | 0.05 | 0.70 | 4.52 | 0.01 |
| Northbound_CD_1 | 0.39 | 47300 | 18454 | 45 | 39417 | 15378 | 0.00033 | 0.00014 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.00027 | 0.0018 | 0.00006 | 2.5 | 7883 | 3076 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 13.23 | 0.52 | 0.00 | 9.30 | 11.24 | 1.00 | 15.27 | 61.06 | 0.21 |
| Northbound_CD_2 | 0.23 | 46500 | 10719 | 45 | 38750 | 8932 | 0.00033 | 0.00014 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.00027 | 0.0018 | 0.00006 | 2.5 | 7750 | 1786 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 7.68 | 0.30 | 0.00 | 5.40 | 6.53 | 0.56 | 8.87 | 35.47 | 0.12 |
| Northbound_CD_3 | 0.33 | 31400 | 10329 | 45 | 26167 | 8608 | 0.00033 | 0.00014 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.00027 | 0.0018 | 0.00006 | 2.5 | 5233 | 1721 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 7.40 | 0.29 | 0.00 | 5.20 | 6.29 | 0.56 | 8.55 | 34.18 | 0.12 |
| Northbound_CD_4 | 0.43 | 29600 | 12836 | 45 | 24667 | 10697 | 0.00033 | 0.00014 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.00027 | 0.0018 | 0.00006 | 2.5 | 4933 | 2139 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.000224 | 0.00036 | 0.0107 | 0.000039 | 9.20 | 0.36 | 0.00 | 6.47 | 7.82 | 0.69 | 10.62 | 42.47 | 0.15 |
| Northbound_CD_5 | 0.14 | 29600 | 4038 | 45 | 24667 | 3365 | 0.00033 | 0.00014 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.00027 | 0.0018 | 0.00006 | 2.5 | 4933</ | | | | | | | | | | | | | | | | | | | |

| Design - 2050 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | Inputs Peak | | | | | | | Rates Peak | | | | | | | Totals | | | | | | | | |
|---------------------|--------|-----------------------|-------------|------------------|----------------|----------------|---------------|---------|------|---------|---------|---------|---------|-------------|----------|---------------|-------------|-------------|---------|---------|------------|---------|---------|----------|---------|--------|----------|--------|-------|------|-------|-------|-------|-------|--------|------|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM |
| Northbound FRNTG 44 | 0.11 | 26400 | 3033 | 40 | 22000 | 2527 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 3 | 4400 | 505 | 0.00259 | 0.00008 | 0.00 | 0.00108 | 0.00109 | 0.00009 | 0.0030 | 0.0035 | 0.000033 | 2.34 | 0.08 | 0.00 | 0.96 | 0.89 | 0.08 | 2.27 | 3.68 | 0.03 |
| Northbound FRNTG 45 | 0.06 | 8700 | 508 | 40 | 7250 | 423 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 17 | 1450 | 85 | 0.00074 | 0.00003 | 0.00 | 0.00031 | 0.00027 | 0.00025 | 0.00006 | 0.0014 | 0.000011 | 0.24 | 0.01 | 0.00 | 0.10 | 0.08 | 0.01 | 0.18 | 0.04 | 0.00 |
| Northbound FRNTG 46 | 0.77 | 35100 | 26974 | 40 | 29250 | 22478 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 17 | 5850 | 4496 | 0.00074 | 0.00003 | 0.00 | 0.00031 | 0.00027 | 0.00025 | 0.00006 | 0.0014 | 0.000011 | 12.49 | 0.46 | 0.00 | 5.06 | 4.24 | 0.40 | 9.61 | 23.40 | 0.20 |
| Northbound FRNTG 47 | 0.19 | 48500 | 9151 | 40 | 40417 | 7626 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 17 | 8083 | 1525 | 0.00074 | 0.00003 | 0.00 | 0.00031 | 0.00027 | 0.00025 | 0.00006 | 0.0014 | 0.000011 | 4.24 | 0.16 | 0.00 | 1.72 | 1.44 | 0.13 | 2.66 | 7.94 | 0.07 |
| Northbound FRNTG 48 | 0.10 | 60500 | 5793 | 40 | 50417 | 4827 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 14 | 10083 | 965 | 0.00084 | 0.00003 | 0.00 | 0.00035 | 0.00033 | 0.00029 | 0.00007 | 0.0015 | 0.000012 | 3.77 | 0.10 | 0.00 | 1.12 | 0.95 | 0.09 | 1.17 | 5.14 | 0.04 |
| Northbound FRNTG 49 | 0.24 | 60500 | 14595 | 40 | 50417 | 12163 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.000007 | 14 | 10083 | 2432 | 0.00084 | 0.00003 | 0.00 | 0.00035 | 0.00033 | 0.00029 | 0.00007 | 0.0015 | 0.000012 | 6.98 | 0.26 | 0.00 | 2.83 | 2.40 | 0.22 | 4.77 | 12.95 | 0.11 |
| Northbound ML 1 | 1.86 | 20850 | 38697 | 60 | 17375 | 32248 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 4 | 3475 | 6450 | 0.00180 | 0.00007 | 0.00 | 0.00132 | 0.00165 | 0.00146 | 0.0023 | 0.0073 | 0.000027 | 20.62 | 0.82 | 0.00 | 13.58 | 15.81 | 1.41 | 21.74 | 87.17 | 0.34 |
| Northbound ML 2 | 0.21 | 20850 | 4388 | 60 | 17375 | 3657 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 4 | 3475 | 731 | 0.00180 | 0.00007 | 0.00 | 0.00132 | 0.00165 | 0.00146 | 0.0023 | 0.0073 | 0.000027 | 2.34 | 0.09 | 0.00 | 1.54 | 1.79 | 0.16 | 2.47 | 9.88 | 0.04 |
| Northbound ML 3 | 0.48 | 15550 | 7422 | 60 | 12958 | 6185 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 12 | 2952 | 1237 | 0.00080 | 0.00003 | 0.00 | 0.00055 | 0.00065 | 0.00058 | 0.0009 | 0.0040 | 0.000013 | 2.72 | 0.11 | 0.00 | 1.65 | 1.79 | 0.16 | 2.38 | 12.53 | 0.05 |
| Northbound ML 4 | 2.60 | 21750 | 56599 | 60 | 18125 | 47166 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 3625 | 9433 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 38.41 | 1.49 | 0.00 | 26.27 | 31.50 | 2.80 | 44.01 | 159.04 | 0.61 |
| Northbound ML 5 | 0.94 | 29250 | 27445 | 60 | 24375 | 22871 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 52 | 4875 | 4574 | 0.00030 | 0.00001 | 0.00 | 0.00018 | 0.00019 | 0.00017 | 0.0002 | 0.0015 | 0.000005 | 7.77 | 0.32 | 0.00 | 4.41 | 4.53 | 0.41 | 5.99 | 35.02 | 0.14 |
| Northbound ML 6 | 0.87 | 32000 | 27733 | 60 | 26667 | 23111 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 55 | 5333 | 4622 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.00016 | 0.0002 | 0.0013 | 0.000005 | 7.81 | 0.32 | 0.00 | 4.40 | 4.51 | 0.41 | 6.00 | 34.69 | 0.14 |
| Northbound ML 7 | 1.91 | 11250 | 21438 | 60 | 9375 | 17865 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 21 | 1875 | 3573 | 0.00053 | 0.00002 | 0.00 | 0.00035 | 0.00040 | 0.00036 | 0.0005 | 0.0032 | 0.000009 | 6.91 | 0.28 | 0.00 | 4.06 | 4.30 | 0.39 | 5.67 | 33.47 | 0.12 |
| Northbound GP 1 | 0.27 | 55900 | 15006 | 60 | 46583 | 12505 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 16 | 9317 | 2501 | 0.00066 | 0.00003 | 0.00 | 0.00045 | 0.00052 | 0.00046 | 0.0007 | 0.0036 | 0.000010 | 5.15 | 0.21 | 0.00 | 3.08 | 3.30 | 0.30 | 4.34 | 24.51 | 0.09 |
| Northbound GP 2 | 0.65 | 69550 | 45220 | 60 | 57958 | 37683 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 4 | 11927 | 7507 | 0.00180 | 0.00007 | 0.00 | 0.00132 | 0.00165 | 0.00146 | 0.0023 | 0.0073 | 0.000027 | 24.09 | 0.95 | 0.00 | 15.87 | 18.48 | 1.65 | 25.41 | 101.86 | 0.39 |
| Northbound GP 3 | 0.27 | 100200 | 26937 | 60 | 83500 | 22447 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 16700 | 4489 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 18.28 | 0.71 | 0.00 | 12.50 | 14.99 | 1.33 | 20.94 | 75.69 | 0.29 |
| Northbound GP 4 | 0.35 | 70500 | 24872 | 60 | 58750 | 20727 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 4 | 11750 | 4145 | 0.00180 | 0.00007 | 0.00 | 0.00132 | 0.00165 | 0.00146 | 0.0023 | 0.0073 | 0.000027 | 13.25 | 0.52 | 0.00 | 8.73 | 10.16 | 0.91 | 13.97 | 56.03 | 0.22 |
| Northbound GP 5 | 0.28 | 88250 | 24463 | 60 | 73542 | 20386 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 14708 | 4077 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 16.60 | 0.64 | 0.00 | 11.35 | 13.62 | 1.21 | 19.02 | 68.74 | 0.26 |
| Northbound GP 6 | 0.67 | 77300 | 51886 | 60 | 64417 | 43238 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 5 | 12883 | 8647 | 0.00151 | 0.00006 | 0.00 | 0.00109 | 0.00135 | 0.00120 | 0.0019 | 0.0062 | 0.000023 | 25.12 | 1.00 | 0.00 | 16.25 | 18.64 | 1.66 | 25.42 | 107.23 | 0.42 |
| Northbound GP 7 | 0.05 | 71100 | 3251 | 60 | 59250 | 2709 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 11850 | 542 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 2.21 | 0.09 | 0.00 | 1.51 | 1.81 | 0.16 | 2.53 | 9.13 | 0.03 |
| Northbound GP 8 | 0.70 | 48950 | 34445 | 60 | 40792 | 28704 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 7 | 8158 | 5741 | 0.00117 | 0.00005 | 0.00 | 0.00083 | 0.00101 | 0.00089 | 0.0014 | 0.0051 | 0.000018 | 14.72 | 0.59 | 0.00 | 9.25 | 10.37 | 0.93 | 14.01 | 64.43 | 0.25 |
| Northbound GP 9 | 0.86 | 80850 | 69761 | 60 | 67375 | 58134 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 56 | 13475 | 11627 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.00015 | 0.0002 | 0.0013 | 0.000005 | 19.63 | 0.81 | 0.00 | 11.05 | 11.31 | 1.02 | 15.05 | 87.02 | 0.36 |
| Northbound GP 10 | 0.33 | 51250 | 17152 | 60 | 42708 | 14293 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 3 | 8542 | 2859 | 0.00228 | 0.00009 | 0.00 | 0.00170 | 0.00214 | 0.000189 | 0.0030 | 0.0092 | 0.000034 | 10.53 | 0.41 | 0.00 | 7.10 | 8.42 | 0.75 | 11.69 | 43.05 | 0.17 |
| Northbound GP 11 | 0.33 | 100050 | 33667 | 60 | 83375 | 27806 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 32 | 16675 | 5561 | 0.00041 | 0.00002 | 0.00 | 0.00026 | 0.00030 | 0.00027 | 0.0004 | 0.0025 | 0.000007 | 10.04 | 0.42 | 0.00 | 5.84 | 6.11 | 0.55 | 7.97 | 48.50 | 0.18 |
| Northbound GP 12 | 0.51 | 92550 | 46806 | 60 | 77125 | 39005 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 15425 | 7801 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 31.76 | 1.23 | 0.00 | 21.72 | 26.05 | 2.31 | 36.39 | 131.52 | 0.50 |
| Northbound GP 13 | 0.84 | 127350 | 107379 | 60 | 106125 | 89483 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 2.5 | 21225 | 17897 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00224 | 0.0036 | 0.0107 | 0.000039 | 72.87 | 2.83 | 0.00 | 49.84 | 59.77 | 5.31 | 83.49 | 301.74 | 1.16 |
| Northbound GP 14 | 1.51 | 96900 | 146767 | 60 | 80750 | 122305 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 56 | 16150 | 24461 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.00017 | 0.00015 | 0.0002 | 0.0013 | 0.000005 | 41.29 | 1.71 | 0.00 | 23.25 | 23.79 | 2.15 | 31.66 | 183.07 | 0.75 |
| Northbound GP 15 | 0.26 | 143850 | 37796 | 60 | 119875 | 31080 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 54 | 23975 | 6216 | 0.00032 | 0.00001 | 0.00 | 0.00017 | 0.00018 | 0.00016 | 0.0002 | 0.0014 | 0.000005 | 10.53 | 0.44 | 0.00 | 5.94 | 6.09 | 0.55 | 8.09 | 46.95 | 0.19 |
| Northbound GP 16 | 0.46 | 126950 | 57788 | 60 | 105792 | 48157 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 46 | 21158 | 9631 | 0.00032 | 0.00001 | 0.00 | 0.00020 | 0.00022 | 0.00020 | 0.0003 | 0.0018 | 0.000006 | 16.57 | 0.69 | 0.00 | 9.50 | 9.82 | 0.89 | 12.88 | 75.59 | 0.30 |
| Northbound GP 17 | 0.43 | 114950 | 49606 | 60 | 95792 | 41338 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 19 | 19158 | 8268 | 0.00058 | 0.00002 | 0.00 | 0.00038 | 0.00044 | 0.00039 | 0.0006 | 0.0033 | 0.000009 | 16.32 | 0.67 | 0.00 | 9.64 | 10.25 | 0.92 | 13.52 | 78.58 | 0.29 |
| Northbound GP 18 | 0.08 | 114950 | 8623 | 60 | 95792 | 7186 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.00021 | 0.0012 | 0.000005 | 54 | 19158 | 1437 | 0.00029 | 0.00001 | 0.00 | 0.00017 | 0.000 | | | | | | | | | | | | | |

| Design - 2050 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | Totals | | | | | | | | | | | |
|---------------------|--------|--------------------|----------------|---------------|------------|---------------|---------|---------|------|---------|---------|---------|---------|-------------|---------|------------|------------|----------|---------|---------|------|---------|---------|---------|--------|--------|---------|-------|-------|------|-------|-------|-------|-------|--------|------|
| Link Name | Length | 24HR ADT 2050 BASE | VMT Base | Speed NonPeak | ADT NoPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM |
| Southbound_FRNTG_30 | 0.18 | 6050 | 1095 | 35 | 5042 | 913 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 3 | 1008 | 182 | 0.00259 | 0.00008 | 0.00 | 0.00108 | 0.00109 | 0.00009 | 0.0030 | 0.0035 | 0.00033 | 0.89 | 0.03 | 0.00 | 0.36 | 0.34 | 0.03 | 0.86 | 1.39 | 0.01 |
| Southbound_FRNTG_31 | 0.15 | 21200 | 3093 | 35 | 17667 | 2578 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 2 | 3533 | 515 | 0.00303 | 0.00009 | 0.00 | 0.00126 | 0.00129 | 0.00017 | 0.0036 | 0.0040 | 0.00038 | 2.73 | 0.09 | 0.00 | 1.12 | 1.05 | 0.10 | 2.71 | 4.21 | 0.04 |
| Southbound_FRNTG_32 | 0.11 | 5200 | 587 | 35 | 4333 | 490 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 2 | 867 | 98 | 0.00303 | 0.00009 | 0.00 | 0.00126 | 0.00129 | 0.00017 | 0.0036 | 0.0040 | 0.00038 | 0.52 | 0.02 | 0.00 | 0.21 | 0.20 | 0.02 | 0.52 | 0.80 | 0.01 |
| Southbound_FRNTG_33 | 0.08 | 77550 | 5841 | 35 | 64625 | 4867 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 45 | 12925 | 973 | 0.00303 | 0.00009 | 0.00 | 0.00015 | 0.00012 | 0.00011 | 0.0036 | 0.0007 | 0.00006 | 2.57 | 0.10 | 0.00 | 1.03 | 0.85 | 0.08 | 1.92 | 4.75 | 0.04 |
| Southbound_FRNTG_34 | 0.44 | 93550 | 41050 | 35 | 77958 | 34208 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 4 | 15592 | 6842 | 0.00204 | 0.00006 | 0.00 | 0.00085 | 0.00085 | 0.00007 | 0.0023 | 0.0028 | 0.00026 | 29.46 | 1.02 | 0.00 | 12.04 | 10.92 | 1.01 | 27.23 | 47.74 | 0.42 |
| Southbound_FRNTG_35 | 0.15 | 27450 | 4080 | 35 | 22875 | 3400 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 13 | 4575 | 680 | 0.00303 | 0.00009 | 0.00 | 0.00036 | 0.00033 | 0.00007 | 0.0028 | 0.0008 | 0.00015 | 2.14 | 0.08 | 0.00 | 0.87 | 0.74 | 0.07 | 1.69 | 3.88 | 0.03 |
| Southbound_FRNTG_36 | 0.13 | 22800 | 2873 | 35 | 19000 | 2394 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 2 | 3800 | 479 | 0.00303 | 0.00009 | 0.00 | 0.00126 | 0.00129 | 0.00017 | 0.0036 | 0.0040 | 0.00038 | 2.54 | 0.08 | 0.00 | 1.04 | 0.98 | 0.09 | 2.52 | 3.91 | 0.04 |
| Southbound_FRNTG_37 | 0.24 | 47250 | 11431 | 35 | 39375 | 9526 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 25 | 7875 | 1905 | 0.00303 | 0.00009 | 0.00 | 0.00024 | 0.00020 | 0.00019 | 0.0005 | 0.0012 | 0.00009 | 5.44 | 0.20 | 0.00 | 2.19 | 1.82 | 0.17 | 4.11 | 10.16 | 0.08 |
| Southbound_FRNTG_38 | 0.07 | 44700 | 3351 | 35 | 37250 | 2793 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 6 | 7450 | 559 | 0.00148 | 0.00002 | 0.00 | 0.00062 | 0.00060 | 0.00055 | 0.0016 | 0.0022 | 0.00020 | 2.09 | 0.07 | 0.00 | 0.85 | 0.75 | 0.07 | 1.82 | 3.54 | 0.03 |
| Southbound_FRNTG_39 | 0.12 | 48800 | 5792 | 35 | 40667 | 4826 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 22 | 8133 | 965 | 0.00064 | 0.00002 | 0.00 | 0.00026 | 0.00022 | 0.00021 | 0.0005 | 0.0012 | 0.00010 | 2.80 | 0.10 | 0.00 | 1.13 | 0.94 | 0.09 | 2.13 | 5.21 | 0.04 |
| Southbound_FRNTG_40 | 0.44 | 25200 | 11102 | 35 | 21000 | 9252 | 0.00045 | 0.00017 | 0.00 | 0.00018 | 0.00015 | 0.00014 | 0.00034 | 0.00008 | 0.00007 | 5 | 4200 | 1850 | 0.00170 | 0.00005 | 0.00 | 0.00071 | 0.00070 | 0.00064 | 0.0019 | 0.0024 | 0.00022 | 7.35 | 0.26 | 0.00 | 3.00 | 2.68 | 0.25 | 6.57 | 12.18 | 0.11 |
| Southbound_FRNTG_41 | 0.16 | 26750 | 4319 | 40 | 22292 | 3599 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 12 | 4458 | 720 | 0.00092 | 0.00003 | 0.00 | 0.00038 | 0.00035 | 0.00032 | 0.0008 | 0.0016 | 0.00013 | 2.12 | 0.08 | 0.00 | 0.86 | 0.74 | 0.07 | 1.69 | 3.88 | 0.03 |
| Southbound_FRNTG_42 | 0.23 | 9250 | 2100 | 40 | 7708 | 1750 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 43 | 1542 | 350 | 0.00039 | 0.00001 | 0.00 | 0.00015 | 0.00013 | 0.00012 | 0.0008 | 0.0007 | 0.00006 | 0.85 | 0.03 | 0.00 | 0.34 | 0.28 | 0.03 | 0.62 | 1.59 | 0.01 |
| Southbound_FRNTG_43 | 0.41 | 24800 | 10249 | 40 | 20667 | 8541 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 12 | 4133 | 1708 | 0.00092 | 0.00003 | 0.00 | 0.00038 | 0.00035 | 0.00032 | 0.0008 | 0.0016 | 0.00013 | 5.04 | 0.18 | 0.00 | 2.05 | 1.74 | 0.16 | 4.02 | 9.20 | 0.08 |
| Southbound_FRNTG_44 | 0.55 | 23850 | 13073 | 40 | 19875 | 10894 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 29 | 3975 | 2179 | 0.00053 | 0.00002 | 0.00 | 0.00022 | 0.00019 | 0.00017 | 0.0004 | 0.0011 | 0.00008 | 5.58 | 0.21 | 0.00 | 2.26 | 1.87 | 0.17 | 4.16 | 10.77 | 0.09 |
| Southbound_FRNTG_45 | 0.33 | 36100 | 11840 | 40 | 30083 | 9867 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 44 | 6017 | 1973 | 0.00038 | 0.00001 | 0.00 | 0.00015 | 0.00012 | 0.00012 | 0.0003 | 0.0007 | 0.00006 | 4.76 | 0.18 | 0.00 | 1.91 | 1.57 | 0.15 | 3.51 | 8.96 | 0.08 |
| Southbound_FRNTG_46 | 0.05 | 75100 | 3882 | 40 | 62583 | 3235 | 0.00041 | 0.00015 | 0.00 | 0.00016 | 0.00013 | 0.00013 | 0.00030 | 0.00008 | 0.00007 | 44 | 12517 | 647 | 0.00038 | 0.00001 | 0.00 | 0.00015 | 0.00012 | 0.00012 | 0.0003 | 0.0007 | 0.00006 | 1.56 | 0.06 | 0.00 | 0.63 | 0.51 | 0.05 | 1.15 | 2.94 | 0.03 |
| Southbound_GP_1 | 0.30 | 114200 | 33998 | 60 | 95167 | 28332 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 59 | 19033 | 5666 | 0.00028 | 0.00001 | 0.00 | 0.00016 | 0.00016 | 0.00015 | 0.0002 | 0.0013 | 0.00005 | 9.33 | 0.39 | 0.00 | 5.35 | 5.47 | 0.50 | 7.28 | 42.07 | 0.17 |
| Southbound_GP_2 | 0.22 | 126900 | 27513 | 60 | 105750 | 22928 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 5 | 21150 | 4586 | 0.00018 | 0.00006 | 0.00 | 0.00109 | 0.00135 | 0.00120 | 0.0019 | 0.0062 | 0.00023 | 13.32 | 0.53 | 0.00 | 8.61 | 9.89 | 0.88 | 13.48 | 56.86 | 0.22 |
| Southbound_GP_3 | 0.73 | 135100 | 98701 | 60 | 112583 | 82251 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 4 | 22517 | 16450 | 0.00180 | 0.00007 | 0.00 | 0.00132 | 0.00165 | 0.00146 | 0.0023 | 0.0073 | 0.00027 | 52.59 | 2.08 | 0.00 | 34.63 | 40.33 | 3.59 | 55.45 | 222.33 | 0.86 |
| Southbound_GP_4 | 0.70 | 80750 | 56419 | 60 | 67292 | 47016 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 47 | 13458 | 9403 | 0.00032 | 0.00001 | 0.00 | 0.00020 | 0.00021 | 0.00019 | 0.0023 | 0.0017 | 0.00006 | 16.14 | 0.67 | 0.00 | 9.24 | 9.54 | 0.86 | 12.53 | 74.31 | 0.29 |
| Southbound_GP_5 | 0.76 | 80750 | 61707 | 60 | 67292 | 51423 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 2 | 13458 | 10284 | 0.00267 | 0.00010 | 0.00 | 0.00200 | 0.00254 | 0.00024 | 0.0036 | 0.0107 | 0.00039 | 41.87 | 1.63 | 0.00 | 28.64 | 34.35 | 3.05 | 47.98 | 173.40 | 0.66 |
| Southbound_GP_6 | 0.83 | 109500 | 90202 | 60 | 90875 | 75168 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 16 | 18170 | 10534 | 0.00066 | 0.00003 | 0.00 | 0.00045 | 0.00052 | 0.00046 | 0.0037 | 0.0036 | 0.00010 | 30.96 | 1.27 | 0.00 | 18.50 | 19.83 | 1.78 | 26.07 | 147.34 | 0.54 |
| Southbound_GP_7 | 0.36 | 88300 | 31627 | 60 | 73583 | 26356 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 7 | 14717 | 5271 | 0.00117 | 0.00005 | 0.00 | 0.00083 | 0.00101 | 0.00089 | 0.0014 | 0.0051 | 0.00018 | 13.52 | 0.54 | 0.00 | 8.49 | 9.52 | 0.85 | 12.87 | 59.16 | 0.23 |
| Southbound_GP_8 | 0.57 | 65600 | 37447 | 60 | 54667 | 31206 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 21 | 10933 | 6241 | 0.00053 | 0.00002 | 0.00 | 0.00035 | 0.00040 | 0.00039 | 0.0005 | 0.0032 | 0.00009 | 12.06 | 0.50 | 0.00 | 7.10 | 7.51 | 0.68 | 9.90 | 58.46 | 0.21 |
| Southbound_GP_9 | 0.66 | 90500 | 59519 | 60 | 75417 | 49599 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 10 | 15083 | 9920 | 0.00091 | 0.00004 | 0.00 | 0.00063 | 0.00074 | 0.00066 | 0.0010 | 0.0042 | 0.00014 | 22.90 | 0.93 | 0.00 | 13.99 | 13.33 | 1.38 | 20.51 | 102.57 | 0.39 |
| Southbound_GP_10 | 1.07 | 49900 | 53410 | 60 | 41583 | 44508 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 7 | 8317 | 8902 | 0.00117 | 0.00004 | 0.00 | 0.00083 | 0.00101 | 0.00089 | 0.0010 | 0.0051 | 0.00018 | 22.83 | 0.92 | 0.00 | 14.34 | 16.09 | 1.44 | 21.73 | 99.91 | 0.39 |
| Southbound_GP_11 | 0.75 | 98550 | 74066 | 60 | 82125 | 61722 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 3 | 16425 | 12344 | 0.00228 | 0.00009 | 0.00 | 0.00170 | 0.00214 | 0.00189 | 0.0030 | 0.0092 | 0.00034 | 45.46 | 1.78 | 0.00 | 30.65 | 36.32 | 3.23 | 50.49 | 189.78 | 0.73 |
| Southbound_GP_12 | 0.35 | 121250 | 42371 | 60 | 101792 | 35309 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 56 | 20358 | 7062 | 0.00029 | 0.00009 | 0.00 | 0.00017 | 0.00017 | 0.00015 | 0.0002 | 0.0013 | 0.00005 | 11.92 | 0.49 | 0.00 | 6.71 | 6.87 | 0.62 | 9.14 | 52.88 | 0.22 |
| Southbound_GP_13 | 0.49 | 106600 | 52671 | 60 | 88833 | 43893 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 22 | 17767 | 8779 | 0.00052 | 0.00002 | 0.00 | 0.00034 | 0.00039 | 0.00035 | 0.0005 | 0.0031 | 0.00008 | 16.82 | 0.69 | 0.00 | 9.88 | 10.45 | 0.94 | 13.75 | 81.77 | 0.30 |
| Southbound_GP_14 | 0.17 | 124100 | 20694 | 60 | 103417 | 17245 | 0.00028 | 0.00012 | 0.00 | 0.00016 | 0.00015 | 0.00015 | 0.00021 | 0.00012 | 0.00005 | 20 | 20683 | 3449 | 0.00055 | 0.00002 | 0.00 | 0.00036 | | | | | | | | | | | | | | |

| BASE - 2023 | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | | | | | | | | Rates Peak | | | | | | | | | | Totals | | | | | |
|---------------|--------|----------------|----------------|---------------|-------------|---------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-------------|----------|----------|--------|---------|---------|---------|---------|---------|---------|------------|---------|---------|-------|------|------|------|-------|------|-------|--------|------|--|--|--|--|
| Link Name | Length | 24 Hr ADT 2023 | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETBY | DPM | POM | | | | | |
| I35 Rmp NB 2 | 0.49 | 13002 | 6382 | 50 | 10835 | 5318 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 8 | 2167 | 1064 | 0.0029 | 0.00033 | 0.00017 | 0.00034 | 0.00022 | 0.00027 | 0.00023 | 0.016 | 0.00013 | 7.53 | 0.82 | 0.45 | 8.21 | 5.31 | 0.64 | 5.28 | 47.92 | 0.35 | | | | | |
| I35 Rmp NB 3 | 0.14 | 22178 | 3071 | 50 | 18482 | 2559 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 45 | 3696 | 512 | 0.0009 | 0.00009 | 0.00005 | 0.00009 | 0.00006 | 0.00007 | 0.00007 | 0.00007 | 0.00007 | 0.00004 | 2.62 | 0.27 | 0.16 | 2.68 | 1.73 | 0.21 | 1.66 | 18.10 | 0.12 | | | | |
| I35 Rmp NB 4 | 0.22 | 8899 | 1959 | 50 | 7416 | 1633 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 37 | 1483 | 327 | 0.0010 | 0.00009 | 0.00006 | 0.00011 | 0.00007 | 0.00008 | 0.00007 | 0.00007 | 0.00007 | 0.00005 | 1.72 | 0.18 | 0.10 | 1.75 | 1.13 | 0.13 | 1.09 | 11.79 | 0.08 | | | | |
| I35 Rmp NB 5 | 0.17 | 16046 | 2669 | 50 | 13371 | 2224 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 11 | 2674 | 445 | 0.0024 | 0.00026 | 0.00014 | 0.00027 | 0.00017 | 0.00021 | 0.00018 | 0.014 | 0.00011 | 2.93 | 0.31 | 0.17 | 3.10 | 2.01 | 0.24 | 1.98 | 18.95 | 0.13 | | | | | |
| I35 Rmp NB 6 | 0.13 | 9959 | 1247 | 50 | 8299 | 1039 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 36 | 1660 | 208 | 0.0011 | 0.00026 | 0.00006 | 0.00011 | 0.00007 | 0.00008 | 0.00007 | 0.00007 | 0.00005 | 1.10 | 0.11 | 0.07 | 1.12 | 0.72 | 0.09 | 0.70 | 7.53 | 0.05 | | | | | |
| I35 Rmp NB 7 | 0.10 | 7746 | 751 | 50 | 6455 | 626 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 7 | 1291 | 125 | 0.0031 | 0.00037 | 0.00018 | 0.00038 | 0.00023 | 0.00030 | 0.00026 | 0.018 | 0.00015 | 0.92 | 0.10 | 0.05 | 1.01 | 0.66 | 0.08 | 0.65 | 5.82 | 0.04 | | | | | |
| I35 Rmp NB 8 | 0.12 | 19411 | 2272 | 50 | 16176 | 1893 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 5 | 3235 | 379 | 0.0039 | 0.00049 | 0.00023 | 0.00051 | 0.00033 | 0.00040 | 0.00024 | 0.018 | 0.00019 | 3.09 | 0.35 | 0.18 | 3.54 | 2.29 | 0.28 | 2.30 | 19.36 | 0.15 | | | | | |
| I35 Rmp NB 9 | 0.14 | 4749 | 656 | 50 | 3958 | 547 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 30 | 792 | 109 | 0.0012 | 0.00012 | 0.00007 | 0.00012 | 0.00008 | 0.00010 | 0.00008 | 0.010 | 0.00005 | 0.59 | 0.06 | 0.04 | 0.61 | 0.39 | 0.05 | 0.38 | 4.20 | 0.03 | | | | | |
| I35 Rmp NB 10 | 0.18 | 12265 | 2199 | 50 | 10221 | 1833 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 2.5 | 2044 | 366 | 0.0067 | 0.00087 | 0.00039 | 0.00091 | 0.00059 | 0.00074 | 0.00063 | 0.041 | 0.00035 | 4.00 | 0.48 | 0.24 | 4.90 | 3.19 | 0.39 | 3.29 | 25.57 | 0.20 | | | | | |
| I35 Rmp NB 11 | 0.11 | 7239 | 785 | 50 | 6032 | 654 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 16 | 1206 | 131 | 0.0019 | 0.00020 | 0.00011 | 0.00020 | 0.00013 | 0.00015 | 0.00013 | 0.012 | 0.00008 | 0.80 | 0.08 | 0.05 | 0.82 | 0.53 | 0.06 | 0.52 | 5.36 | 0.04 | | | | | |
| I35 Rmp NB 12 | 0.13 | 16968 | 2157 | 50 | 14140 | 1797 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 5 | 2828 | 359 | 0.0039 | 0.00049 | 0.00023 | 0.00051 | 0.00033 | 0.00040 | 0.00034 | 0.022 | 0.00019 | 2.93 | 0.33 | 0.17 | 3.36 | 2.18 | 0.26 | 2.18 | 18.38 | 0.14 | | | | | |
| I35 Rmp NB 13 | 0.17 | 12311 | 2116 | 50 | 10259 | 1763 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 26 | 2052 | 353 | 0.0013 | 0.00013 | 0.00008 | 0.00014 | 0.00009 | 0.00011 | 0.00009 | 0.010 | 0.00006 | 1.95 | 0.20 | 0.12 | 2.00 | 1.30 | 0.15 | 1.26 | 13.70 | 0.09 | | | | | |
| I35 Rmp NB 14 | 0.28 | 9683 | 2692 | 50 | 8069 | 2244 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 5 | 1614 | 449 | 0.0039 | 0.00049 | 0.00023 | 0.00051 | 0.00033 | 0.00040 | 0.00034 | 0.022 | 0.00019 | 3.66 | 0.41 | 0.22 | 4.20 | 2.72 | 0.33 | 2.72 | 22.94 | 0.17 | | | | | |
| I35 Rmp NB 15 | 0.43 | 7147 | 3070 | 50 | 5956 | 2558 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 3 | 1191 | 512 | 0.0058 | 0.00074 | 0.00034 | 0.00077 | 0.00050 | 0.00063 | 0.00053 | 0.035 | 0.00030 | 5.11 | 0.60 | 0.30 | 6.16 | 4.01 | 0.49 | 4.10 | 32.52 | 0.25 | | | | | |
| I35 Rmp NB 16 | 0.15 | 7193 | 1093 | 50 | 5994 | 911 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 2.5 | 1199 | 182 | 0.0067 | 0.00087 | 0.00039 | 0.00091 | 0.00059 | 0.00074 | 0.00063 | 0.041 | 0.00035 | 1.99 | 0.24 | 0.12 | 2.44 | 1.59 | 0.19 | 1.64 | 12.71 | 0.10 | | | | | |
| I35 Rmp NB 17 | 0.11 | 14340 | 1621 | 50 | 11950 | 1351 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 4 | 2390 | 270 | 0.0046 | 0.00058 | 0.00027 | 0.00061 | 0.00039 | 0.00049 | 0.00041 | 0.027 | 0.00023 | 2.39 | 0.27 | 0.14 | 2.80 | 1.82 | 0.22 | 1.84 | 15.07 | 0.11 | | | | | |
| I35 Rmp NB 18 | 0.07 | 2305 | 163 | 50 | 1921 | 136 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 43 | 384 | 27 | 0.0009 | 0.00010 | 0.00006 | 0.00010 | 0.00006 | 0.00007 | 0.00006 | 0.007 | 0.00004 | 0.14 | 0.01 | 0.01 | 0.14 | 0.09 | 0.01 | 0.09 | 0.97 | 0.01 | | | | | |
| I35 Rmp NB 19 | 0.06 | 6824 | 396 | 50 | 5687 | 330 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 42 | 1137 | 66 | 0.0009 | 0.00010 | 0.00006 | 0.00010 | 0.00006 | 0.00007 | 0.00006 | 0.007 | 0.00004 | 0.34 | 0.04 | 0.02 | 0.35 | 0.23 | 0.03 | 0.22 | 2.35 | 0.02 | | | | | |
| I35 Rmp NB 20 | 0.05 | 10144 | 518 | 50 | 8453 | 432 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 10 | 1691 | 86 | 0.0025 | 0.00028 | 0.00015 | 0.00029 | 0.00019 | 0.00022 | 0.00019 | 0.014 | 0.00011 | 0.58 | 0.06 | 0.03 | 0.62 | 0.40 | 0.05 | 0.40 | 3.72 | 0.03 | | | | | |
| I35 Rmp NB 21 | 0.08 | 3781 | 316 | 50 | 3151 | 263 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 34 | 630 | 53 | 0.0011 | 0.00011 | 0.00007 | 0.00011 | 0.00007 | 0.00009 | 0.00007 | 0.008 | 0.00005 | 0.28 | 0.03 | 0.02 | 0.29 | 0.18 | 0.02 | 0.18 | 1.93 | 0.01 | | | | | |
| I35 Rmp NB 22 | 0.15 | 7377 | 1121 | 50 | 6148 | 934 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 35 | 1230 | 187 | 0.0011 | 0.00011 | 0.00006 | 0.00011 | 0.00007 | 0.00008 | 0.00007 | 0.007 | 0.00005 | 0.99 | 0.10 | 0.06 | 1.01 | 0.65 | 0.08 | 0.63 | 6.99 | 0.04 | | | | | |
| I35 Rmp NB 23 | 0.10 | 6547 | 679 | 50 | 5456 | 566 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 23 | 1091 | 113 | 0.0014 | 0.00015 | 0.00008 | 0.00015 | 0.00010 | 0.00011 | 0.00010 | 0.010 | 0.00006 | 0.64 | 0.07 | 0.04 | 0.66 | 0.43 | 0.05 | 0.41 | 4.43 | 0.03 | | | | | |
| I35 Rmp NB 24 | 0.10 | 19688 | 1895 | 50 | 16407 | 1579 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 13 | 3281 | 316 | 0.0022 | 0.00023 | 0.00013 | 0.00023 | 0.00015 | 0.00018 | 0.00016 | 0.013 | 0.00009 | 2.01 | 0.21 | 0.12 | 2.10 | 1.36 | 0.16 | 1.34 | 13.23 | 0.09 | | | | | |
| I35 Rmp NB 25 | 0.14 | 8760 | 1219 | 50 | 7300 | 1016 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 43 | 1460 | 203 | 0.0009 | 0.00010 | 0.00006 | 0.00010 | 0.00006 | 0.00007 | 0.00006 | 0.007 | 0.00004 | 1.05 | 0.11 | 0.06 | 1.07 | 0.69 | 0.08 | 0.66 | 7.22 | 0.05 | | | | | |
| I35 Rmp NB 26 | 0.17 | 9037 | 1570 | 50 | 7531 | 1308 | 0.00084 | 0.00087 | 0.00050 | 0.00086 | 0.00056 | 0.00066 | 0.00053 | 0.00058 | 0.00038 | 49 | 1506 | 262 | 0.0009 | 0.00009 | 0.00005 | 0.00009 | 0.00006 | 0.00007 | 0.00005 | 0.006 | 0.00004 | 1.33 | 0.14 | 0.08 | 1.36 | 0.88 | 0.10 | 0.84 | 9.09 | 0.06 | | | | | |
| I35 CD NB 1 | 0.20 | 4472 | 896 | 55 | 3727 | 747 | 0.00080 | 0.00082 | 0.00047 | 0.00080 | 0.00051 | 0.00061 | 0.00049 | 0.00050 | 0.00036 | 8 | 745 | 149 | 0.0029 | 0.00033 | 0.00017 | 0.00034 | 0.00022 | 0.00027 | 0.00023 | 0.016 | 0.00013 | 1.02 | 0.11 | 0.06 | 1.11 | 0.71 | 0.09 | 0.71 | 6.13 | 0.05 | | | | | |
| I35 CD NB 2 | 0.21 | 15446 | 3312 | 55 | 12872 | 2760 | 0.00080 | 0.00082 | 0.00047 | 0.00080 | 0.00051 | 0.00061 | 0.00049 | 0.00050 | 0.00036 | 38 | 2574 | 552 | 0.0010 | 0.00010 | 0.00006 | 0.00010 | 0.00007 | 0.00008 | 0.00007 | 0.007 | 0.00005 | 2.76 | 0.28 | 0.16 | 2.79 | 1.78 | 0.21 | 1.73 | 17.64 | 0.12 | | | | | |
| I35 DC NB 1 | 0.25 | 30984 | 7884 | 55 | 25820 | 6570 | 0.00080 | 0.00082 | 0.00047 | 0.00080 | 0.00051 | 0.00061 | 0.00049 | 0.00050 | 0.00036 | 55 | 5164 | 1314 | 0.0008 | 0.00008 | 0.00005 | 0.00008 | 0.00005 | 0.00006 | 0.00005 | 0.005 | | | | | | | | | | | | | | | |

| BASE - 2023 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | | Inputs Peak | | | | Rates Peak | | | | | | Totals | | | | | | | | | |
|-----------------|--------|----------------|----------|----------------|-------------|-------------|---------------|---------|---------|---------|---------|----------|---------|--------|----------|------------|-------------|----------|--------|---------|------------|---------|---------|---------|---------|--------|---------|-------|-------|------|------|------|-------|------|-------|------|
| Link Name | Length | 24 Hr ADT 2023 | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETVB | DPM | POM |
| I35 Frmtg SB 15 | 0.18 | 16387 | 2928 | 40 | 13656 | 2440 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 33 | 2731 | 488 | 0.0013 | 0.00010 | 0.00007 | 0.00009 | 0.00005 | 0.00006 | 0.00008 | 0.003 | 0.00004 | 3.34 | 0.25 | 0.18 | 2.21 | 1.33 | 0.15 | 2.00 | 8.83 | 0.10 |
| I35 Frmtg SB 16 | 0.27 | 21142 | 5639 | 40 | 17618 | 4699 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 15 | 3524 | 940 | 0.0022 | 0.00016 | 0.00011 | 0.00015 | 0.00009 | 0.00010 | 0.00015 | 0.006 | 0.00007 | 7.23 | 0.54 | 0.39 | 4.84 | 2.92 | 0.34 | 4.47 | 18.95 | 0.22 |
| I35 Frmtg SB 17 | 0.08 | 19803 | 1555 | 40 | 16503 | 1296 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 31 | 3301 | 259 | 0.0014 | 0.00016 | 0.00008 | 0.00009 | 0.00006 | 0.00006 | 0.00008 | 0.0005 | 0.00004 | 1.80 | 0.13 | 0.10 | 1.19 | 0.71 | 0.08 | 1.08 | 4.77 | 0.06 |
| I35 Frmtg SB 18 | 0.25 | 11725 | 2912 | 40 | 9771 | 2427 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 35 | 1954 | 485 | 0.0013 | 0.00009 | 0.00007 | 0.00008 | 0.00005 | 0.00006 | 0.00008 | 0.003 | 0.00004 | 3.29 | 0.24 | 0.18 | 2.18 | 1.31 | 0.15 | 1.97 | 8.64 | 0.10 |
| I35 Frmtg SB 19 | 0.17 | 13987 | 2345 | 40 | 11656 | 1955 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 12 | 2331 | 391 | 0.0024 | 0.00019 | 0.00013 | 0.00017 | 0.00010 | 0.00012 | 0.00017 | 0.006 | 0.00008 | 3.11 | 0.23 | 0.17 | 2.10 | 1.27 | 0.15 | 1.96 | 8.09 | 0.10 |
| I35 Frmtg SB 20 | 0.14 | 10479 | 1452 | 40 | 8732 | 1210 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 34 | 1746 | 242 | 0.0013 | 0.00009 | 0.00007 | 0.00008 | 0.00005 | 0.00006 | 0.00008 | 0.003 | 0.00004 | 1.65 | 0.12 | 0.09 | 1.09 | 0.66 | 0.08 | 0.99 | 4.34 | 0.05 |
| I35 Frmtg SB 21 | 0.14 | 13571 | 1877 | 40 | 11309 | 1564 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 29 | 2262 | 313 | 0.0015 | 0.00009 | 0.00008 | 0.00009 | 0.00005 | 0.00007 | 0.00009 | 0.004 | 0.00004 | 2.19 | 0.16 | 0.12 | 1.45 | 0.87 | 0.10 | 1.31 | 5.83 | 0.07 |
| I35 Frmtg SB 22 | 0.09 | 18649 | 1603 | 40 | 15541 | 1336 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 3 | 3108 | 267 | 0.0062 | 0.00053 | 0.00030 | 0.00050 | 0.00030 | 0.00037 | 0.0054 | 0.017 | 0.00021 | 3.12 | 0.25 | 0.16 | 2.32 | 1.40 | 0.17 | 2.32 | 8.36 | 0.10 |
| I35 Frmtg SB 23 | 0.17 | 22157 | 3722 | 40 | 18464 | 3102 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 4 | 3693 | 620 | 0.0049 | 0.00042 | 0.00025 | 0.00039 | 0.00024 | 0.00029 | 0.0042 | 0.013 | 0.00017 | 6.48 | 0.51 | 0.34 | 4.72 | 2.84 | 0.34 | 4.63 | 17.10 | 0.21 |
| I35 Frmtg SB 24 | 0.10 | 28574 | 2947 | 40 | 23811 | 2456 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 4762 | 491 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 6.22 | 0.50 | 0.32 | 4.69 | 2.83 | 0.34 | 4.74 | 16.83 | 0.21 |
| I35 Frmtg SB 25 | 0.02 | 24419 | 605 | 40 | 20349 | 504 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 5 | 4070 | 101 | 0.0042 | 0.00035 | 0.00021 | 0.00033 | 0.00020 | 0.00024 | 0.0034 | 0.011 | 0.00014 | 0.98 | 0.08 | 0.05 | 0.70 | 0.42 | 0.05 | 0.68 | 2.55 | 0.03 |
| I35 Frmtg SB 26 | 0.15 | 10986 | 1613 | 40 | 9155 | 1344 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 11 | 1831 | 269 | 0.0025 | 0.00020 | 0.00013 | 0.00018 | 0.00011 | 0.00013 | 0.0018 | 0.006 | 0.00008 | 2.17 | 0.16 | 0.12 | 1.47 | 0.89 | 0.10 | 1.38 | 5.63 | 0.07 |
| I35 Frmtg SB 27 | 0.04 | 20819 | 861 | 40 | 17349 | 717 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 6 | 3470 | 143 | 0.0037 | 0.00030 | 0.00019 | 0.00028 | 0.00017 | 0.00021 | 0.0029 | 0.009 | 0.00012 | 1.32 | 0.10 | 0.07 | 0.93 | 0.56 | 0.07 | 0.89 | 3.44 | 0.04 |
| I35 Frmtg SB 28 | 0.09 | 24788 | 2264 | 40 | 20657 | 1887 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 7 | 4131 | 377 | 0.0033 | 0.00027 | 0.00017 | 0.00025 | 0.00015 | 0.00018 | 0.0026 | 0.008 | 0.00011 | 3.34 | 0.26 | 0.18 | 2.34 | 1.41 | 0.16 | 2.22 | 8.68 | 0.11 |
| I35 Frmtg SB 29 | 0.14 | 22019 | 3110 | 40 | 18349 | 2592 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 23 | 3670 | 518 | 0.0017 | 0.00012 | 0.00009 | 0.00011 | 0.00007 | 0.00008 | 0.0011 | 0.004 | 0.00005 | 3.76 | 0.28 | 0.20 | 2.48 | 1.49 | 0.17 | 2.27 | 9.88 | 0.12 |
| I35 Frmtg SB 30 | 0.06 | 32405 | 2056 | 40 | 27004 | 1713 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 3 | 5401 | 343 | 0.0062 | 0.00053 | 0.00030 | 0.00050 | 0.00030 | 0.00037 | 0.0054 | 0.017 | 0.00021 | 4.00 | 0.32 | 0.21 | 2.98 | 1.79 | 0.22 | 2.97 | 10.72 | 0.13 |
| I35 Frmtg SB 31 | 0.07 | 23404 | 1536 | 40 | 19503 | 1280 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 3901 | 256 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 3.24 | 0.26 | 0.17 | 2.45 | 1.47 | 0.18 | 2.47 | 8.78 | 0.11 |
| I35 Frmtg SB 32 | 0.08 | 26081 | 2016 | 40 | 21734 | 1680 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 4347 | 336 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 4.26 | 0.35 | 0.22 | 3.21 | 1.93 | 0.23 | 3.25 | 11.52 | 0.14 |
| I35 Frmtg SB 33 | 0.12 | 8817 | 1097 | 40 | 7347 | 914 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 1469 | 183 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 2.32 | 0.19 | 0.12 | 1.75 | 1.05 | 0.13 | 1.77 | 6.27 | 0.08 |
| I35 Frmtg SB 34 | 0.17 | 4801 | 823 | 40 | 4001 | 686 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 800 | 137 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 1.74 | 0.14 | 0.09 | 1.31 | 0.79 | 0.10 | 1.33 | 4.70 | 0.06 |
| I35 Frmtg SB 35 | 0.03 | 12417 | 399 | 40 | 10348 | 332 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 2.5 | 2070 | 67 | 0.0071 | 0.00062 | 0.00035 | 0.00059 | 0.00036 | 0.00044 | 0.0064 | 0.020 | 0.00025 | 0.84 | 0.07 | 0.04 | 0.64 | 0.38 | 0.05 | 0.64 | 2.28 | 0.03 |
| I35 Frmtg SB 36 | 0.10 | 19849 | 1989 | 40 | 16541 | 1657 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 11 | 3308 | 331 | 0.0025 | 0.00020 | 0.00013 | 0.00018 | 0.00011 | 0.00013 | 0.0018 | 0.006 | 0.00008 | 2.67 | 0.20 | 0.14 | 1.82 | 1.09 | 0.13 | 1.70 | 6.95 | 0.08 |
| I35 Frmtg SB 37 | 0.17 | 7340 | 1243 | 40 | 6116 | 1036 | 0.00111 | 0.00082 | 0.00060 | 0.00073 | 0.00044 | 0.000051 | 0.00066 | 0.0029 | 0.000034 | 11 | 1223 | 207 | 0.0025 | 0.00020 | 0.00013 | 0.00018 | 0.00011 | 0.00013 | 0.0018 | 0.006 | 0.00008 | 1.67 | 0.13 | 0.09 | 1.14 | 0.68 | 0.08 | 1.06 | 3.44 | 0.05 |
| I35 Frmtg SB 38 | 0.17 | 9232 | 1572 | 45 | 7694 | 1310 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 37 | 1539 | 262 | 0.0012 | 0.00009 | 0.00006 | 0.00008 | 0.00005 | 0.00005 | 0.00007 | 0.003 | 0.00004 | 1.62 | 0.12 | 0.09 | 1.08 | 0.65 | 0.07 | 0.96 | 4.39 | 0.05 |
| I35 Frmtg SB 39 | 0.49 | 24604 | 11988 | 45 | 20503 | 9990 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 20 | 4101 | 1998 | 0.0019 | 0.00014 | 0.00010 | 0.00012 | 0.00007 | 0.00008 | 0.0012 | 0.005 | 0.00006 | 13.71 | 0.72 | 0.74 | 9.16 | 5.50 | 0.63 | 8.30 | 36.87 | 0.43 |
| I35 Frmtg SB 40 | 0.21 | 17827 | 3738 | 45 | 14856 | 3115 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 10 | 2971 | 623 | 0.0014 | 0.00010 | 0.00008 | 0.00009 | 0.00006 | 0.00006 | 0.00009 | 0.004 | 0.00004 | 4.00 | 0.30 | 0.22 | 2.67 | 1.61 | 0.18 | 2.39 | 10.99 | 0.13 |
| I35 Frmtg SB 41 | 0.15 | 36941 | 5390 | 45 | 30784 | 4492 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 22 | 6177 | 898 | 0.0018 | 0.00013 | 0.00009 | 0.00011 | 0.00007 | 0.00008 | 0.0011 | 0.005 | 0.00005 | 6.07 | 0.45 | 0.33 | 4.05 | 2.43 | 0.28 | 3.66 | 16.37 | 0.19 |
| I35 Frmtg SB 42 | 0.16 | 21181 | 3364 | 45 | 17651 | 2804 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 11 | 3530 | 561 | 0.0025 | 0.00020 | 0.00013 | 0.00018 | 0.00011 | 0.00013 | 0.0018 | 0.006 | 0.00008 | 4.21 | 0.32 | 0.22 | 2.90 | 1.74 | 0.20 | 2.68 | 11.22 | 0.14 |
| I35 Frmtg SB 43 | 0.18 | 24765 | 4453 | 45 | 20638 | 3711 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 40 | 4128 | 742 | 0.0011 | 0.00008 | 0.00006 | 0.00007 | 0.00004 | 0.00005 | 0.00007 | 0.003 | 0.00003 | 4.52 | 0.34 | 0.24 | 3.04 | 1.82 | 0.21 | 2.69 | 12.33 | 0.13 |
| I35 Frmtg SB 44 | 0.38 | 17046 | 6452 | 45 | 14205 | 5377 | 0.00100 | 0.00075 | 0.00054 | 0.00067 | 0.00040 | 0.00046 | 0.00059 | 0.0027 | 0.000032 | 37 | 2841 | 1075 | 0.0012 | 0.00009 | 0.00006 | 0.00008 | 0.00005 | 0.00005 | 0.00007 | 0.003 | 0.00004 | 6.64 | 0.50 | 0.36 | 4.45 | 2.66 | 0.31 | 3.95 | 18.01 | 0.21 |
| I35 Frmtg SB 45 | 0.29 | 21503 | 6226 | 50 | 17919 | 5188 | 0.00092 | 0.00070 | 0.00049 | 0.00062 | 0.00037 | 0.00043 | 0.0005 | | | | | | | | | | | | | | | | | | | | | | | |

| BASE - 2023 | | | | Inputs NonPeak | | | Rates NonPeak | | | | | | | | | Inputs Peak | | | Rates Peak | | | | | | | | | Totals | | | | | | | | | |
|-------------|--------|----------------|----------|----------------|-------------|-------------|---------------|----------|----------|---------|---------|----------|---------|--------|----------|-------------|----------|----------|------------|---------|---------|--------|--------|---------|--------|---------|---------|---------|-------|-------|------|------|-------|-------|-------|-------|------|
| Link Name | Length | 24 Hr ADT 2023 | VMT Base | Speed NonPeak | ADT NonPeak | VMT NonPeak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | Speed Peak | ADT Peak | VMT Peak | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | BENZ | NAPTH | BUTA | FORM | ACTE | ACROL | ETYB | DPM | POM | |
| 135 DC EB 2 | 0.30 | 35872 | 10825 | 55 | 29893 | 9021 | 0.00080 | 0.000082 | 0.000047 | 0.00080 | 0.00051 | 0.000061 | 0.00049 | 0.0050 | 0.000036 | 55 | 5979 | 1804 | 0.0008 | 0.00008 | 0.00005 | 0.0008 | 0.0005 | 0.00006 | 0.0005 | 0.00004 | 0.0005 | 0.00004 | 8.63 | 0.89 | 0.51 | 8.70 | 5.53 | 0.66 | 5.34 | 53.73 | 0.39 |
| 135 DC EB 3 | 0.34 | 20011 | 6821 | 55 | 16676 | 5685 | 0.00080 | 0.000082 | 0.000047 | 0.00080 | 0.00051 | 0.000061 | 0.00049 | 0.0050 | 0.000036 | 46 | 3335 | 1137 | 0.0009 | 0.00009 | 0.00005 | 0.0009 | 0.0006 | 0.00007 | 0.0006 | 0.0006 | 0.00004 | 5.54 | 0.57 | 0.33 | 5.61 | 3.58 | 0.43 | 3.45 | 35.43 | 0.25 | |
| 135 DC WB 1 | 0.19 | 17982 | 3439 | 55 | 14985 | 2866 | 0.00080 | 0.000082 | 0.000047 | 0.00080 | 0.00051 | 0.000061 | 0.00049 | 0.0050 | 0.000036 | 55 | 2997 | 573 | 0.0008 | 0.00008 | 0.00005 | 0.0008 | 0.0005 | 0.00006 | 0.0005 | 0.00004 | 2.74 | 0.28 | 0.16 | 2.76 | 1.76 | 0.21 | 1.70 | 17.07 | 0.12 | | |
| 135 DC WB 2 | 0.32 | 41082 | 13273 | 55 | 34235 | 11060 | 0.00080 | 0.000082 | 0.000047 | 0.00080 | 0.00051 | 0.000061 | 0.00049 | 0.0050 | 0.000036 | 55 | 6847 | 2212 | 0.0008 | 0.00008 | 0.00005 | 0.0008 | 0.0005 | 0.00006 | 0.0005 | 0.00004 | 10.58 | 1.09 | 0.63 | 10.67 | 6.78 | 0.81 | 6.55 | 65.87 | 0.47 | | |

**Carbon Monoxide Traffic Air Quality Analysis – as Published in the DEIS,
January 5, 2023**



Carbon Monoxide Traffic Air Quality Analysis

I-35 Capital Express Central Project

Travis County, Texas
Austin District
CSJ: 0015-13-388

August 2022

The environmental review, consultation, and other actions required by applicable Federal environmental laws for this project are being, or have been, carried out by TxDOT pursuant to 23 U.S.C. 327 and a Memorandum of Understanding dated December 9, 2019, and executed by FHWA and TxDOT.

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Appendices

- Appendix A: Project Location Map
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- Appendix C: CO Receptor Locations

1.0 Introduction

The Texas Department of Transportation (TxDOT) Austin District is proposing improvements to Interstate Highway 35 (I-35) from US Highway 290 East (US 290E) to State Highway 71 (SH 71)/Ben White Boulevard (CSJ: 0015-13-388). See **Appendix A** for a Project Location Map.

Modeled Scenarios

The project is evaluating improvements between two potential build alternatives, referred to as Build Alternative 2 (Alt 2) and Modified Build Alternative 3 (Alt 3 Mod). Alt 2, Alt 3 Mod, and the No Build Alternative were modeled for this carbon monoxide (CO) analysis for the estimated time of completion (ETC) year (2030) and design year (2050), in accordance with TxDOT's *Environmental Guide: Volume 2 Activity Instructions* (September 2021).

2.0 Background Information

CO is a primary pollutant from motor vehicles that is largely emitted from a vehicle's exhaust system; thus, there is a federal requirement to model localized CO concentrations for proposed highway projects. Projects that are adding capacity may result in an increase of CO emissions; therefore, TxDOT requires the completion of a project-level CO analysis for added capacity projects that exceed an annual average daily traffic (AADT) volume of 140,000 vehicles per day (vpd).

Since the project would add capacity and the design year traffic volume is above 140,000 vpd (see **Table 1** below), a CO traffic air quality analysis (TAQA) is required to assess whether the project would adversely affect local air quality by contributing to CO levels that exceed the 1-hour or 8-hour CO National Ambient Air Quality Standard (NAAQS).

3.0 Analysis Methodology

CO concentrations for the No Build Alternative, Alt 2, and Alt 3 Mod were modeled for the ETC and design years using the CAL3QHC dispersion model. The supplied traffic data includes 24-hour average annual volumes for the years of 2030 and 2050. Traffic for the ETC and design year is shown by section in **Table 1**. See **Appendix B** for the complete traffic data provided by TxDOT Austin District.

Table 1: Projected AADT and DHV

| I-35 Sections: Mainlanes | AADT | | DHV | |
|--|------------|---------------|------------|---------------|
| | 2030 (ETC) | 2050 (Design) | 2030 (ETC) | 2050 (Design) |
| Section 1: S of William Cannon Dr Ramp to N of 32 nd St Ramps | 181,550 | 238,300 | 12,708 | 16,681 |
| Section 2: N of 32 nd St Ramps to N end of project | 245,200 | 305,900 | 14,466 | 18,048 |
| I-35 Sections: Frontage Roads | AADT | | DHV | |
| | 2030 (ETC) | 2050 (Design) | 2030 (ETC) | 2050 (Design) |
| Section 3: S of William Cannon Drive Ramp to N of Lady Bird Lake (S of Holly St Off Ramp) | 78,900 | 103,550 | 5,523 | 7,248 |
| Section 4: N of Lady Bird Lake (S of Holly St Off Ramp) to S of 32 nd St Off Ramp | 71,050 | 89,450 | 4,973 | 6,261 |
| Section 5: S of 32 nd Street Off Ramp to N of Airport Blvd Ramps | 48,400 | 60,200 | 2,855 | 3,551 |
| Section 6: N of Airport Blvd Ramps to S of US 290 INTX Ramps | 84,400 | 104,500 | 4,979 | 6,165 |

DHV – Design Hourly Volume

The CO analysis includes modeled free-flow areas, as well as select intersections. The free-flow segments (segments 1 through 4) modeled in the CO analysis were chosen based on the areas of the project with the highest AADT and a narrow ROW. Each of the segments were modeled for both alternatives in both the ETC and design year. The modeled segment limits and their respective traffic sections are as follows:

- Segment 1: South of 51st St to N of Airport Blvd (within Traffic Section 2 (Mainlanes) and Section 6 (Frontage Roads))
- Segment 2: North of Dean Keeton to Manor Rd (within Traffic Section 1 (Mainlanes) and Section 4 (Frontage Roads))
- Segment 3: Holly St to north of Lake Austin Dr (within Traffic Section 1 (Mainlanes) and Section 4 (Frontage Roads))
- Segment 4: Woodward St to south of Oltorf St (within Traffic Section 1 (Mainlanes) and Section 3 (Frontage Roads))

Intersection segments (segments 5 through 6) were modeled and chosen based on their Level of Service (LOS) rating (either D, E, or F, with F being the worst LOS). LOS for all the intersections within the Alt 2 and Alt 3 Mod study area were identified for the ETC and design year, as well as AM and PM peak periods. From this,

the two intersections with the most prevalent “F” rated LOS across the peak periods and analyzed years were chosen as the segments for this CO analysis.

- Segment 5: 7th St Intersection (within Traffic Section 1 (Mainlanes) and Section 4 (Frontage Roads)).
- Segment 6: Riverside Dr Intersection (within Traffic Section 1 (Mainlanes) and Section 4 (Frontage Roads))

Background CO concentrations of 1.6 parts per million (ppm) (1-hour) and 1.3 ppm (8-hour) were used for the model in accordance with Appendix B of TxDOT’s *Environmental Guide: Volume 2 Activity Instructions (September 2021)*.

Variable emission rates were used in the analysis based on worst-case peak speeds. Worst-case peak traffic speeds range from 3 to 67 mph for both free-flow and intersection scenarios. The rates were derived from the MOVES2014 model, gathered from the TxDOT Running and Idling Emission Rates Lookup Tables (ERLT) for TAQA (*TxDOT Air Quality Toolkit, May 2021*). Running emissions were used for free-flow road links and idling emissions were used for the intersection idling road links.

The following adverse meteorological conditions are the worst-case assumptions and input parameters used in the analysis, in accordance with Appendix D of TxDOT’s *Environmental Guide: Volume 2 Activity Instructions (July 2021)*:

- Averaging time of 60 minutes
- Atmospheric Stability Class of 4 (stable)
- Mixing height of 1,000 meters
- Wind speed of 1 meter per second
- Winds blowing parallel to the roadway

The following input parameters were used in the intersection analysis, in accordance with *User’s Guide to CAL3QHC Version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations Near Roadway Intersections (Revised)*:

- Average total signal cycle length
- Average red total signal cycle length
- Clearance lost time
- Approach volume on queue link
- Idle emission factor

- Saturation flow rate
- Signal type
- Arrival rate

4.0 Receptor Locations

Free-flow receptors were modeled on the ROW line for each modeled segment. Intersection receptors were modeled at least 10 feet away from the nearest travel lane and on public use features, such as a sidewalk, and placed at each quadrant of the intersection. A standard height of 5.9 feet was given to the receptors for all models to simulate the average height of a person. **Table 2** and **Table 3** depict the associated ROW, LOS, and traffic at each of the modeled receptors. Aerial maps depicting the receptor locations along the project ROW are found in **Appendix C**.

Table 2: Free-flow Receptor Descriptions

| Name | Segment | Distance from Roadway | | ROW Width | | 2030 Total DHV | 2050 Total DHV | 2030 Total AADT | 2050 Total AADT | Traffic Speeds |
|-----------------|-----------|-----------------------|-----------|-----------|-----------|----------------|----------------|-----------------|-----------------|----------------|
| | | Alt 2 | Alt 3 Mod | Alt 2 | Alt 3 Mod | | | | | |
| Receptor 1 (R1) | Segment 1 | 58 ft | 34 ft | 422 ft | 422 ft | 19,445 | 24,213 | 329,600 | 410,400 | 4-58 mph |
| Receptor 2 (R2) | Segment 1 | 88 ft | 79 ft | 422 ft | 422 ft | 19,445 | 24,213 | 329,600 | 410,400 | 4-58 mph |
| Receptor 3 (R3) | Segment 2 | 7 ft | 7 ft | 216 ft | 216 ft | 17,681 | 22,942 | 252,600 | 327,750 | 3-55 mph |
| Receptor 4 (R4) | Segment 2 | 9 ft | 9 ft | 216 ft | 216 ft | 17,681 | 22,942 | 252,600 | 327,750 | 3-55 mph |
| Receptor 5 (R5) | Segment 3 | 32 ft | 30 ft | 345 ft | 336 ft | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| Receptor 6 (R6) | Segment 3 | 33 ft | 26 ft | 345 ft | 336 ft | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| Receptor 7 (R7) | Segment 4 | 34 ft | 24 ft | 350 ft | 350 ft | 18,231 | 23,929 | 260,450 | 341,850 | 3-66 mph |
| Receptor 8 (R8) | Segment 4 | 23 ft | 23 ft | 350 ft | 350 ft | 18,231 | 23,929 | 260,450 | 341,850 | 3-66 mph |

Table 3: Intersection Receptor Descriptions

| Name | Segment | Distance from Roadway | LOS | 2030 Total DHV | 2050 Total DHV | 2030 Total AADT | 2050 Total AADT | Traffic Speeds |
|-----------------------------|-----------|-----------------------|-----|----------------|----------------|-----------------|-----------------|----------------|
| 7 th St (7th SE) | Segment 5 | 11 ft | F | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| 7 th St (7th NE) | Segment 5 | 11 ft | F | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| 7 th St (7th NW) | Segment 5 | 10 ft | F | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| 7 th St (7th SW) | Segment 5 | 21 ft | F | 17,681 | 22,942 | 252,600 | 327,750 | 3-67 mph |
| Riverside Dr (RS SE) | Segment 6 | 25 ft | F | 18,231 | 23,929 | 260,450 | 341,850 | 3-67 mph |
| Riverside Dr (RS NE) | Segment 6 | 27 ft | F | 18,231 | 23,929 | 260,450 | 341,850 | 3-67 mph |
| Riverside Dr (RS SW) | Segment 6 | 12 ft | F | 18,231 | 23,929 | 260,450 | 341,850 | 3-67 mph |
| Riverside Dr (RS NW) | Segment 6 | 21 ft | F | 18,231 | 23,929 | 260,450 | 341,850 | 3-67 mph |

5.0 Analysis Results

The 1-hour CO NAAQS is 35 ppm, while the 8-hour NAAQS is 9 ppm, which are not to be exceeded more than once in a year. Modeling results indicate that local concentrations of CO are not expected to exceed national standards at any time along any segment of the project. While emission rates are expected to decrease over time, some model results show a slight increase in CO concentrations from 2030 to 2050. These increases can be explained with the worsening traffic speeds predicted for 2050.

The highest CO concentration result and percent of the 1-hour and 8-hour NAAQS along the I-35 project for all scenarios and intersections are recorded in **Tables 4 through 7**. The highest modeled CO concentrations consistently occur in Segment 2, from north of Dean Keaton to Manor Road, and represents the worst-case results for the project. Though the AADT for Segment 2 is the lowest, it has the slowest speeds and narrowest ROW by 120 feet. In contrast, the lowest modeled CO concentrations occur in Segments 1 and 4, which have the widest ROW.

The projected CO concentrations are relatively consistent between the 7th St and Riverside intersections, with the highest CO concentration result occurring at 7th Street in the Alt 3 Mod 2050 scenario. Results showed that neither 2030 nor 2050 CO concentrations at the worst ranking LOS intersections for the project (peaking

at 2.0 ppm) do not surpass the free-flow segment CO concentrations for any of the build alternatives (peaking at 2.3 ppm).

Among all modeled segments, receptor proximity to roadway section tends to be a standout determining factor for CO concentrations. Peak speed limit is the obvious contributing factor for any variance in expected CO concentrations between ETC and Design scenarios since they vary with year while AADT between the scenarios grow in tandem.

The associated input and output CAL3QHC files have been submitted with this technical report for inclusion in the project files.

Table 4: Free-flow No Build, Alt 2, and Alt 3 Mod 1-Hour and 8-Hour CO Concentrations (ETC Year)

| ETC Year: 2030 | | | | | | | |
|-----------------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| No Build | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 2 (NB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 3 (SB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 4 (NB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 5 (SB) | Segment 3 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 6 (NB) | Segment 3 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 7 (SB) | Segment 4 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 8 (NB) | Segment 4 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Alt 2 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 2 (NB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 3 (SB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 4 (NB) | Segment 2 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 5 (SB) | Segment 3 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 6 (NB) | Segment 3 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |

| Alt 3 Mod | | | | | | | |
|--|------------------------|---|--|--|---|-----------------------|-----------------------|
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| Receptor 2 (NB) | Segment 1 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| Receptor 3 (SB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 4 (NB) | Segment 2 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 5 (SB) | Segment 3 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 6 (NB) | Segment 3 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| Note: 8-Hour CO Concentrations have been rounded to the nearest tenth decimal. | | | | | | | |

Table 5: Free-flow No Build, Alt 2, and Alt 3 Mod 1-Hour and 8-Hour CO Concentrations (Design Year)

| Design Year: 2050 | | | | | | | |
|-------------------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| No Build | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 2 (NB) | Segment 1 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 3 (SB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 4 (NB) | Segment 2 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 5 (SB) | Segment 3 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 6 (NB) | Segment 3 | 2.2 | 1.6 | 1.3 | 1.7 | 6.3% | 18.9% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Alt 2 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 2 (NB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 3 (SB) | Segment 2 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 4 (NB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 5 (SB) | Segment 3 | 2.3 | 1.6 | 1.3 | 1.8 | 6.6% | 20.0% |
| Receptor 6 (NB) | Segment 3 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |

| Alt 3 Mod | | | | | | | |
|--|------------------------|---|--|--|---|-----------------------|-----------------------|
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| Receptor 1 (SB) | Segment 1 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 2 (NB) | Segment 1 | 1.7 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 3 (SB) | Segment 2 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 4 (NB) | Segment 2 | 2.1 | 1.6 | 1.3 | 1.7 | 6.0% | 18.9% |
| Receptor 5 (SB) | Segment 3 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| Receptor 6 (NB) | Segment 3 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Receptor 7 (SB) | Segment 4 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Receptor 8 (NB) | Segment 4 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| Note: 8-Hour CO Concentrations have been rounded to the nearest tenth decimal. | | | | | | | |

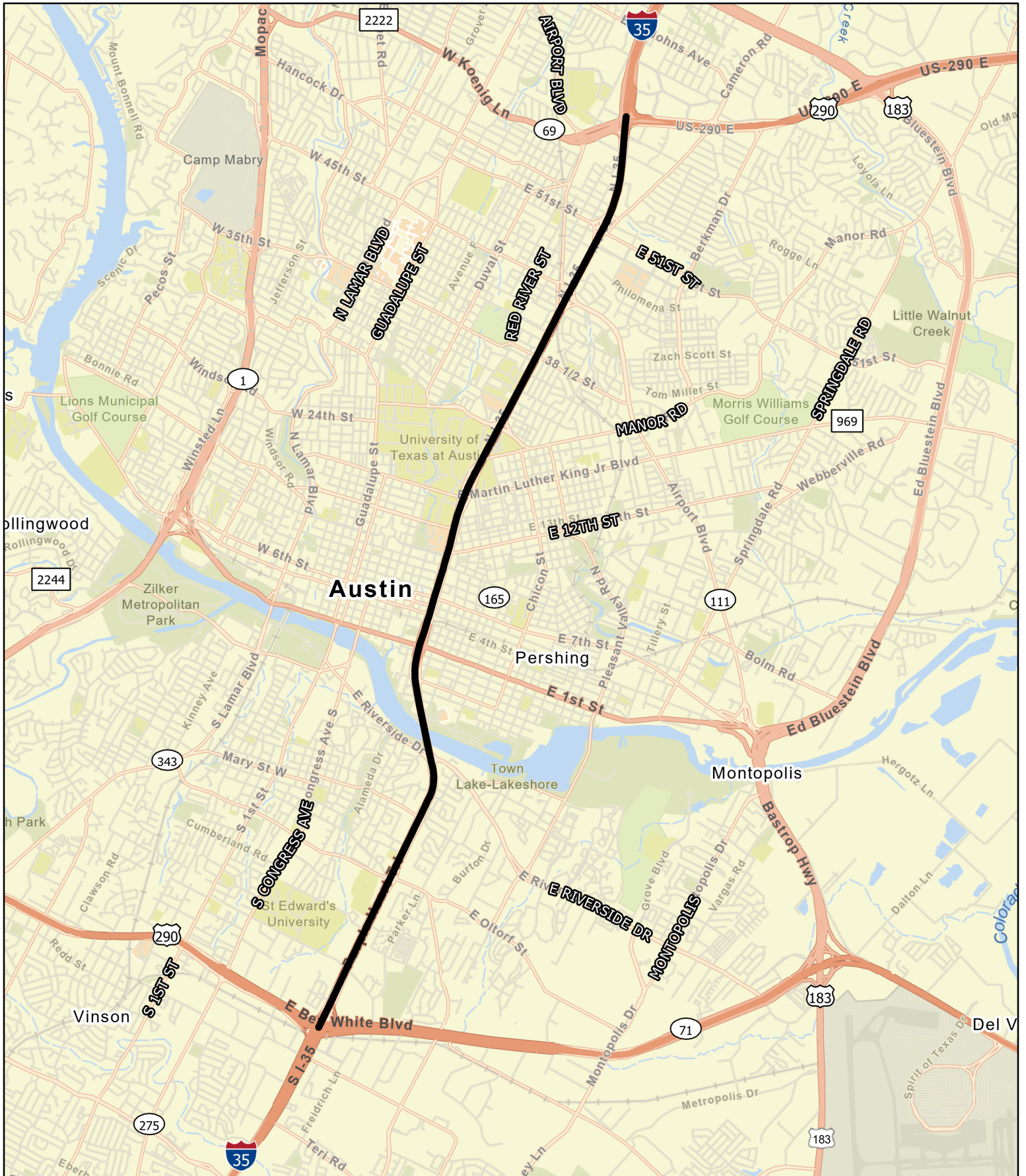
Table 6: Alt 2 and Alt 3 Mod Intersection 1-Hour and 8-Hour CO Concentrations (ETC Year)

| 2030 | | | | | | | |
|--------------------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| Alt 2 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7 th SE | Segment 5 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| 7 th NE | Segment 5 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| 7 th NW | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7 th SW | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS SE | Segment 6 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| RS NE | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS SW | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS NW | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| Alt 3 Mod | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7 th SE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7 th NE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7 th NW | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7 th SW | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS SE | Segment 6 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| RS NE | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS SW | Segment 6 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| RS NW | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |

Table 7: Alt 2 and Alt 3 Mod Intersection 1-Hour and 8-Hour CO Concentrations (Design Year)

| 2050 | | | | | | | |
|-----------|-----------------|--------------------------------------|---|---|--------------------------------------|----------------|----------------|
| Alt 2 | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7th SE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7th NE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7th NW | Segment 5 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| 7th SW | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS SE | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS NE | Segment 6 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| RS SW | Segment 6 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| RS NW | Segment 6 | 1.7 | 1.6 | 1.3 | 1.4 | 4.9% | 15.6% |
| Alt 3 Mod | | | | | | | |
| Receptor | Modeled Segment | 1-Hour CO Concentration (Grams/Mile) | 1-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Background Concentration (Grams/Mile) | 8-Hour CO Concentration (Grams/Mile) | 1-Hour % NAAQS | 8-Hour % NAAQS |
| 7th SE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7th NE | Segment 5 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| 7th NW | Segment 5 | 2.0 | 1.6 | 1.3 | 1.6 | 5.7% | 17.8% |
| 7th SW | Segment 5 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| RS SE | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |
| RS NE | Segment 6 | 1.9 | 1.6 | 1.3 | 1.5 | 5.4% | 16.7% |
| RS SW | Segment 6 | 1.6 | 1.6 | 1.3 | 1.3 | 4.6% | 14.4% |
| RS NW | Segment 6 | 1.8 | 1.6 | 1.3 | 1.4 | 5.1% | 15.6% |

APPENDIX A
Project Location Map



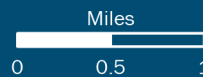
Project Location

I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: ESRI Basemaps 2021

 Project Location



Travis County

APPENDIX B

Traffic Data

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

August 22, 2019

| Description of Location | Base Year | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | |
|--|-----------------------|------|------------|----------|----------------|-----|---|----------------|------|
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | | | |
| | 2030 | 2050 | | | ADT | DHW | Flexible Pavement | Rigid Pavement | SLAB |
| | | | % of ADT | % of DHV | S | N | S | N | |
| Data for Use in Air & Noise Analysis | | | | | | | | | |
| Vehicle Class | | | | | | | | | |
| | | 89.7 | 95.4 | | | | | | |
| | | 1.8 | 0.8 | | | | | | |
| | | 8.5 | 3.8 | | | | | | |
| Light Duty | | | | | | | | | |
| Medium Duty | | | | | | | | | |
| Heavy Duty | | | | | | | | | |
| Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | |
| Description of Location | Base Year | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | |
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | | | |
| | 2030 | 2060 | | | ADT | DHW | Flexible Pavement | Rigid Pavement | SLAB |
| | | | % of ADT | % of DHV | S | N | S | N | |

I-35 (Mainlanes)

Section 1

Mainlanes Cutline Section 1

Travis County

181,550 238,300 51 - 49 7.0 10.3 4.6 0 0 0 3 0 8"

I-35 (Mainlanes)

Section 1

Mainlanes Cutline Section 1

Travis County

181,550 262,450 51 - 49 7.0 10.3 4.6 0 0 0 3 0 8"

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

August 22, 2019

| Description of Location | Base Year | | | | | | Percent Tandem Axles in ATHWLD | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | |
|--|-----------------------|-----------|------------|----------|----------------|-----|--------------------------------|---|---|---|----------------|------|
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | | Flexible Pavement | S | N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHW | | | | | | |
| | | | % | % | % | % | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| | | Base Year | | | | | | | | | | |
| | | % of ADT | % of DHV | | | | | | | | | |
| Light Duty | | 97.4 | 98.0 | | | | | | | | | |
| Medium Duty | | 2.3 | 1.7 | | | | | | | | | |
| Heavy Duty | | 0.3 | 0.3 | | | | | | | | | |
| Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| | | Base Year | | | | | | | | | | |
| | | % of ADT | % of DHV | | | | | | | | | |
| Light Duty | | 97.4 | 98.0 | | | | | | | | | |
| Medium Duty | | 2.3 | 1.7 | | | | | | | | | |
| Heavy Duty | | 0.3 | 0.3 | | | | | | | | | |
| Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| | | Base Year | | | | | | | | | | |
| | | % of ADT | % of DHV | | | | | | | | | |
| Light Duty | | 97.4 | 98.0 | | | | | | | | | |
| Medium Duty | | 2.3 | 1.7 | | | | | | | | | |
| Heavy Duty | | 0.3 | 0.3 | | | | | | | | | |
| Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| Vehicle Class | | | | | | | | | | | | |
| | | Base Year | | | | | | | | | | |
| | | % of ADT | % of DHV | | | | | | | | | |
| Light Duty | | 97.4 | 98.0 | | | | | | | | | |
| Medium Duty | | 2.3 | 1.7 | | | | | | | | | |
| Heavy Duty | | 0.3 | 0.3 | | | | | | | | | |

I-35 (Frontage Roads)

Section 3

Frontage Road Outline Section 3

Travis County

I-35 (Frontage Roads)

Section 3

Frontage Road Outline Section 3

Travis County

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

August 22, 2019

| Description of Location | Base Year | | | | | | Percent Tandem Axles in ATHWLD | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | |
|---|-----------------------|--------|------------|----------|----------------|-----|--------------------------------|---|---|---|----------------|------|
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | | Flexible Pavement | S | N | Rigid Pavement | SLAB |
| | 2030 | 2050 | | | ADT | DHW | | | | | | |
| | | | % | % | % | % | | % | % | % | % | % |
| <u>I-35 (Frontage Roads)</u> Section 4 Frontage Road Outline Section 4 Travis County | 71,050 | 89,450 | 51 - 49 | 7.0 | 2.7 | 2.0 | 0 | 0 | 3 | 0 | 8" | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| Vehicle Class | Base Year | | Base Year | | | | | | | | | |
| | % of ADT | | % of DHV | | | | | | | | | |
| Light Duty | 97.3 | | 98.0 | | | | | | | | | |
| Medium Duty | 2.4 | | 1.8 | | | | | | | | | |
| Heavy Duty | 0.3 | | 0.2 | | | | | | | | | |
| Description of Location | Base Year | | | | | | Percent Tandem Axles in ATHWLD | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | |
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | | Flexible Pavement | S | N | Rigid Pavement | SLAB |
| | 2030 | 2060 | | | ADT | DHW | | | | | | |
| | | | % | % | % | % | | % | % | % | % | % |
| <u>I-35 (Frontage Roads)</u> Section 4 Frontage Road Outline Section 4 Travis County | 71,050 | 98,350 | 51 - 49 | 7.0 | 2.7 | 2.0 | 0 | 0 | 3 | 0 | 8" | |

TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

August 22, 2019

| Description of Location | Base Year | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period (2030 to 2050) | | | | |
|--------------------------------------|--------------------------------------|----------|------------|----------|----------------|-----|--------|--------------------------------|---|---|----------------|----|------|
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | | Rigid Pavement | | SLAB |
| | 2030 | 2050 | | | ADT | DHW | | | S | N | S | N | |
| | Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| <u>Section 5</u> | | | | | | | | | | | | | |
| Frontage Road Culline Section 5 | 48,400 | 60,200 | 51 - 49 | 5.9 | 3.2 | 2.4 | 0 | 0 | 0 | 3 | 0 | 8" | |
| Travis County | | | | | | | | | | | | | |
| Data for Use in Air & Noise Analysis | | | | | | | | | | | | | |
| Vehicle Class | Base Year | | | | | | | | | | | | |
| | % of ADT | % of DHV | | | | | | | | | | | |
| Light Duty | 96.8 | 97.6 | | | | | | | | | | | |
| Medium Duty | 2.8 | 2.1 | | | | | | | | | | | |
| Heavy Duty | 0.4 | 0.3 | | | | | | | | | | | |
| Description of Location | Base Year | | | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period (2030 to 2060) | | | | |
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | | Rigid Pavement | | SLAB |
| | 2030 | 2060 | | | ADT | DHW | | | S | N | S | N | |
| | Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| <u>Section 5</u> | | | | | | | | | | | | | |
| Frontage Road Culline Section 5 | 48,400 | 66,250 | 51 - 49 | 5.9 | 3.2 | 2.4 | 0 | 0 | 0 | 3 | 0 | 8" | |
| Travis County | | | | | | | | | | | | | |

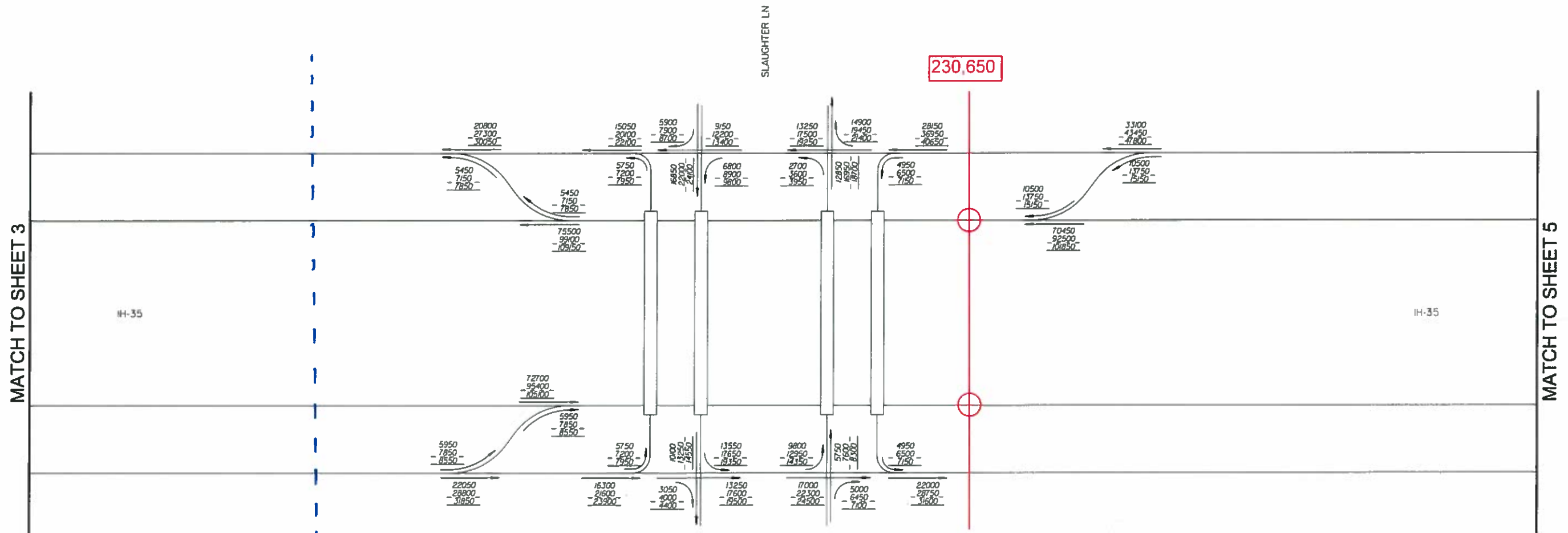
TRAFFIC ANALYSIS FOR HIGHWAY DESIGN

Austin District

August 22, 2019

| Description of Location | Base Year | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 20 Year Period | | | | | | |
|--|--------------------------------------|------|------------|----------|----------------|-----|--|--------------------------------|-------------------|---|----------------|---|------|
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | | Rigid Pavement | | SLAB |
| | 2030 | 2050 | | | ADT | DHV | | | S | N | S | N | |
| | Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| I-35 (Frontage Roads) Section 6 Frontage Road Culline Section 6 Travis County | 84,400 | | 104,500 | 51 - 49 | 5.9 | 2.6 | 2.0 | 0 | 0 | 0 | 3 | 0 | 8" |
| | Vehicle Class | | | | | | | | | | | | |
| | % of ADT | | Base Year | | % of DHV | | | | | | | | |
| | 97.4 | | 98.0 | | 98.0 | | | | | | | | |
| 2.3 | | 1.7 | | 1.7 | | | | | | | | | |
| 0.3 | | 0.3 | | 0.3 | | | | | | | | | |
| I-35 (Frontage Roads) Section 6 Frontage Road Culline Section 6 Travis County | Base Year | | | | | | Total Number of Equivalent 18k Single Axle Load Applications One Direction Expected for a 30 Year Period | | | | | | |
| | Average Daily Traffic | | Dir Dist % | K Factor | Percent Trucks | | ATHWLD | Percent Tandem Axles in ATHWLD | Flexible Pavement | | Rigid Pavement | | SLAB |
| | 2030 | 2060 | | | ADT | DHV | | | S | N | S | N | |
| | Data for Use in Air & Noise Analysis | | | | | | | | | | | | |
| I-35 (Frontage Roads) Section 6 Frontage Road Culline Section 6 Travis County | 84,400 | | 112,550 | 51 - 49 | 5.9 | 2.6 | 2.0 | 0 | 0 | 0 | 3 | 0 | 8" |
| | Vehicle Class | | | | | | | | | | | | |
| | % of ADT | | Base Year | | % of DHV | | | | | | | | |
| | 97.4 | | 98.0 | | 98.0 | | | | | | | | |
| 2.3 | | 1.7 | | 1.7 | | | | | | | | | |
| 0.3 | | 0.3 | | 0.3 | | | | | | | | | |

NO-BUILD CONFIGURATION



Frontage RD
cutline
Section 2

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

DRAFT

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES (SHEET 4 OF 28)

| | | | | | |
|-----------------|----------------|-------------------|----------|-------------|--|
| SCALE: N. T. S. | | | | PROJECT NO. | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 4 | |

NO-BUILD CONFIGURATION

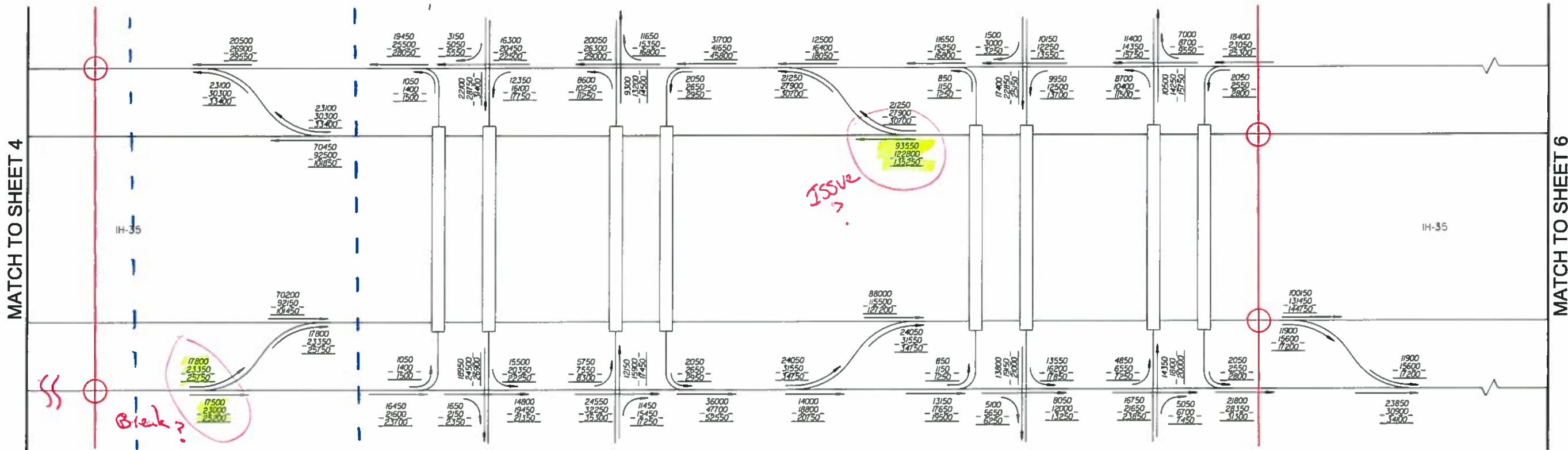


ML
Eobline
Section 1

WILLIAM CANNON DR

STASSNEY LN

190,050



MATCH TO SHEET 4

MATCH TO SHEET 6

Break?

ISSUE?

113,900

Frontage to
cutline
Section 3

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

DRAFT

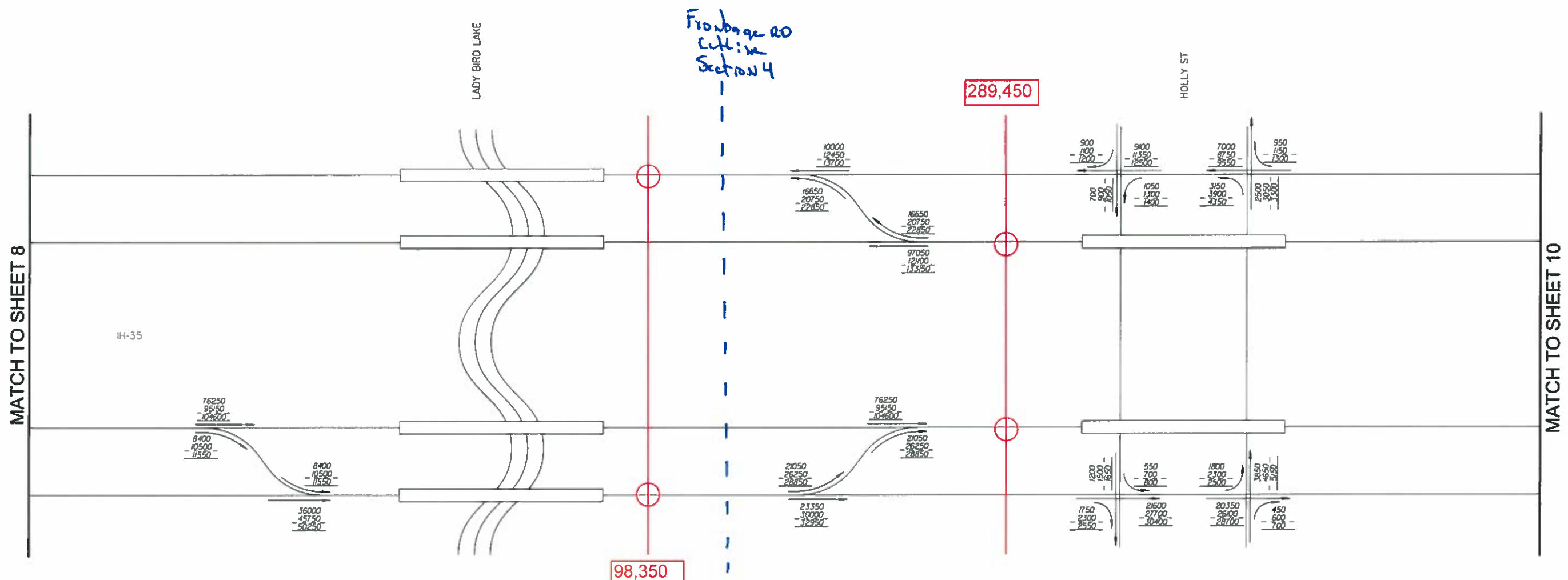
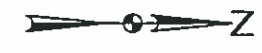
LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

| | | | | |
|------------------------|---------|----------------|--------------------|-----------|
| | | | | |
| | | | | |
| CAPITAL EXPRESS | | | | |
| NO-BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES | | | | |
| (SHEET 5 OF 28) | | | | |
| SCALE: N. T. S. | | PROJECT NO. | | |
| OWN: TH | CRD: HH | STATE DISTRICT | FED. RD. DIST. NO. | COUNTY |
| TEXAS | 14 | 6 | | TRAVIS |
| CONTROL | SECTION | JOB | HY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

DRAFT

- LEGEND
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

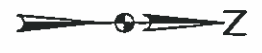
NOT TO SCALE



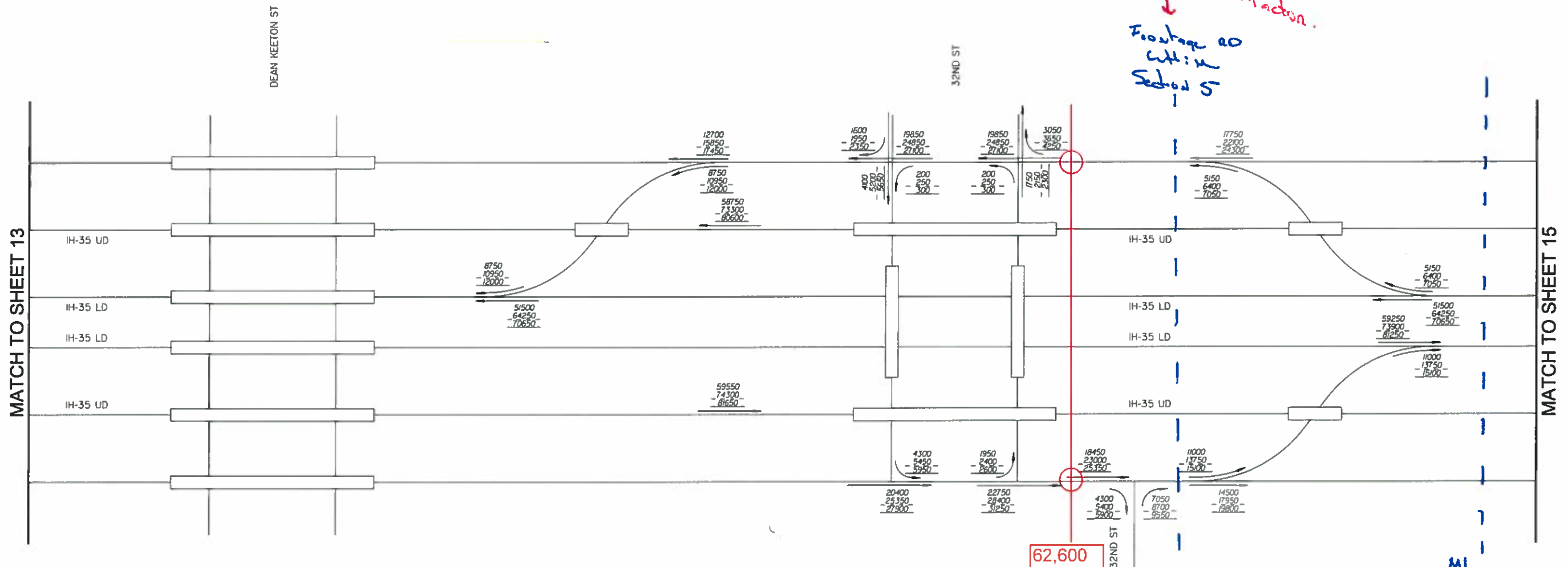
| | | | | |
|------------------------|----------------|-------------------|----------|-----------|
| CAPITAL EXPRESS | | | | |
| NO-BUILD CONFIGURATION | | | | |
| 24 HOUR VOLUMES | | | | |
| (SHEET 9 OF 28) | | | | |
| SCALE: N. T. S. | | PROJECT NO. | | |
| DWN: TH | CRD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 9 |

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NO-BUILD CONFIGURATION



30 > 20 growth Factor.
 ↓
 Footage 20
 within
 Section 5



ML
 within
 Section 2

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

DRAFT

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



CAPITAL EXPRESS
 NO-BUILD CONFIGURATION
 24 HOUR VOLUMES
 (SHEET 14 OF 28)

| | | | |
|-----------------|---------|----------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| DWN: TH | CRD: HH | STATE DISTRICT | FED. RD. DIV. NO. |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 14 |

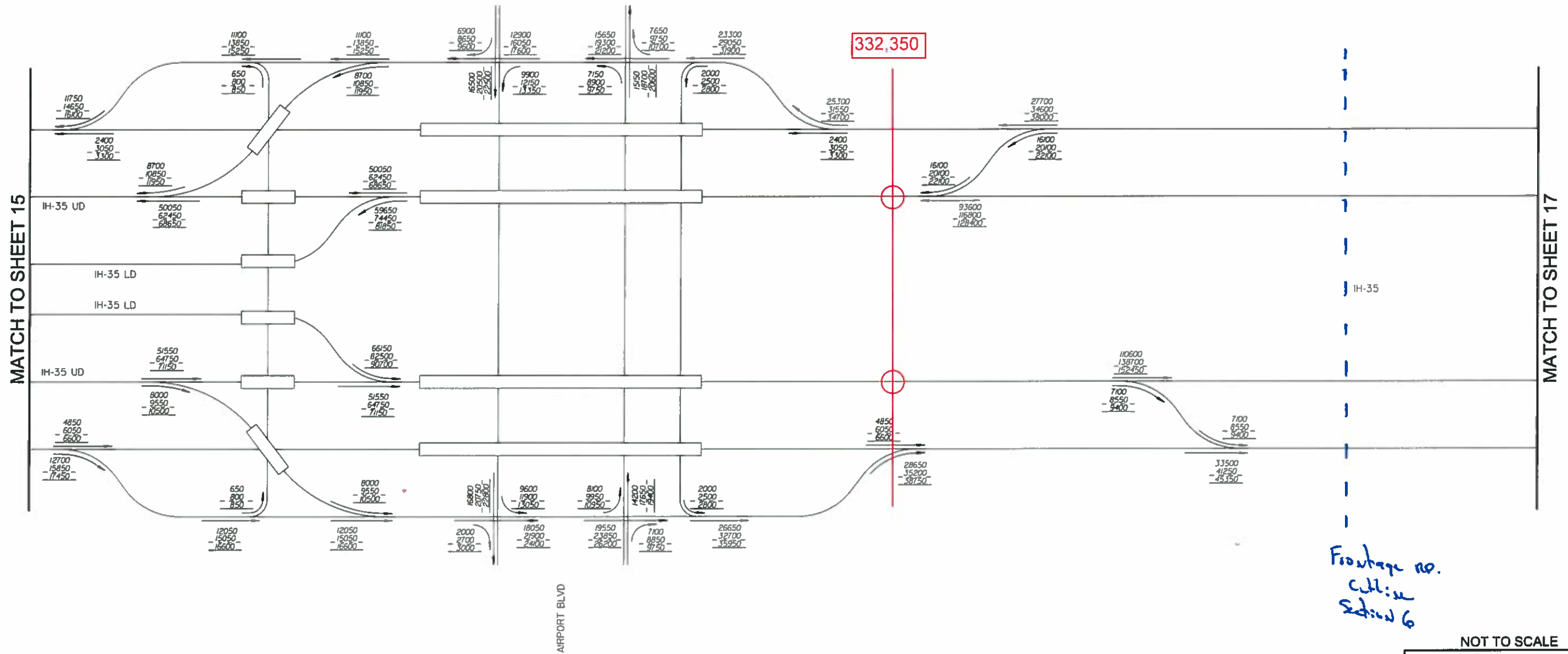
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NO-BUILD CONFIGURATION



332,350

Frontage no. collision section 6

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

DRAFT

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION

24 HOUR VOLUMES

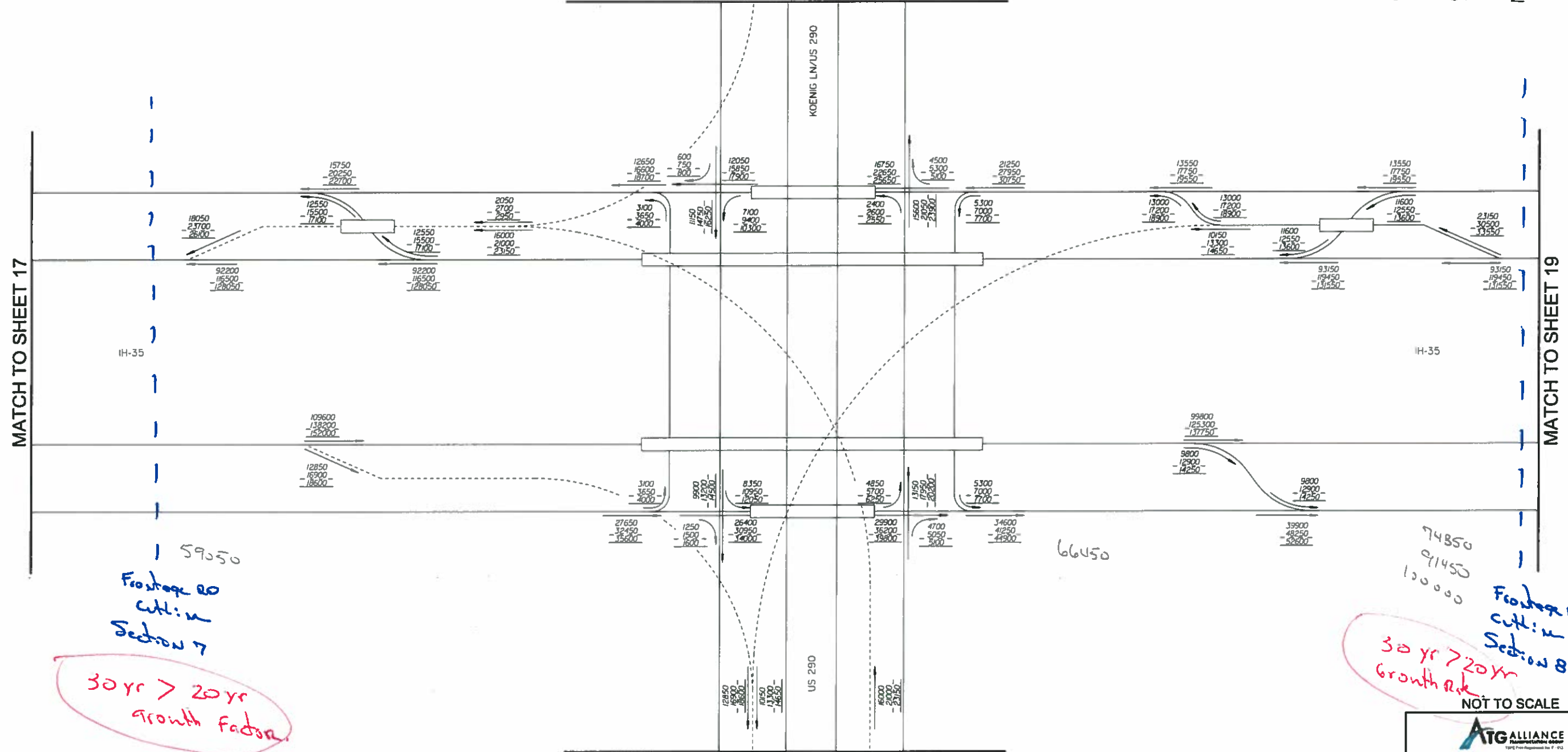
(SHEET 16 OF 28)

| | | | |
|-----------------|----------|---------------|--------------------|
| SCALE: N. T. S. | | PROJECT NO. | |
| STATE | DISTRICT | FED. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

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NO-BUILD CONFIGURATION

MATCH TO SHEET 27



MATCH TO SHEET 17

MATCH TO SHEET 19

MATCH TO SHEET 28

DRAFT

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

59050
Frostage RD
cut: w
Section 7
30 yr > 20 yr
growth factor

66450

74850
91450
130000
Frostage RD
cut: w
Section 8
30 yr > 20 yr
Growth Rate

NOT TO SCALE

ATG ALLIANCE
TRANSPORTATION

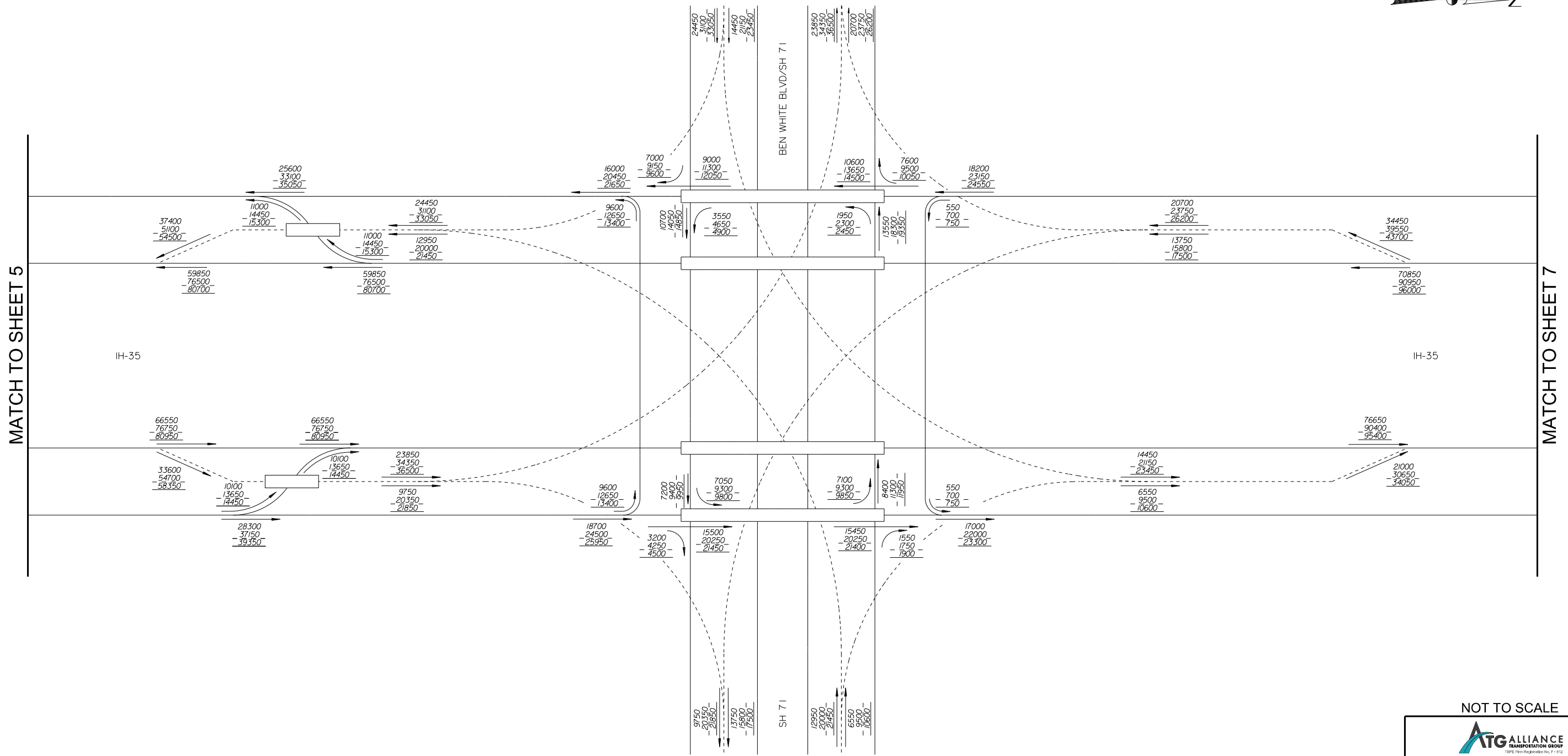
Texas Department of Transportation

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 18 OF 28)

SCALE: N. T. S. PROJECT NO.

| | | | | | | |
|----------|---------|--------|---------------|---------------|-----------|--------|
| DWG. TH. | STATE | COUNTY | FED. DISTRICT | FED. DIV. NO. | ROUTE NO. | COUNTY |
| | TEXAS | 14 | 6 | | | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | | |
| 5000 | 00 | 106 | IH-35 | 18 | | |

NO-BUILD CONFIGURATION




MATCH TO SHEET 5

MATCH TO SHEET 7


2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

NOT TO SCALE



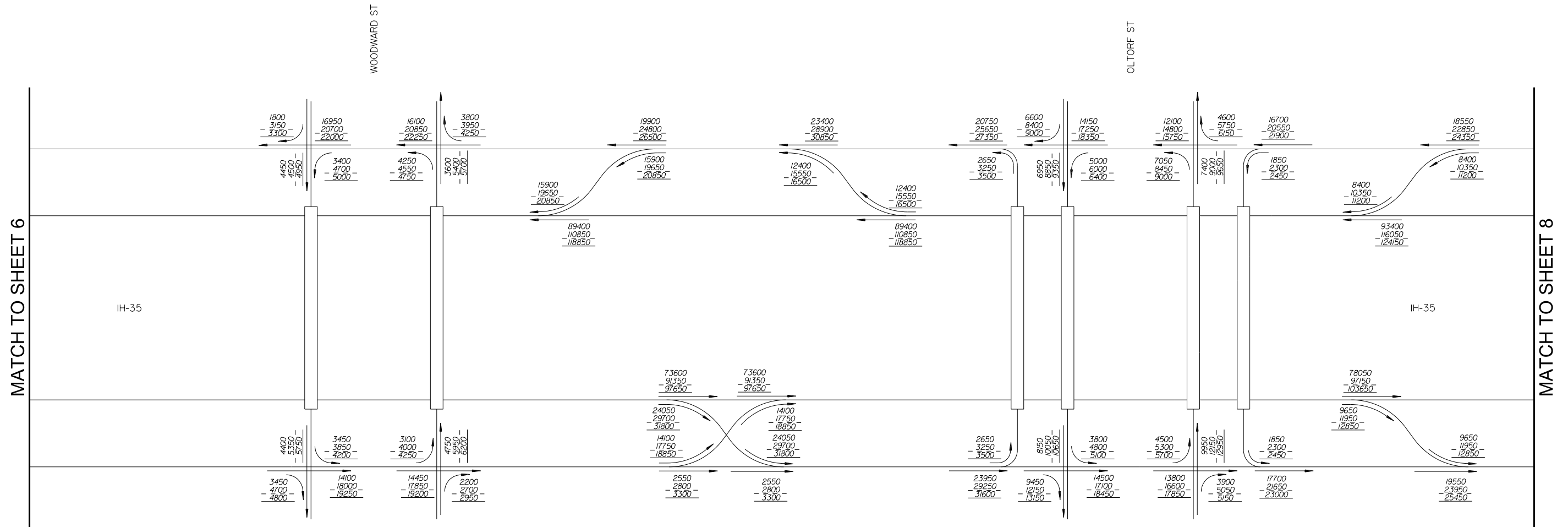
TRANSPORTATION GROUP



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 6 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 6 |

NO-BUILD CONFIGURATION



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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- - - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

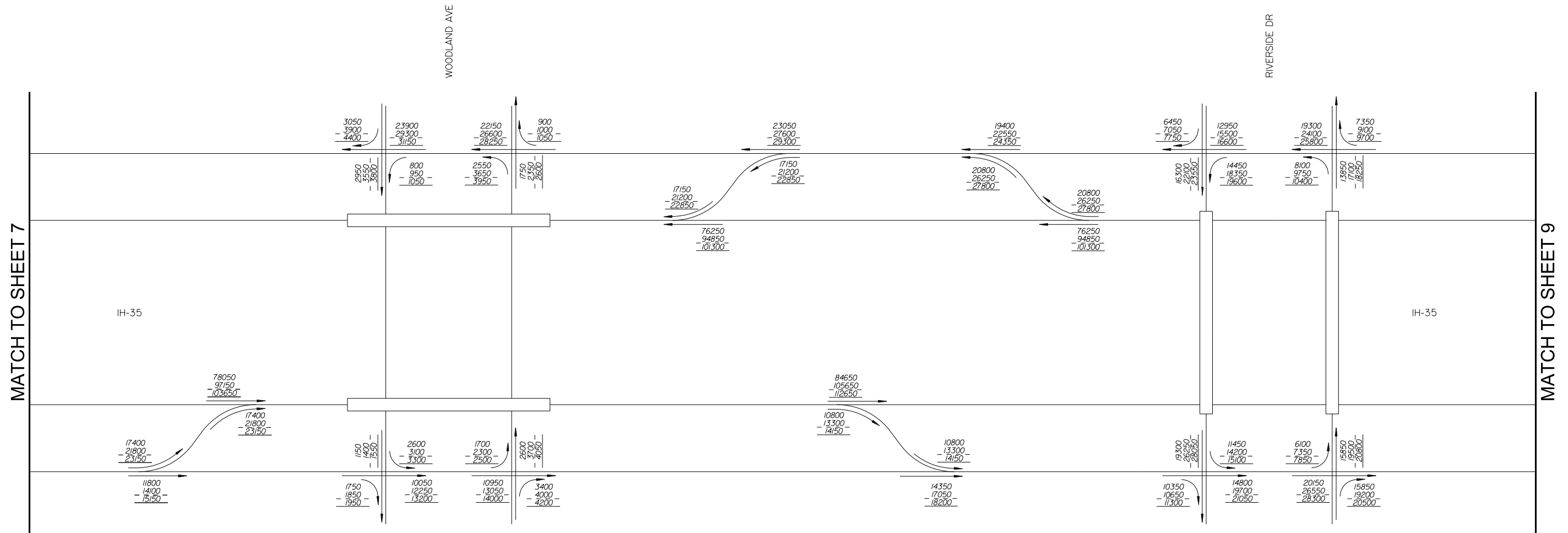
NOT TO SCALE



CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 7 OF 28)

| | | | | | |
|------------------|----------------|---------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. NO. | COUNTY | |
| TEXAS | 14 | 6 | | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 7 | |

NO-BUILD CONFIGURATION



IH-35

IH-35

MATCH TO SHEET 7

MATCH TO SHEET 9

WOODLAND AVE


RIVERSIDE DR

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



TRANSPORTATION GROUP



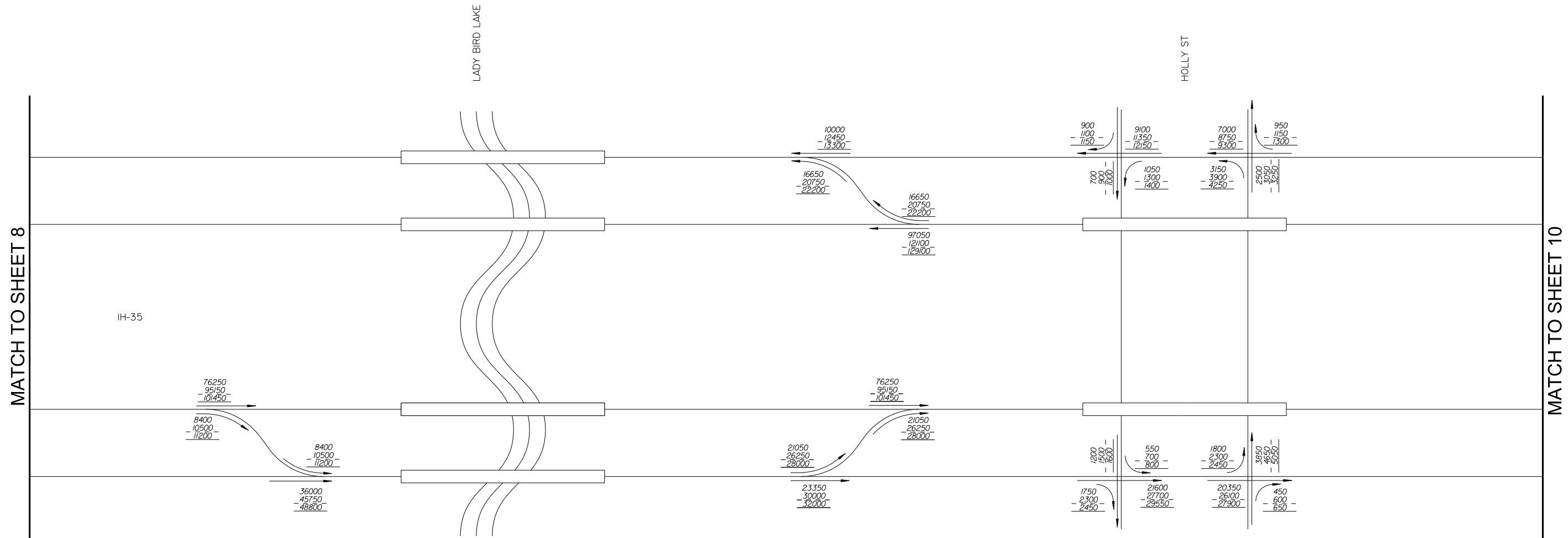
Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 8 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 8 |

NO-BUILD CONFIGURATION



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THouston

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1/25/2019

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

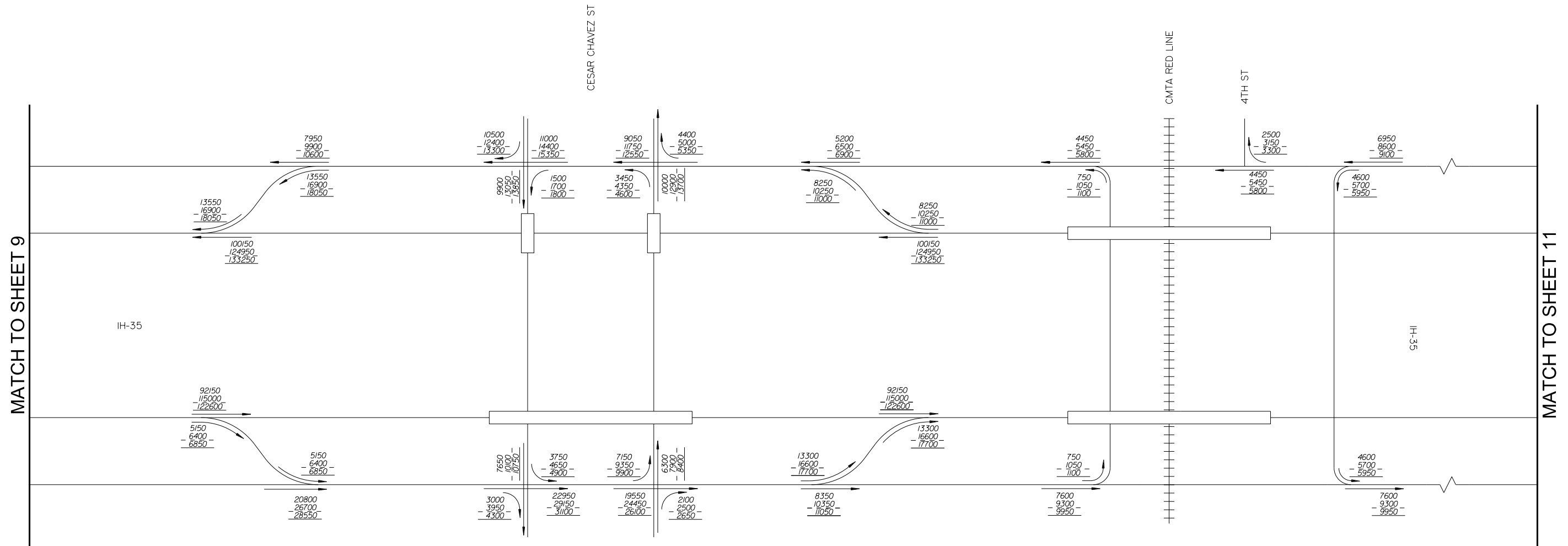
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 9 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 9 |

NO-BUILD CONFIGURATION





2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
1000 - 2050 ADT
1000 - 2060 ADT
LD - LOWER DECK
UD - UPPER DECK
→ TRAVEL DIRECTION

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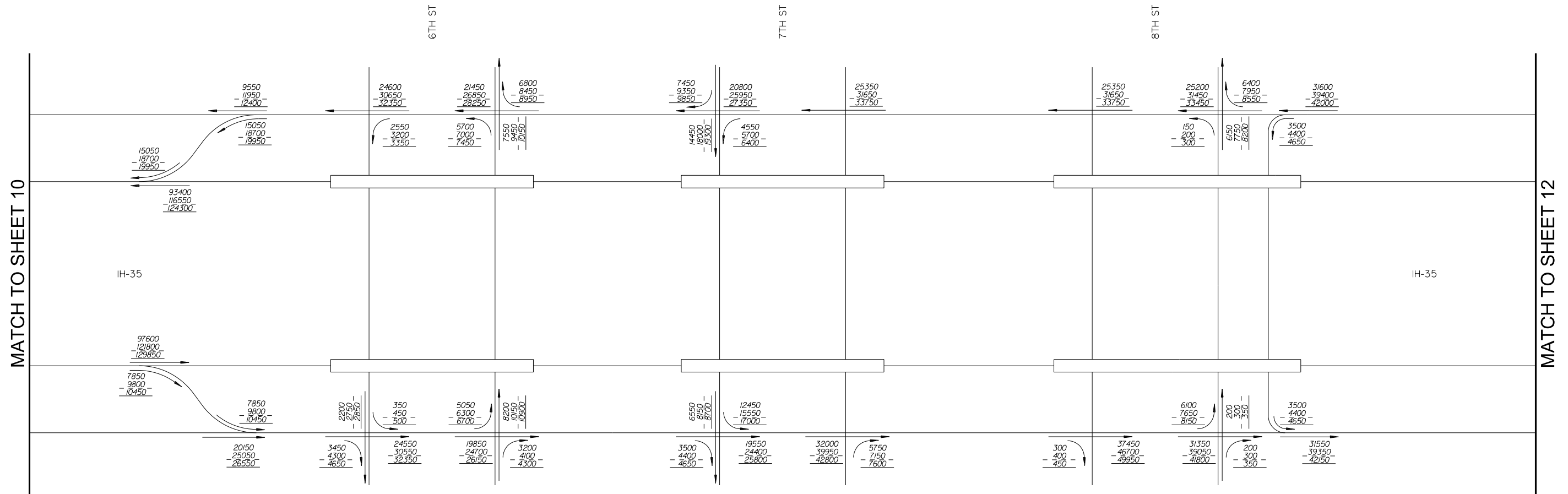
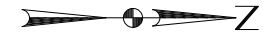
NOT TO SCALE

CAPITAL EXPRESS
 NO-BUILD CONFIGURATION
 24 HOUR VOLUMES
 (SHEET 10 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 10 |

NO-BUILD CONFIGURATION



MATCH TO SHEET 10

MATCH TO SHEET 12

2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

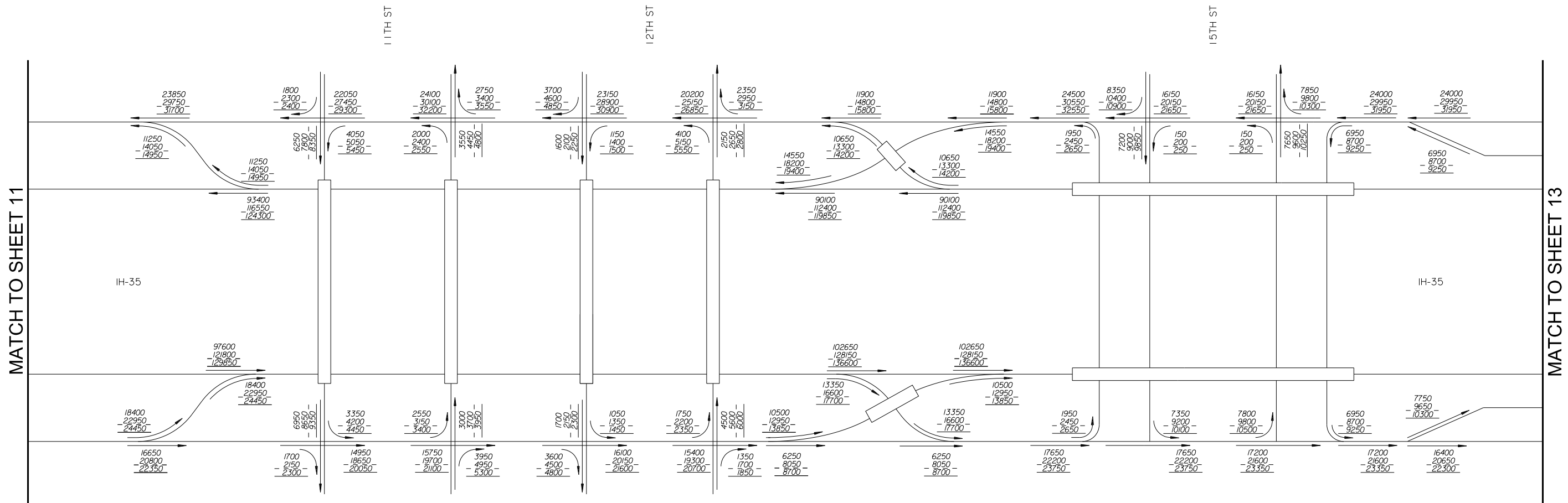


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 11 OF 28)

| | | | | | |
|------------------|----------------|-------------------|----------|-------------|--|
| SCALE : N. T. S. | | | | PROJECT NO. | |
| DWN: TH | CKD: HH | | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS | 14 | 6 | TRAVIS | | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 | 00 | 106 | IH-35 | 11 | |

NO-BUILD CONFIGURATION



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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

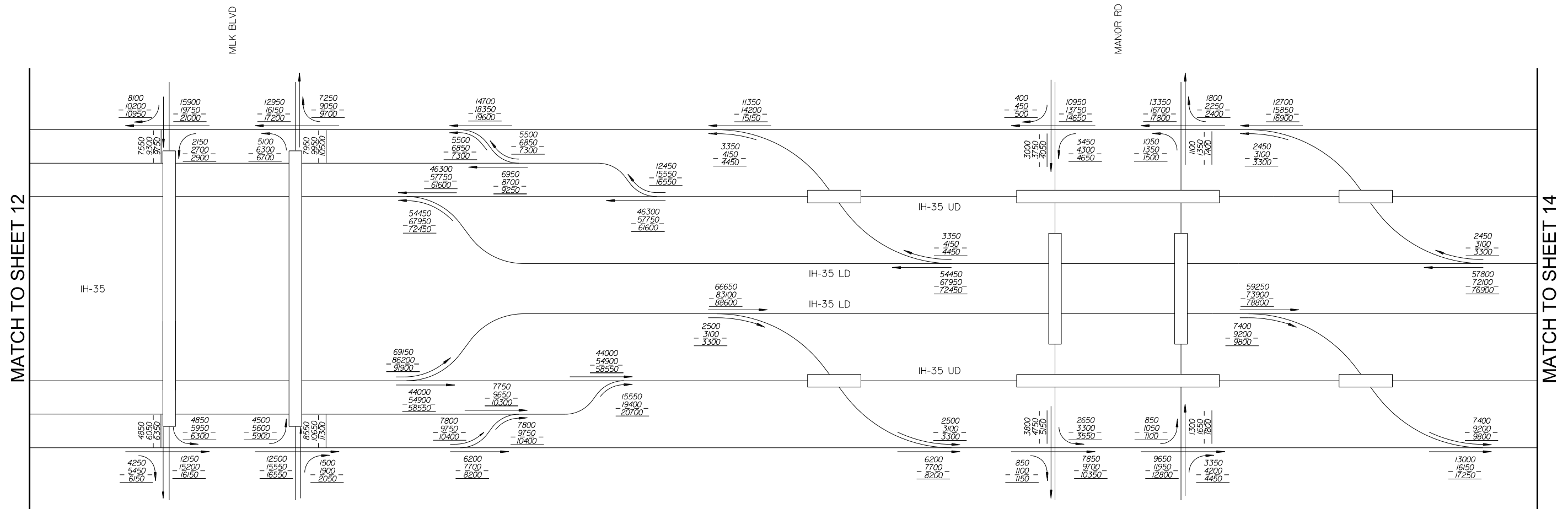
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 12 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 12 |

NO-BUILD CONFIGURATION




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2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



TRANSPORTATION GROUP



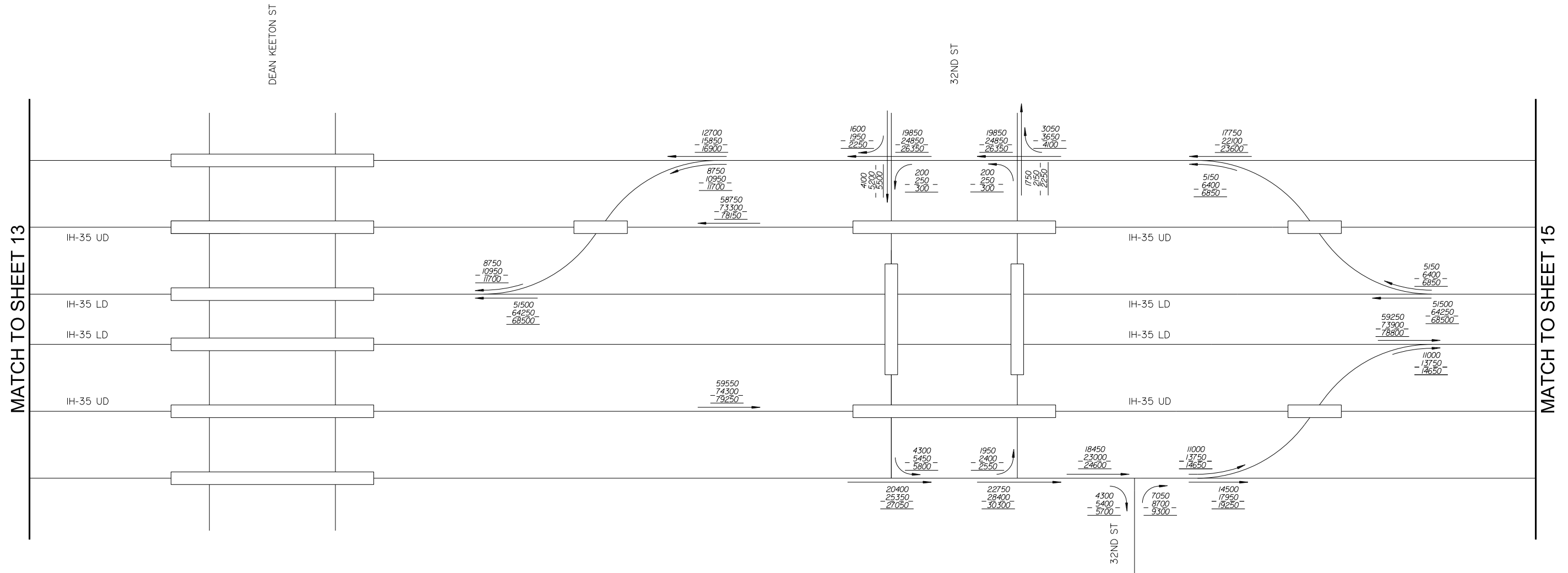
Texas Department of Transportation

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 13 OF 28)

| | | | |
|------------------|---------|-------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE | FED. RD. DISTRICT |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 13 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

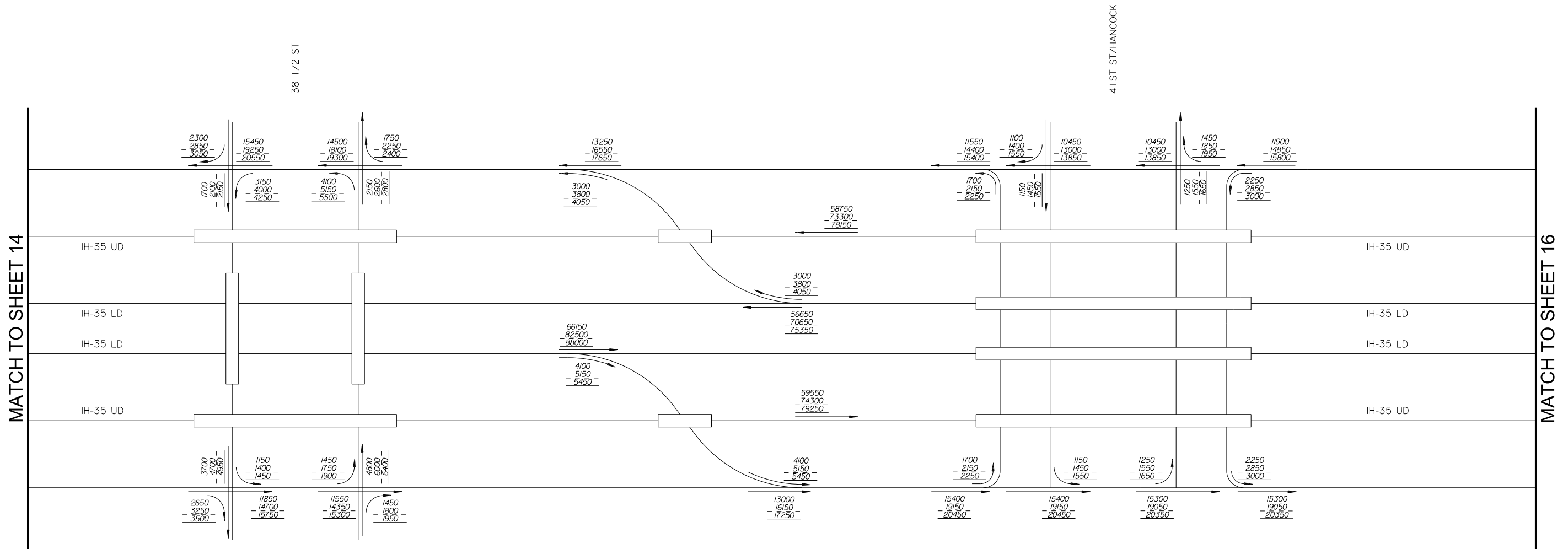


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 14 OF 28)

| | | | | |
|------------------|----------------|---------------|------------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. DIV. NO. | RD. COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 14 |



NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - LD - LOWER DECK
 - UD - UPPER DECK
 - TRAVEL DIRECTION

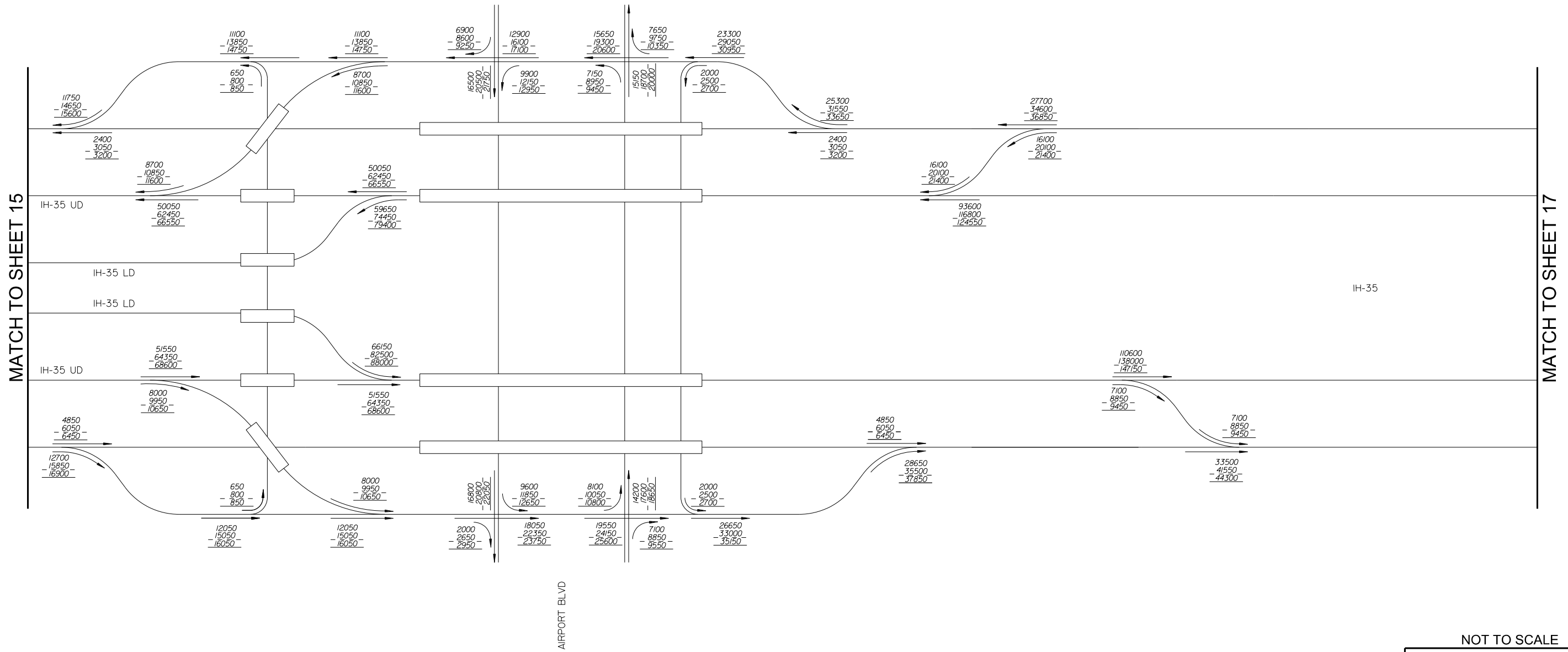
NOT TO SCALE

CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 15 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 15 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

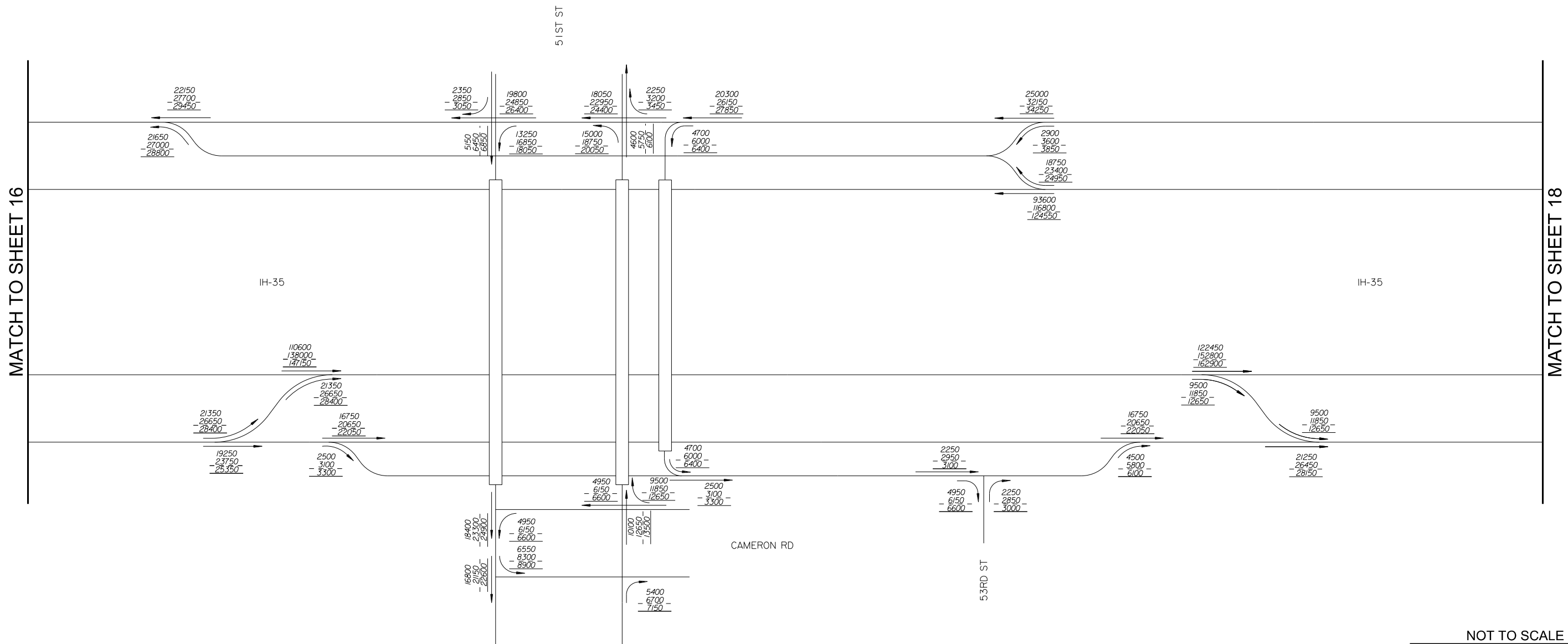


CAPITAL EXPRESS NO-BUILD CONFIGURATION 24 HOUR VOLUMES

(SHEET 16 OF 28)

| | | | | |
|------------------|----------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 16 |

NO-BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE

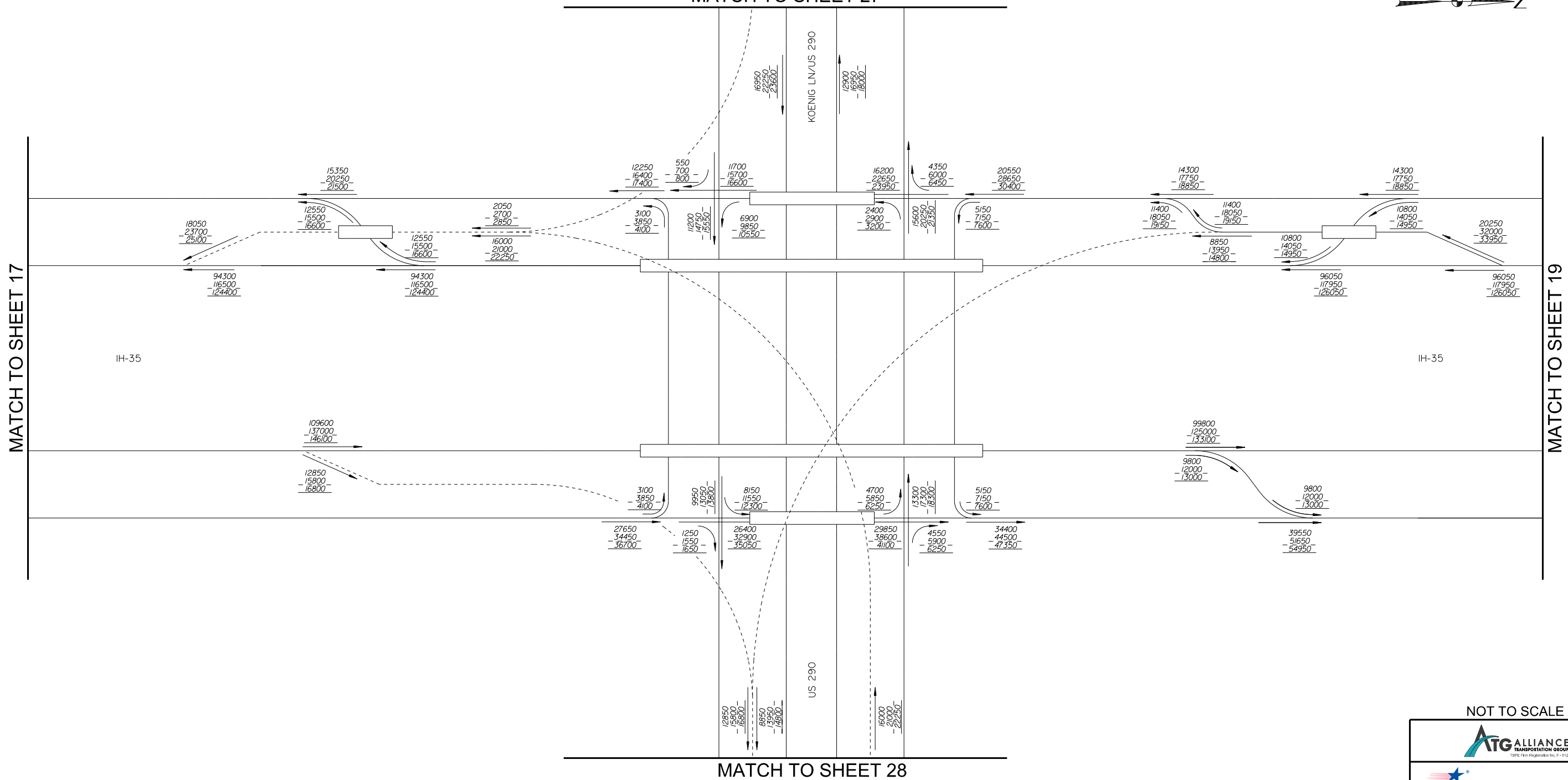


CAPITAL EXPRESS
NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 17 OF 28)

| | | | | |
|------------------|----------------|-------------------|----------|-----------|
| SCALE : N. T. S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 17 |

NO-BUILD CONFIGURATION

MATCH TO SHEET 27




2030, 2050, 2060 FORECASTED NO-BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183


LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT
- LD - LOWER DECK
- UD - UPPER DECK
- TRAVEL DIRECTION

NOT TO SCALE



ATG ALLIANCE
TRANSPORTATION GROUP



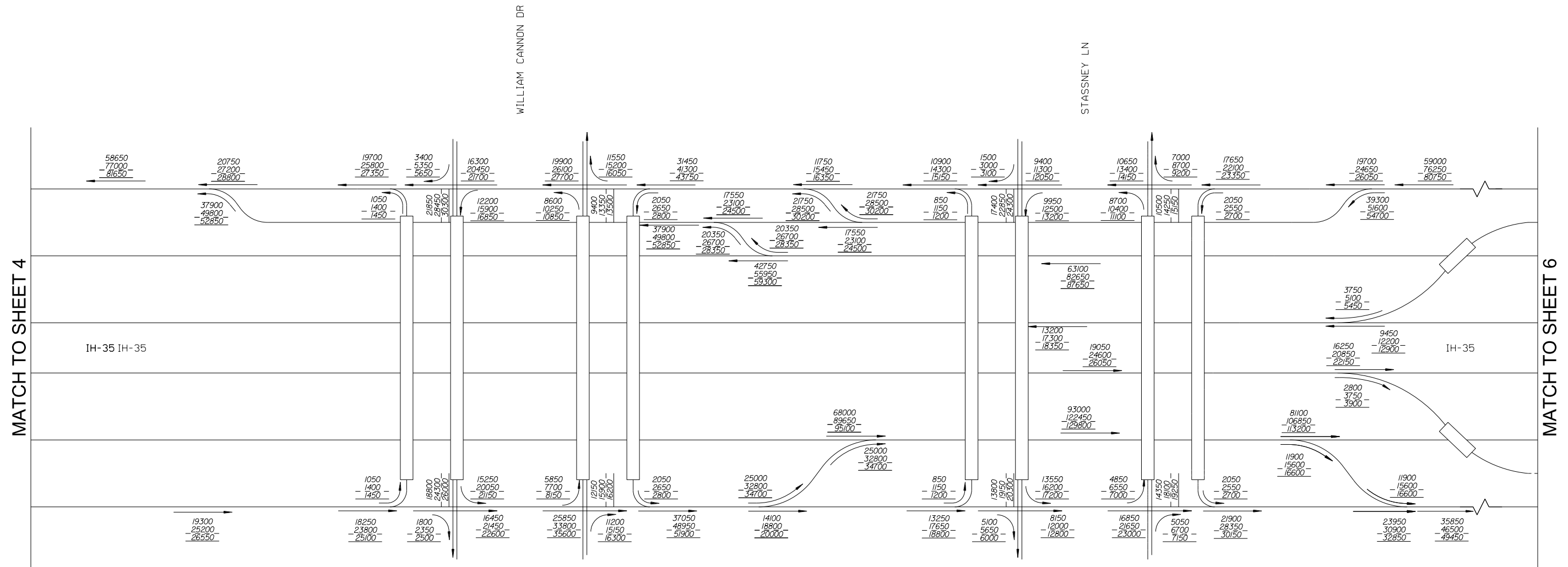
TEXAS DEPARTMENT OF TRANSPORTATION

CAPITAL EXPRESS

NO-BUILD CONFIGURATION
24 HOUR VOLUMES
(SHEET 18 OF 28)

| | | | |
|------------------|----------------|-------------------|--------------------|
| SCALE : N. T. S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

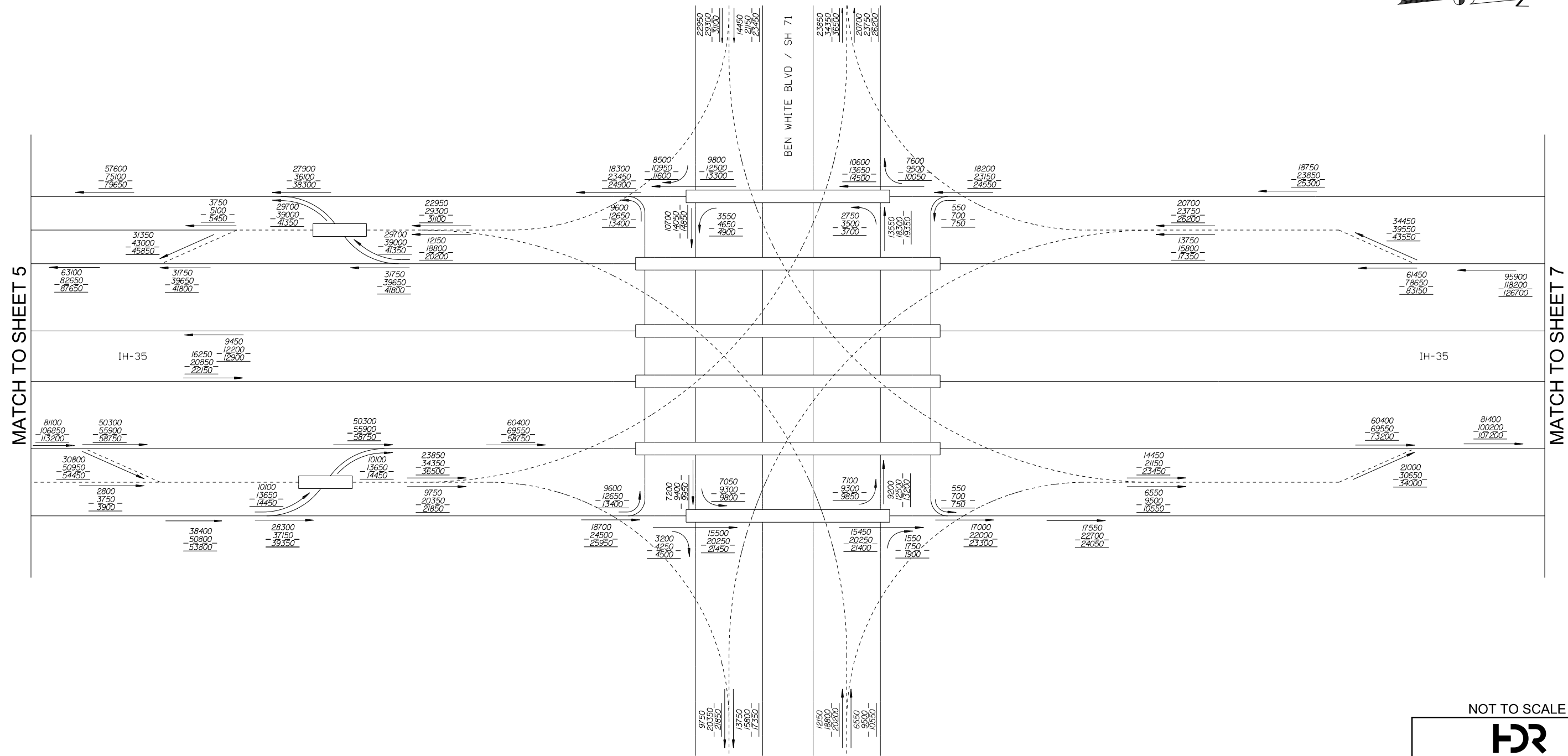


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 5 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

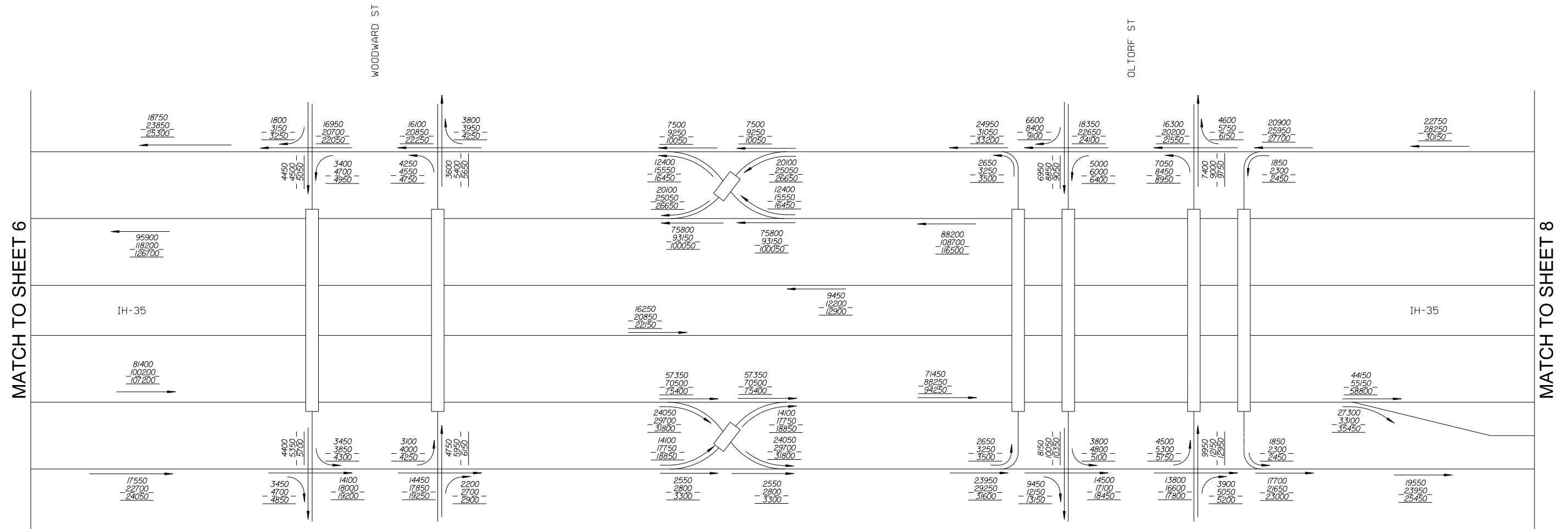
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 6 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 6 |


BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



HDR

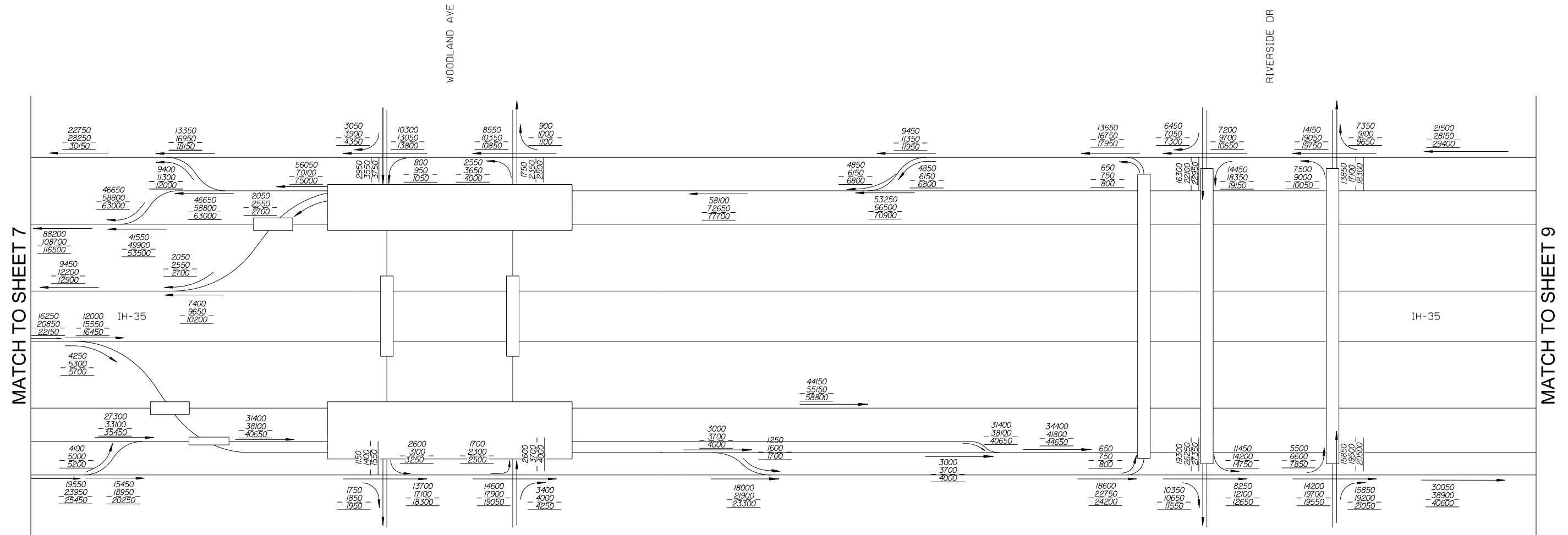


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 7 OF 28)

| | | | |
|-----------------|-------------------|-------------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS 14 | 6 | TRAVIS | |
| CONTROL SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 00 | 106 | IH-35 | 7 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

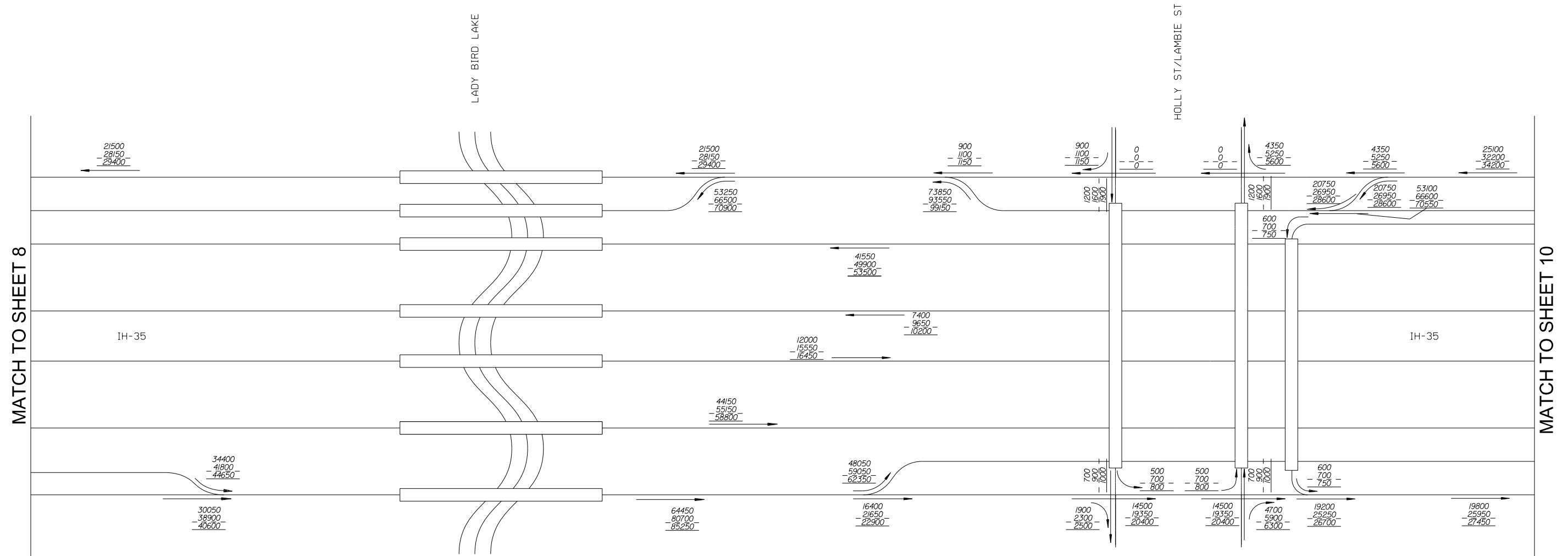


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 8 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 8 |

BUILD CONFIGURATION




MATCH TO SHEET 8

MATCH TO SHEET 10

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

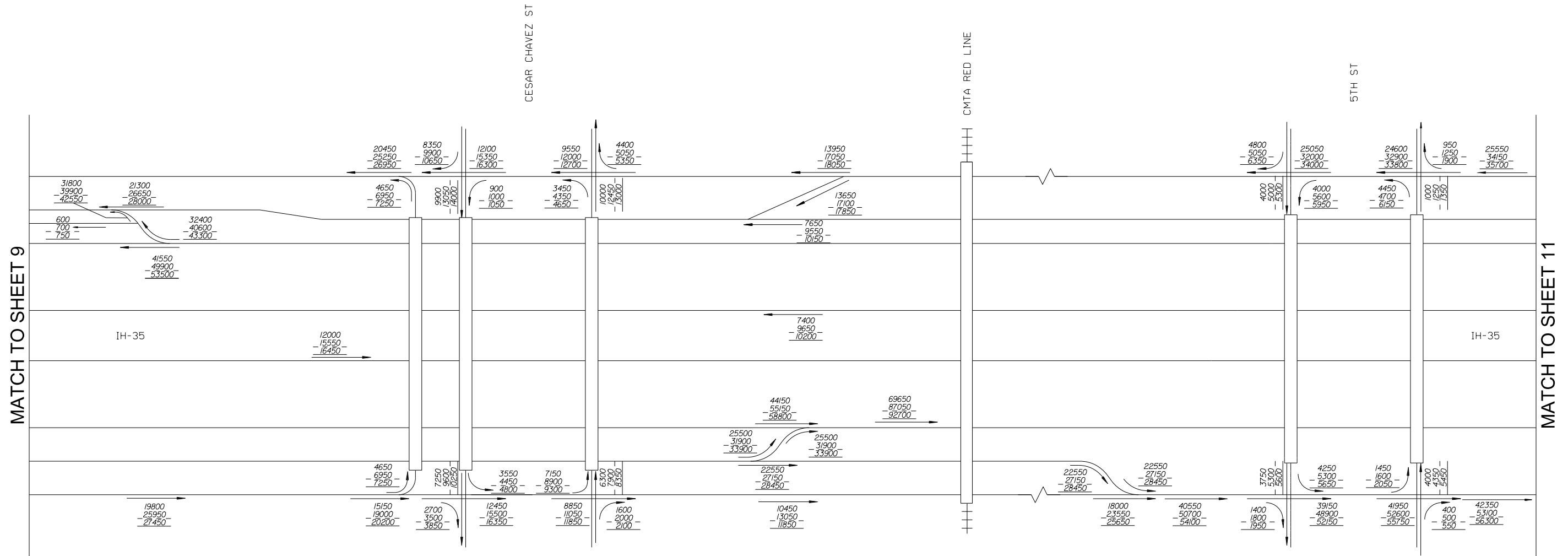


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 9 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 9 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

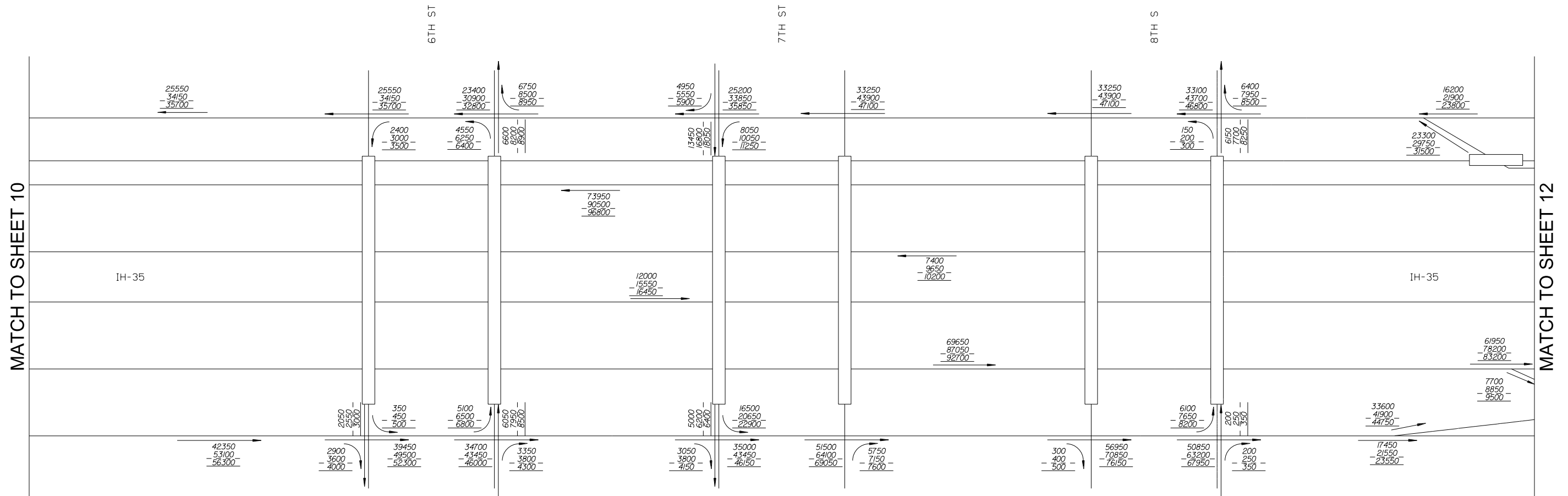
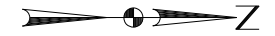
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 10 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 10 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

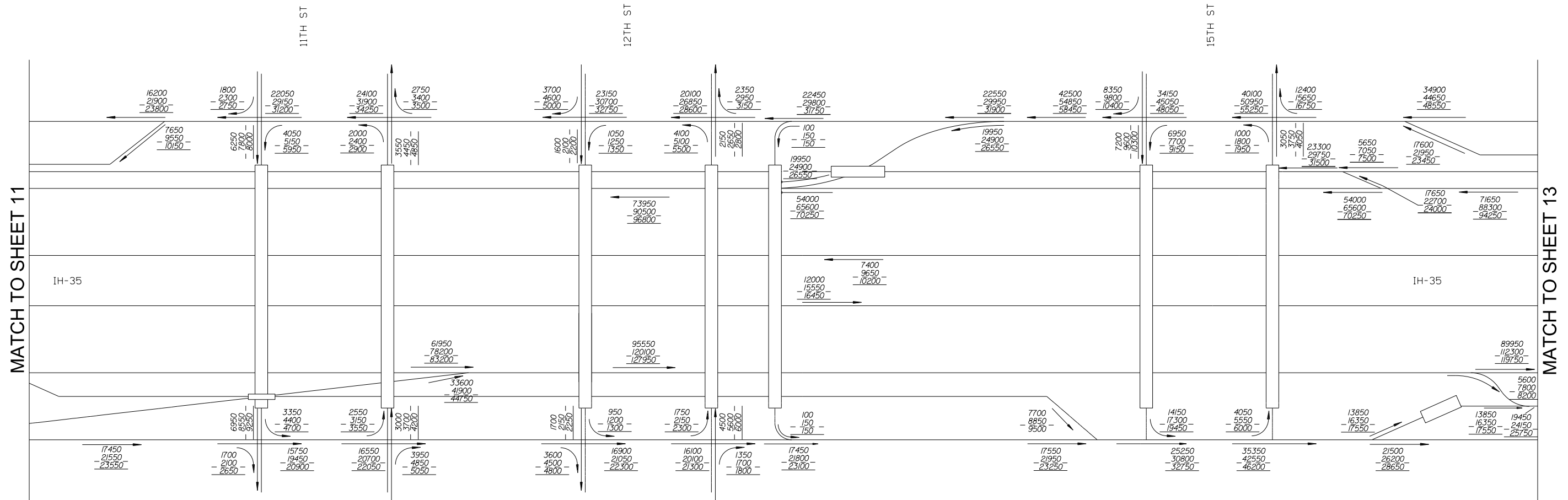
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 11 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 11 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

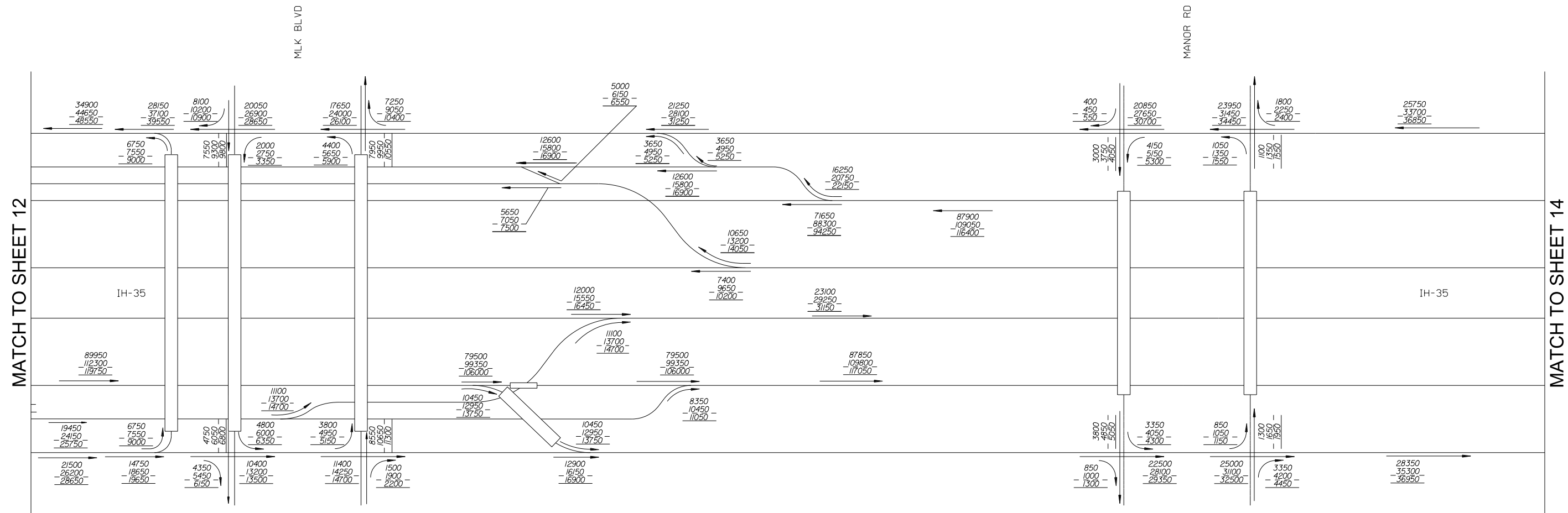


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 12 OF 28)

| | | | |
|-----------------|-------------------|-------------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS 14 | 6 | TRAVIS | |
| CONTROL SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 00 | 106 | IH-35 | 12 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

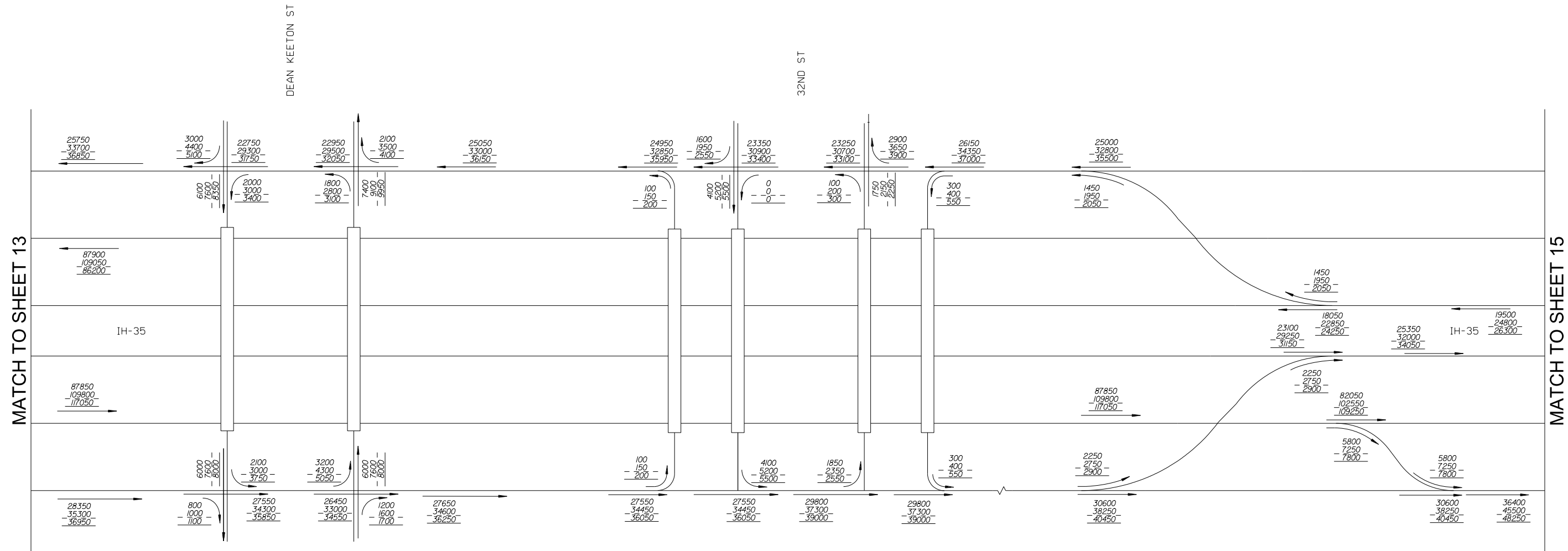
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 13 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 13 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

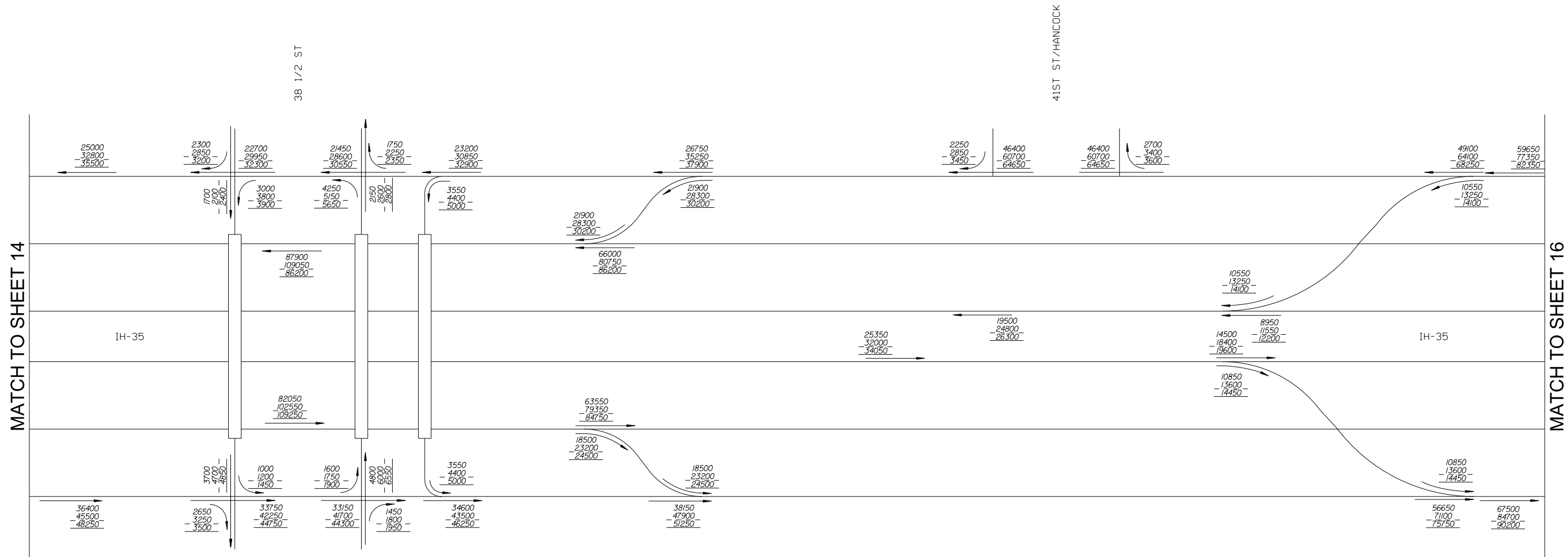


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 14 OF 28)

| | | | | |
|---------------|----------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 14 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

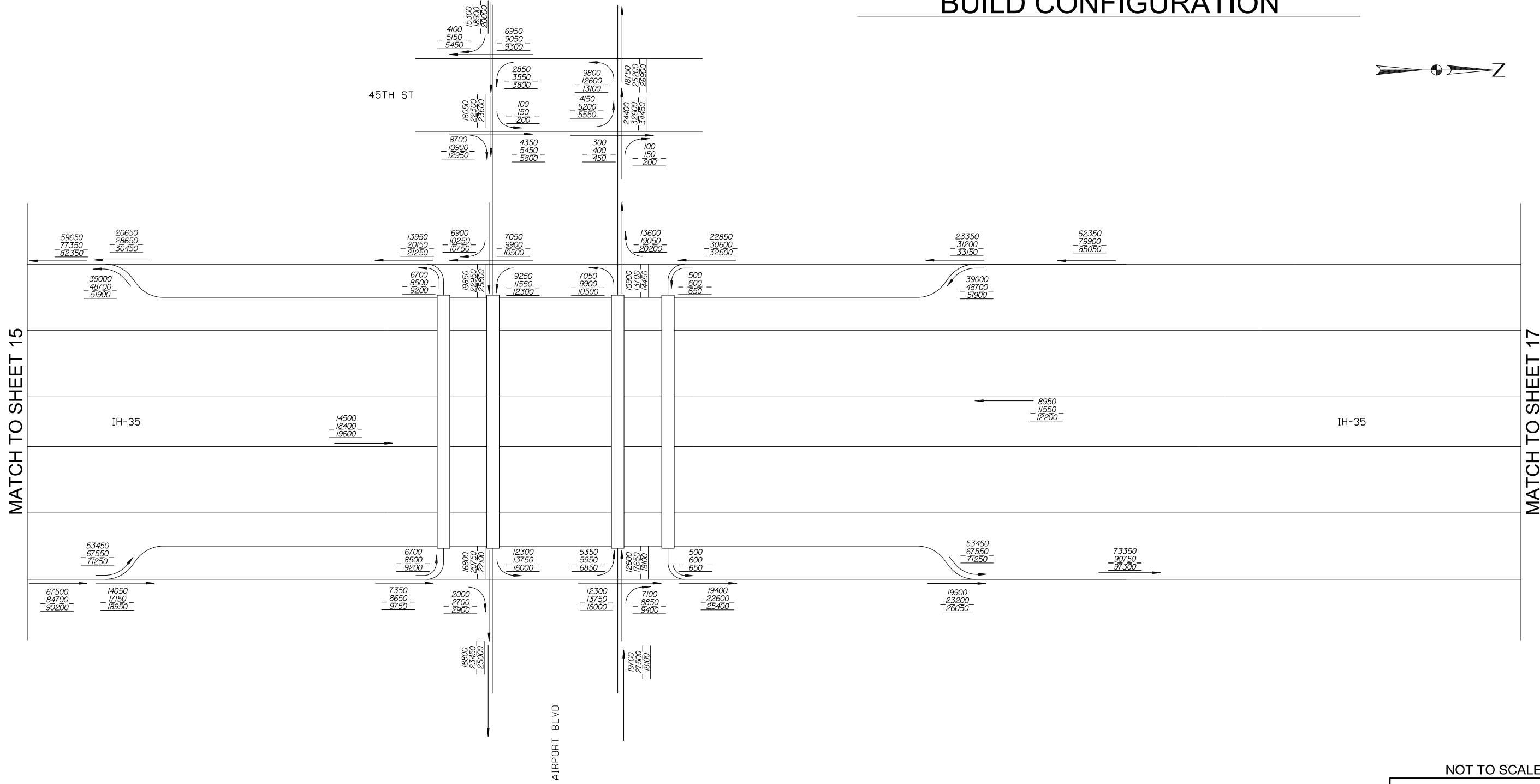
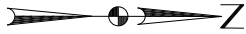
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 15 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 15 |


BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000_ - 2050 ADT
 1000_ - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



HR

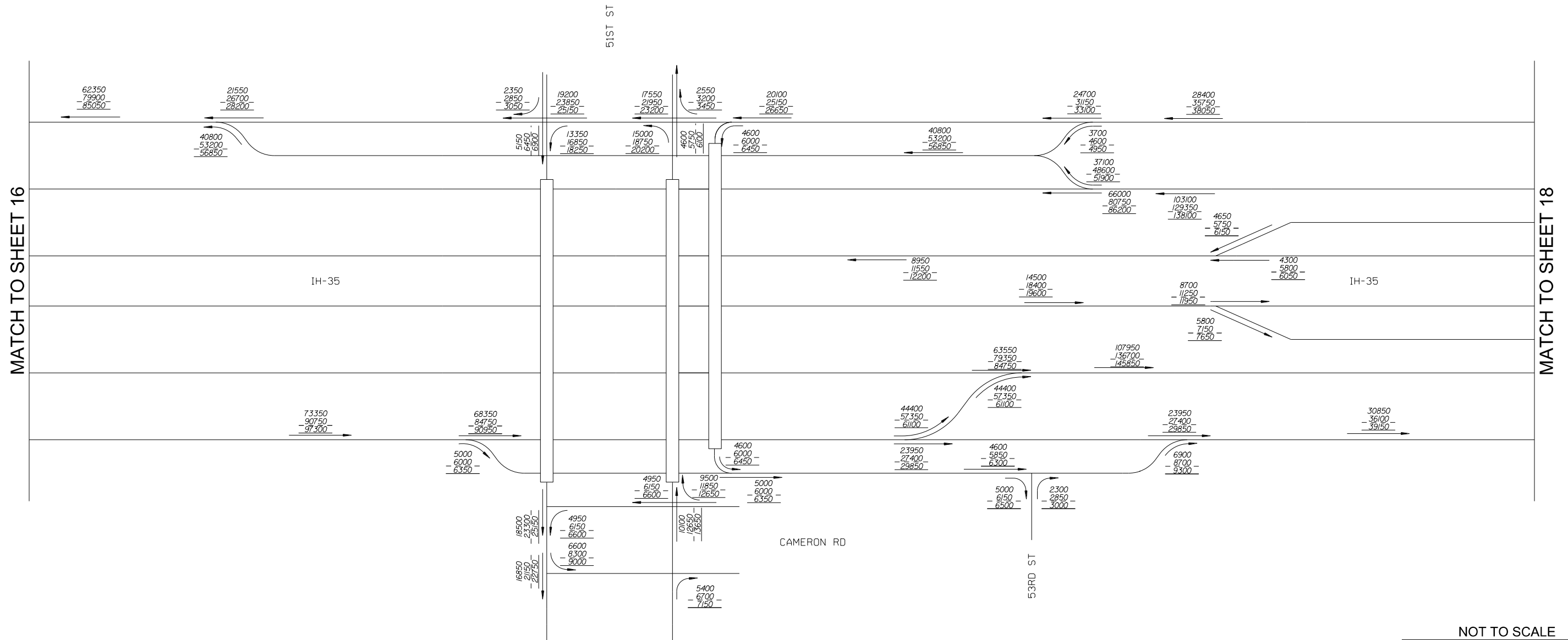


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 16 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

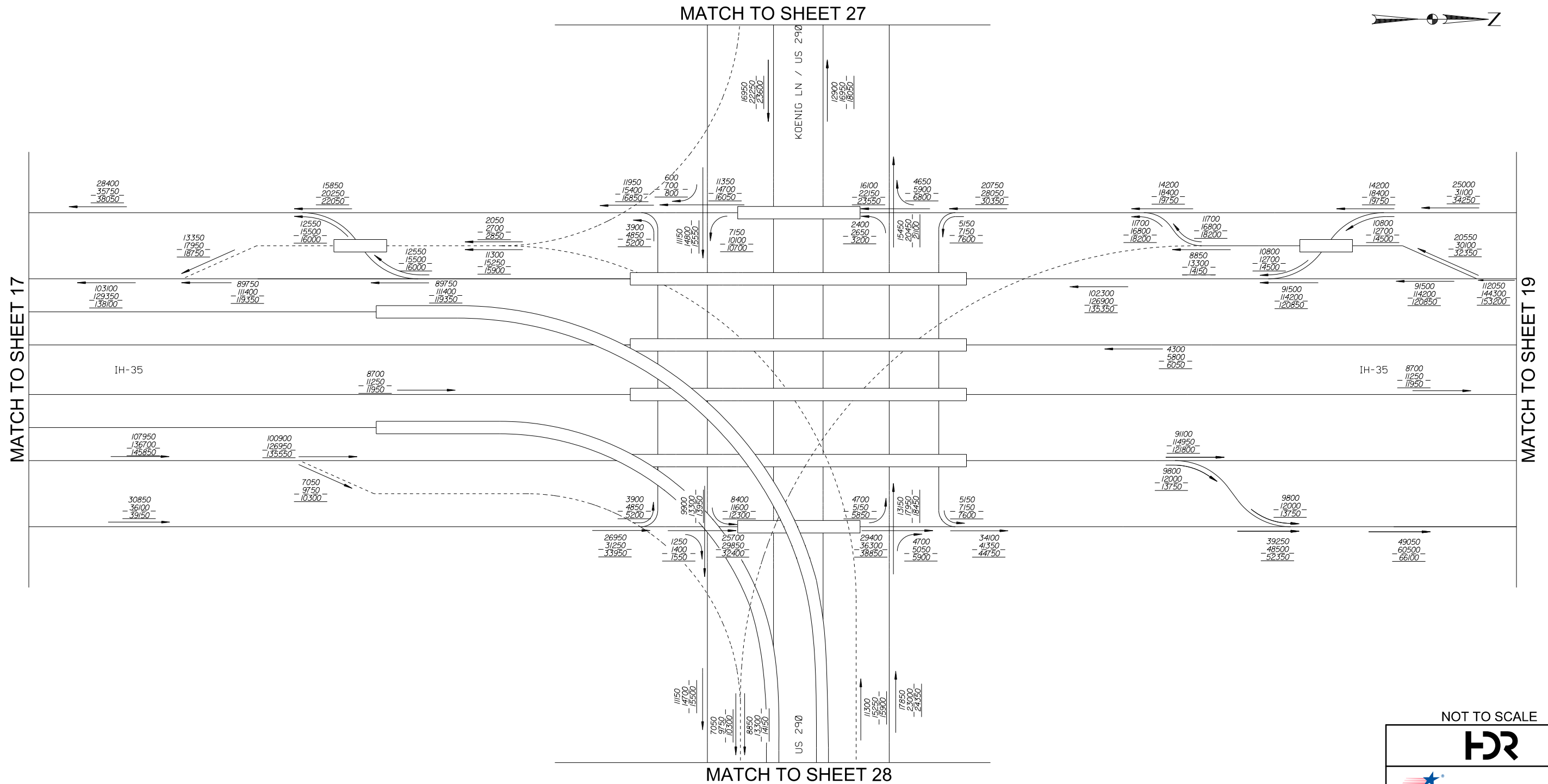
NOT TO SCALE

HR
 Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 17 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 17 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

- LEGEND**
- 1000 - 2030 ADT
 - 1000 - 2050 ADT
 - 1000 - 2060 ADT
 - TRAVEL DIRECTION

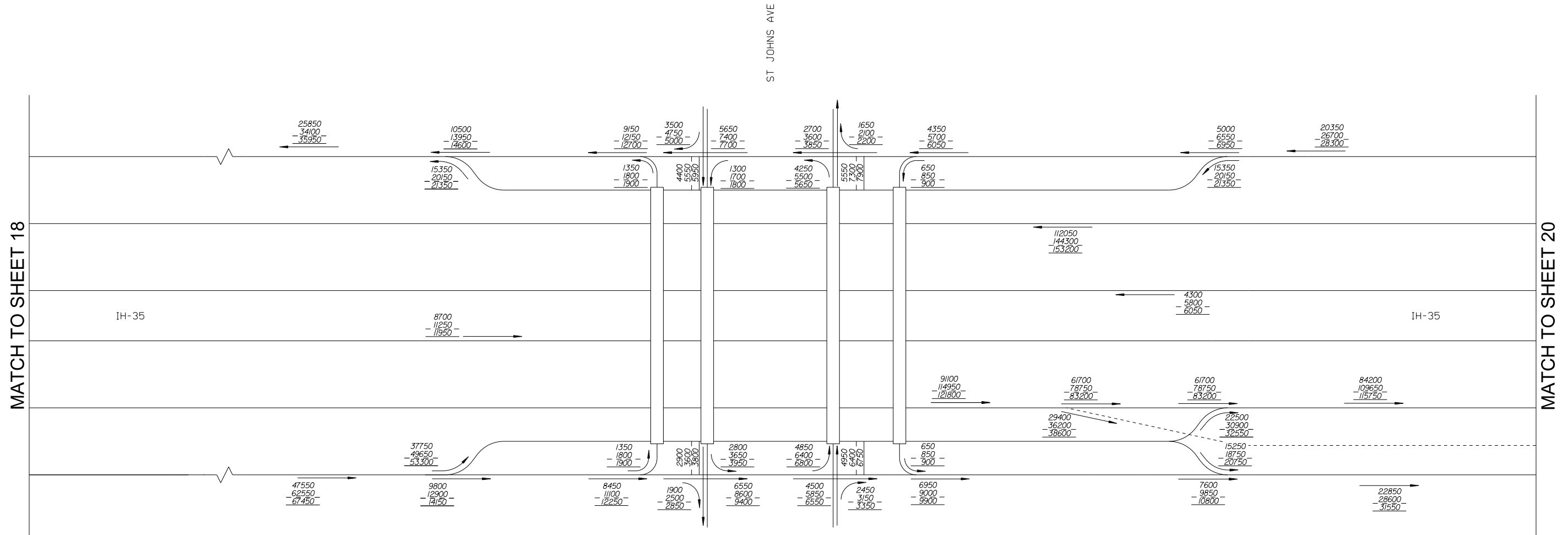
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 18 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 18 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

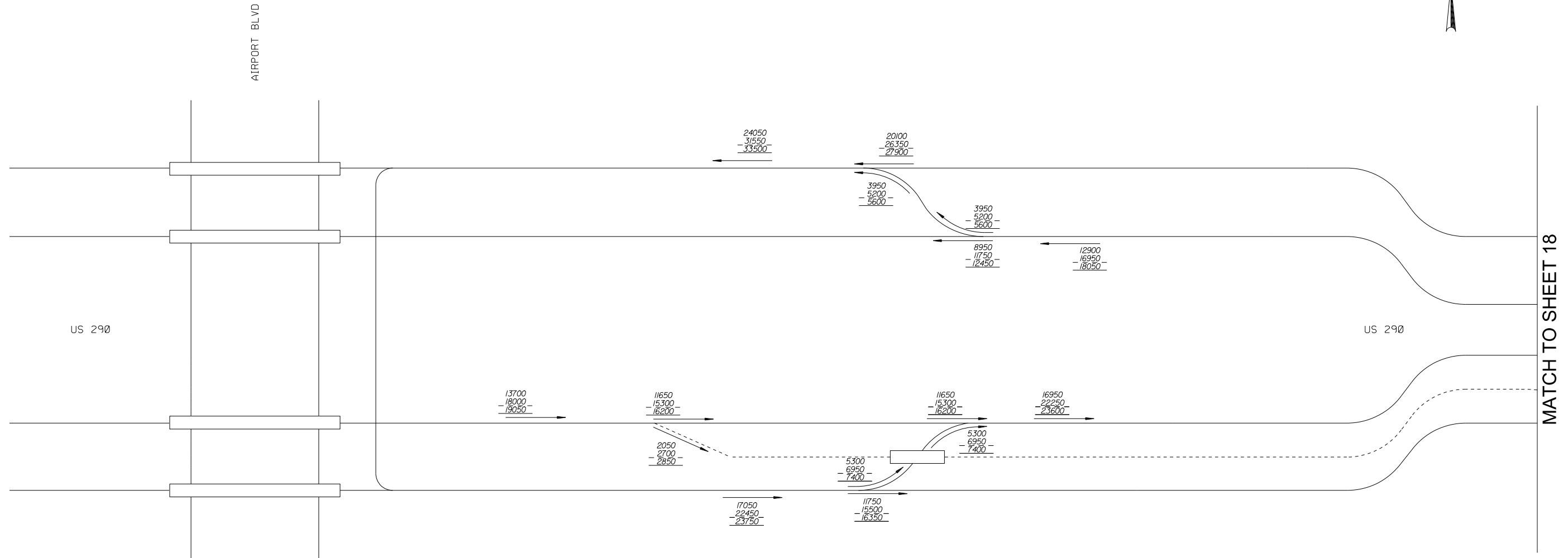
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 19 |

BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

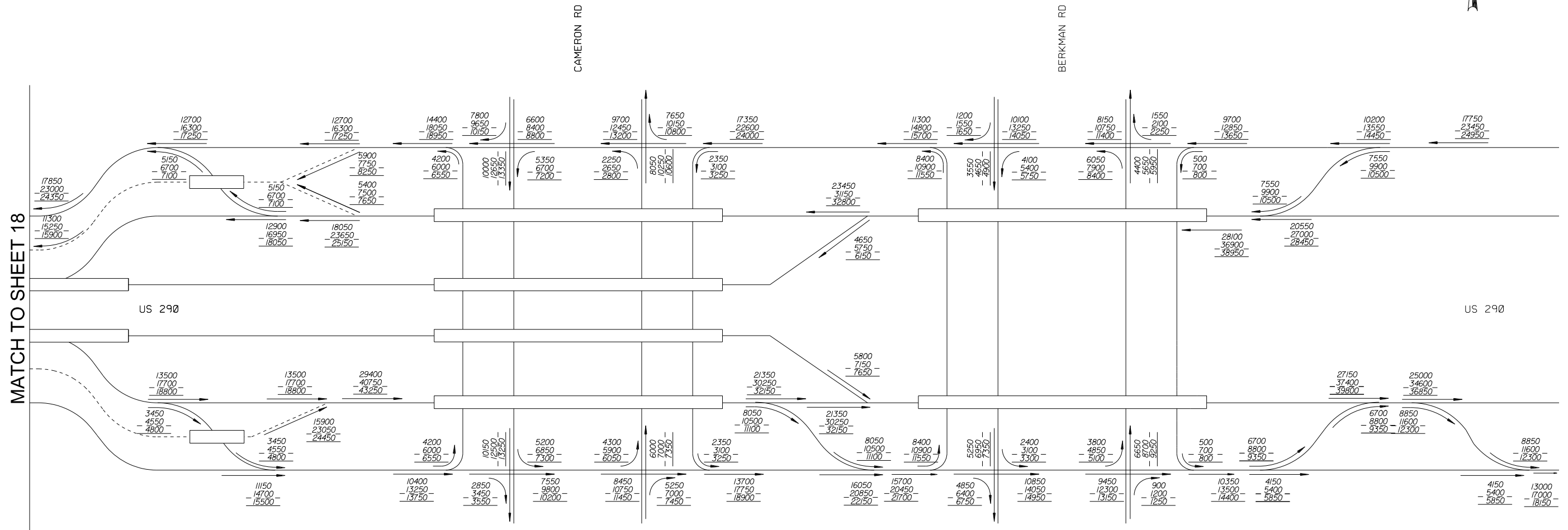
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 27 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 27 |

BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

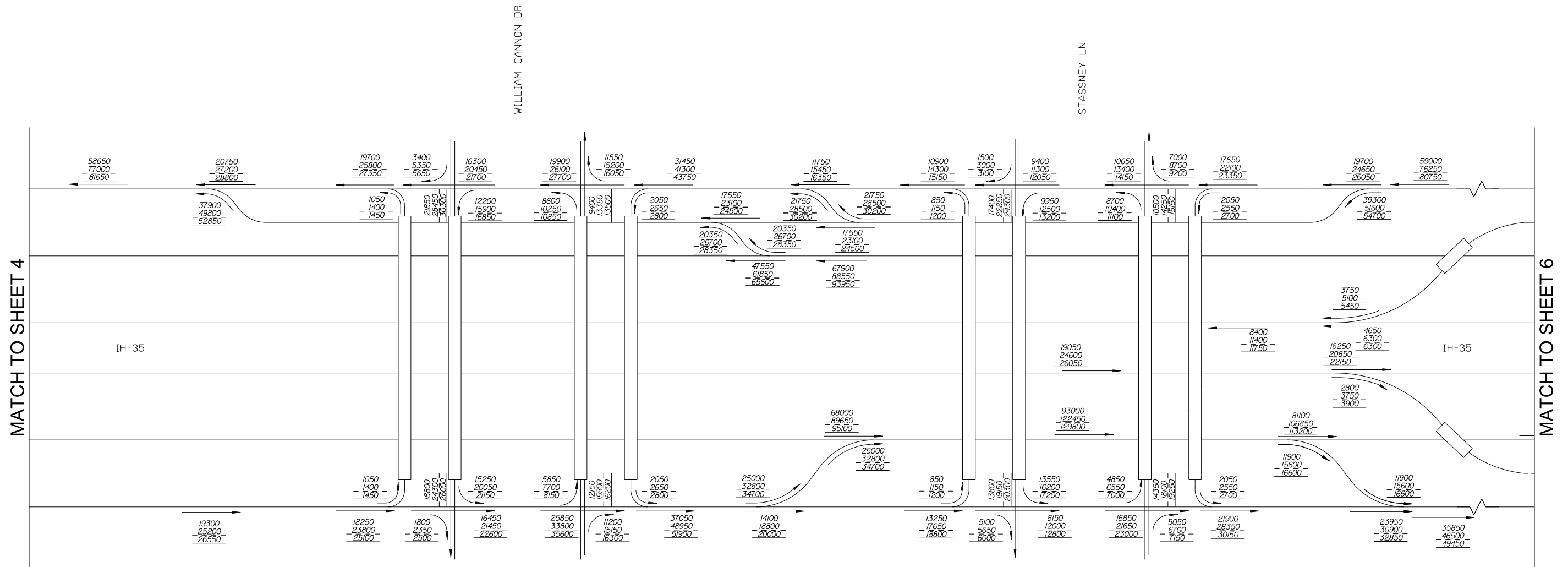


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 2
 24 HOUR VOLUMES
 (SHEET 28 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 28 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

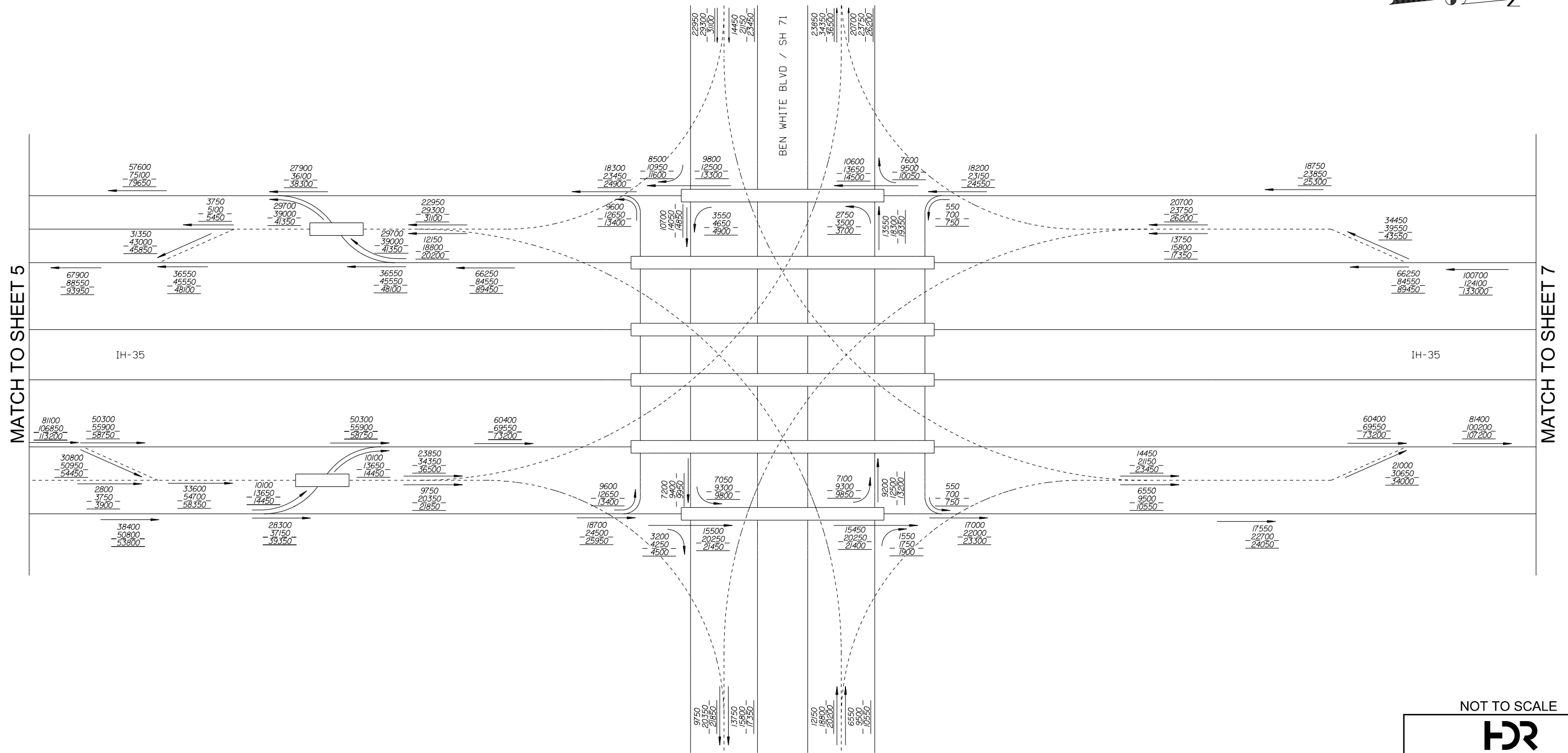


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 5 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 5 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

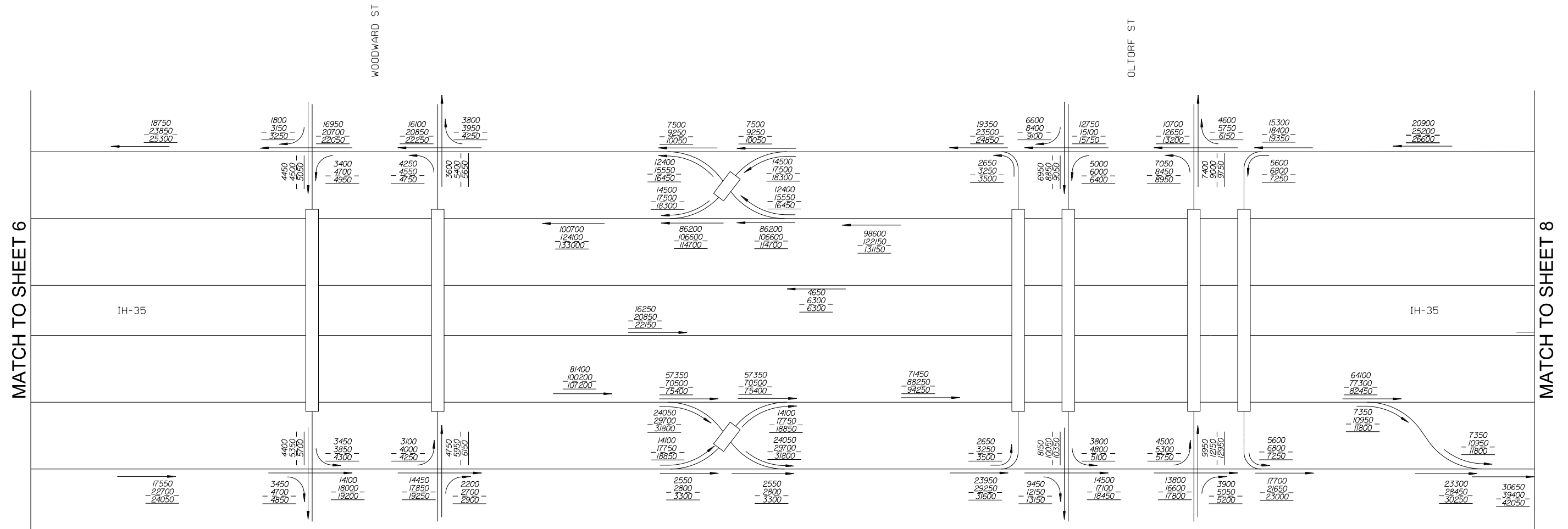
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 6 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 6 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE



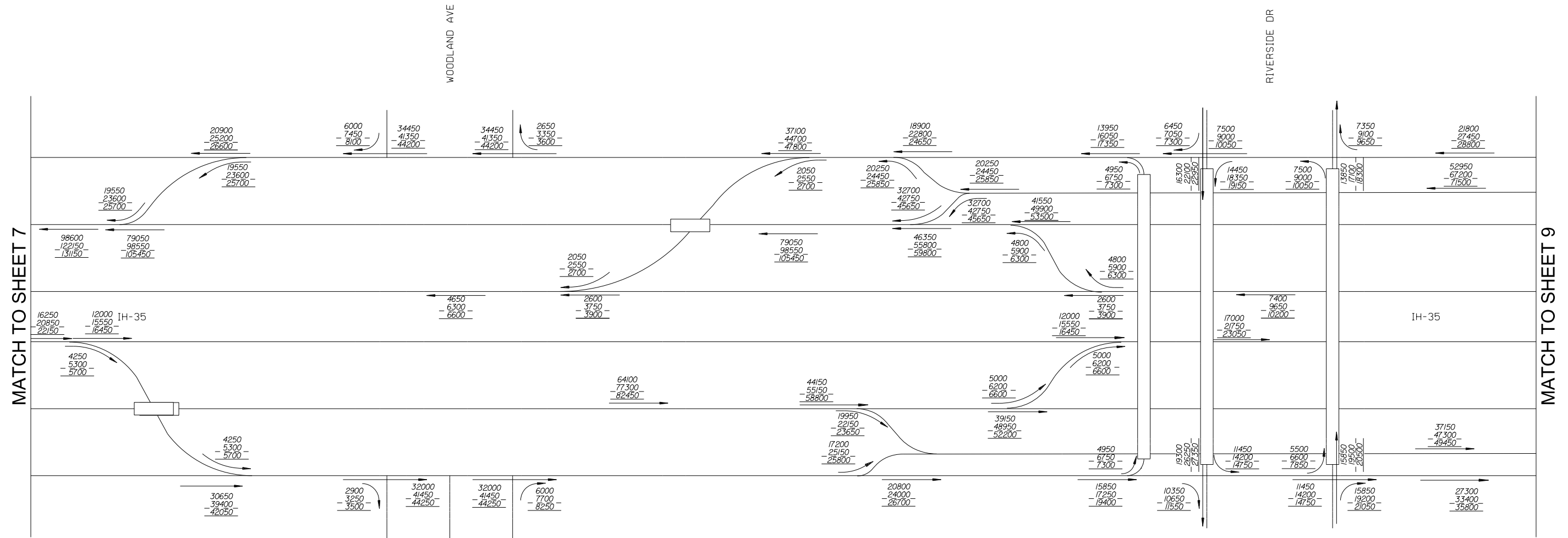
CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES

(SHEET 7 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 7 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

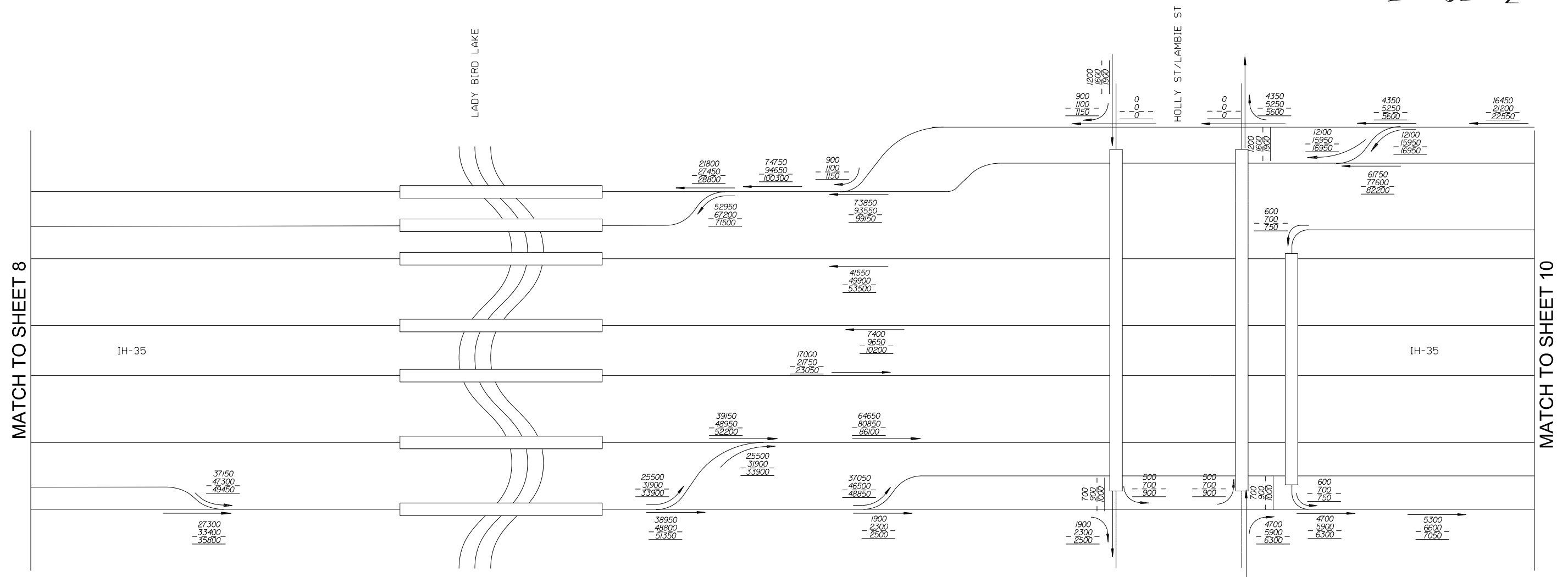


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 8 OF 28)

| | | | | |
|---------------|----------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 8 |

BUILD CONFIGURATION



MATCH TO SHEET 8

MATCH TO SHEET 10

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

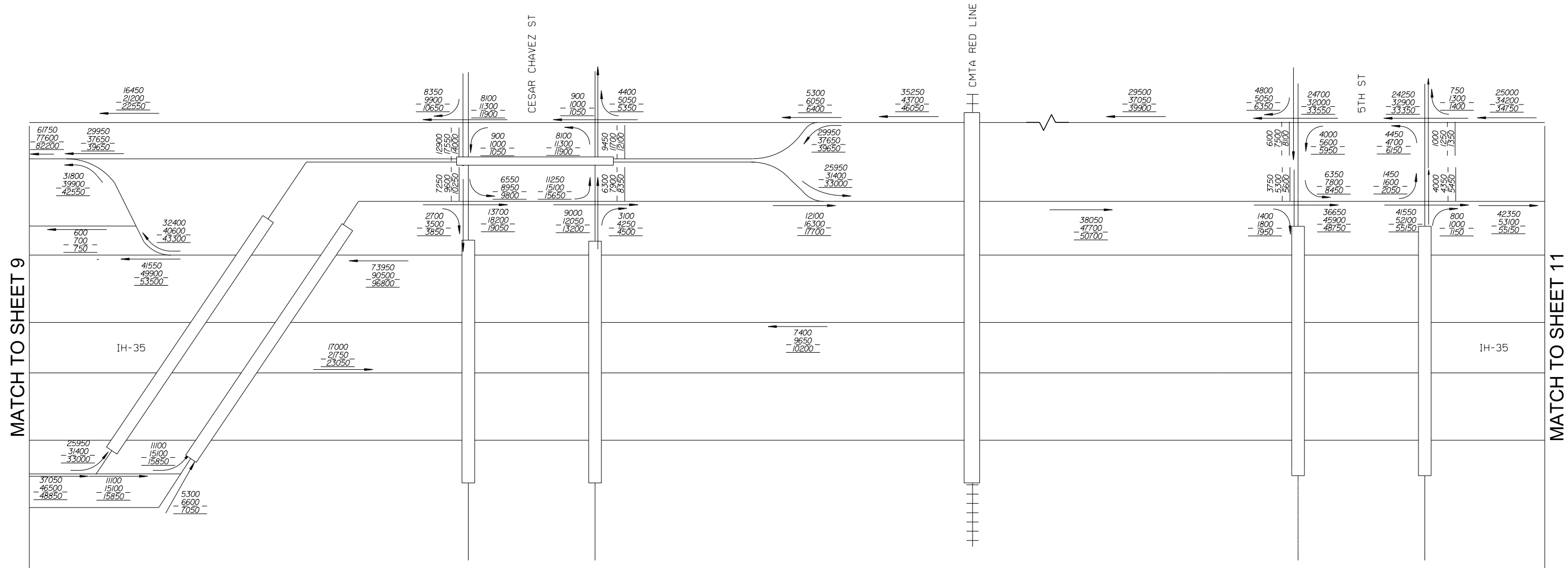


CAPITAL EXPRESS

BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 9 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 9 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

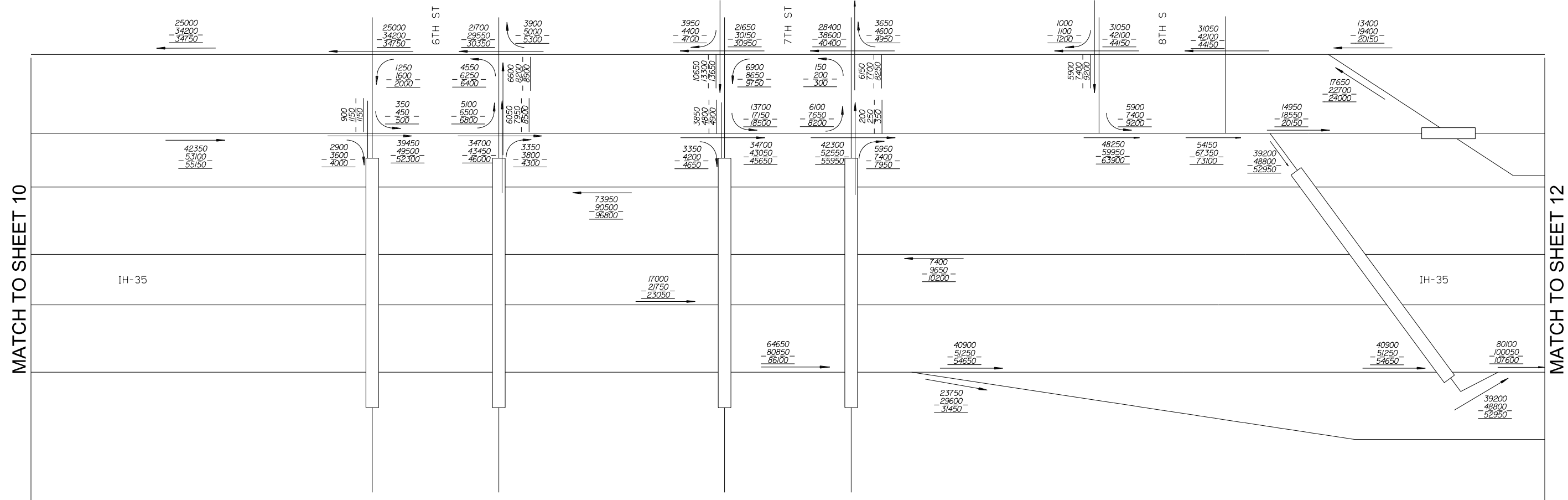
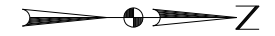
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 10 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 10 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

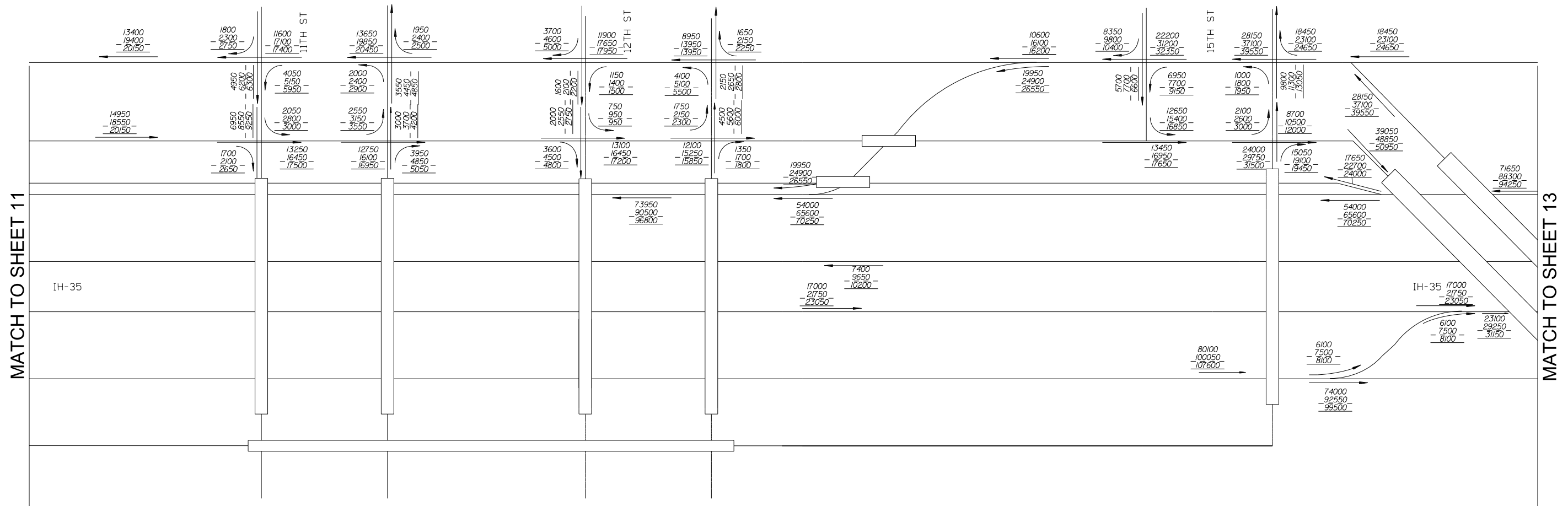
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 11 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 11 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

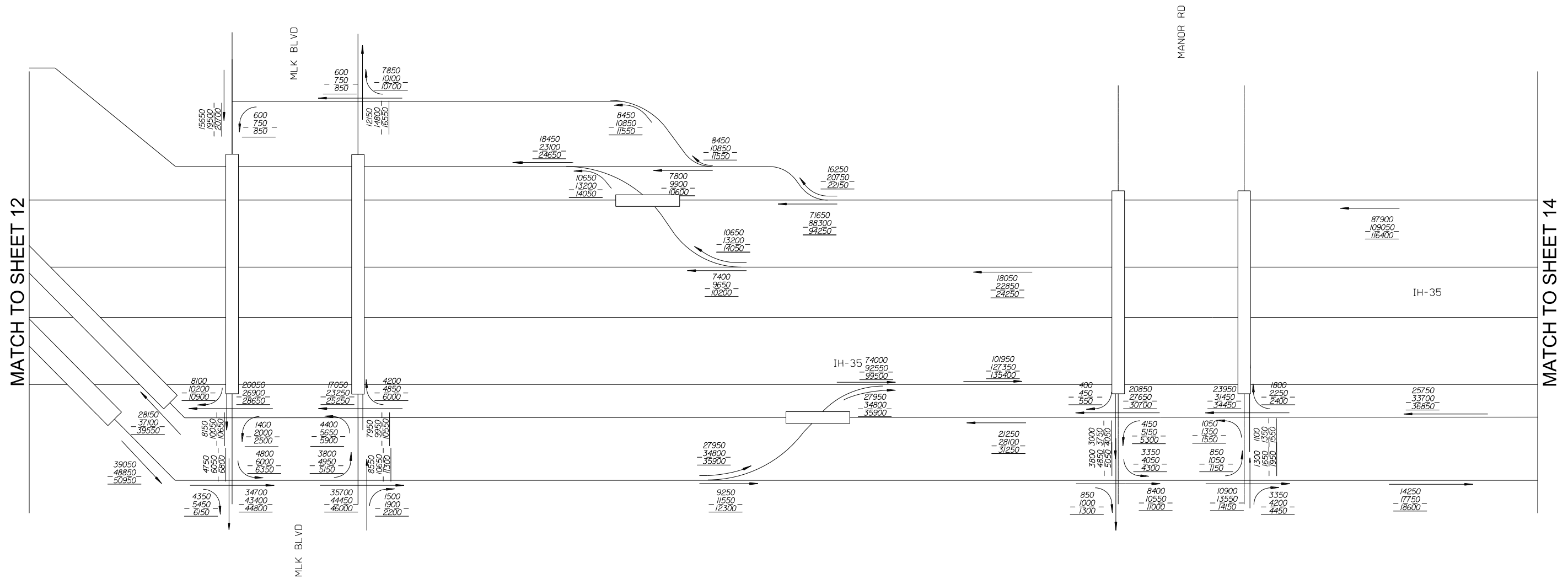
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 12 OF 28)

| | | | | |
|-----------------|-------------------|-------------|-----------|--|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | | |
| TEXAS 14 | 6 | TRAVIS | | |
| CONTROL SECTION | JOB | HWY. NO. | SHEET NO. | |
| 5000 00 | 106 | IH-35 | 12 | |


BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE

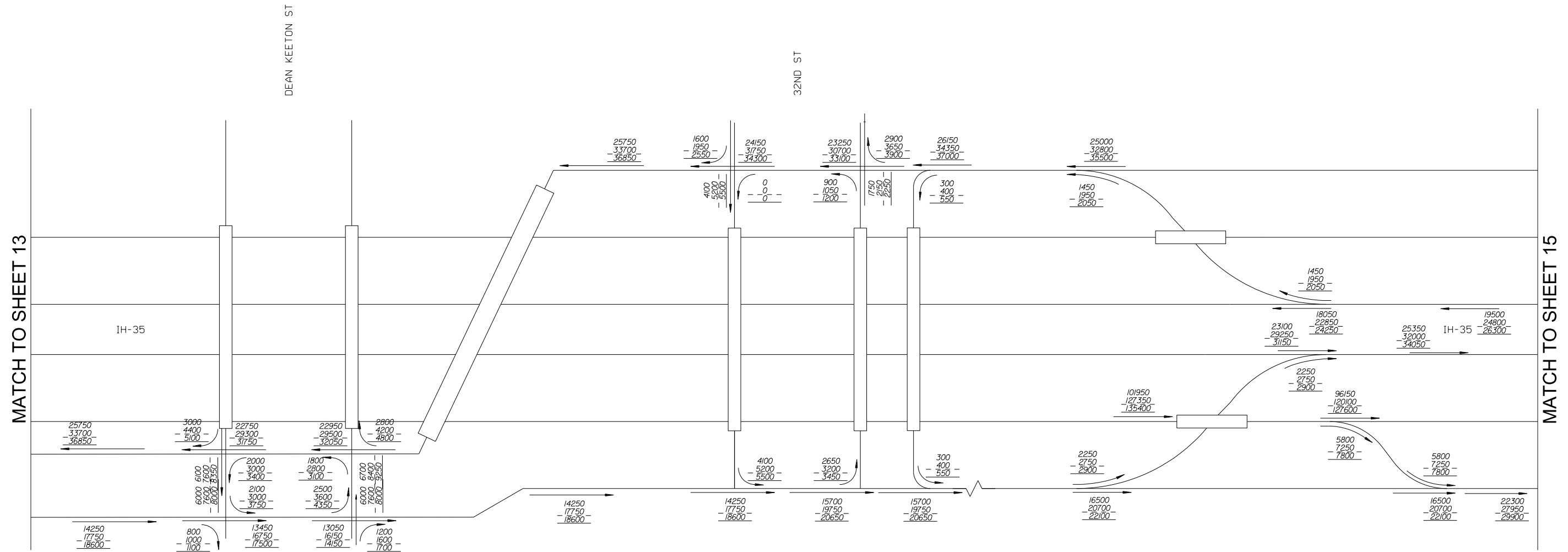


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 13 OF 28)

| | | | |
|---------------|---------|----------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | STATE DISTRICT | FED. RD. DIV. NO. |
| TEXAS | 14 | 6 | COUNTY TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 13 |

BUILD CONFIGURATION



NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 14 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 14 |

LEGEND

1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT

→ TRAVEL DIRECTION

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000_ - 2050 ADT
 1000_ - 2060 ADT
 → TRAVEL DIRECTION

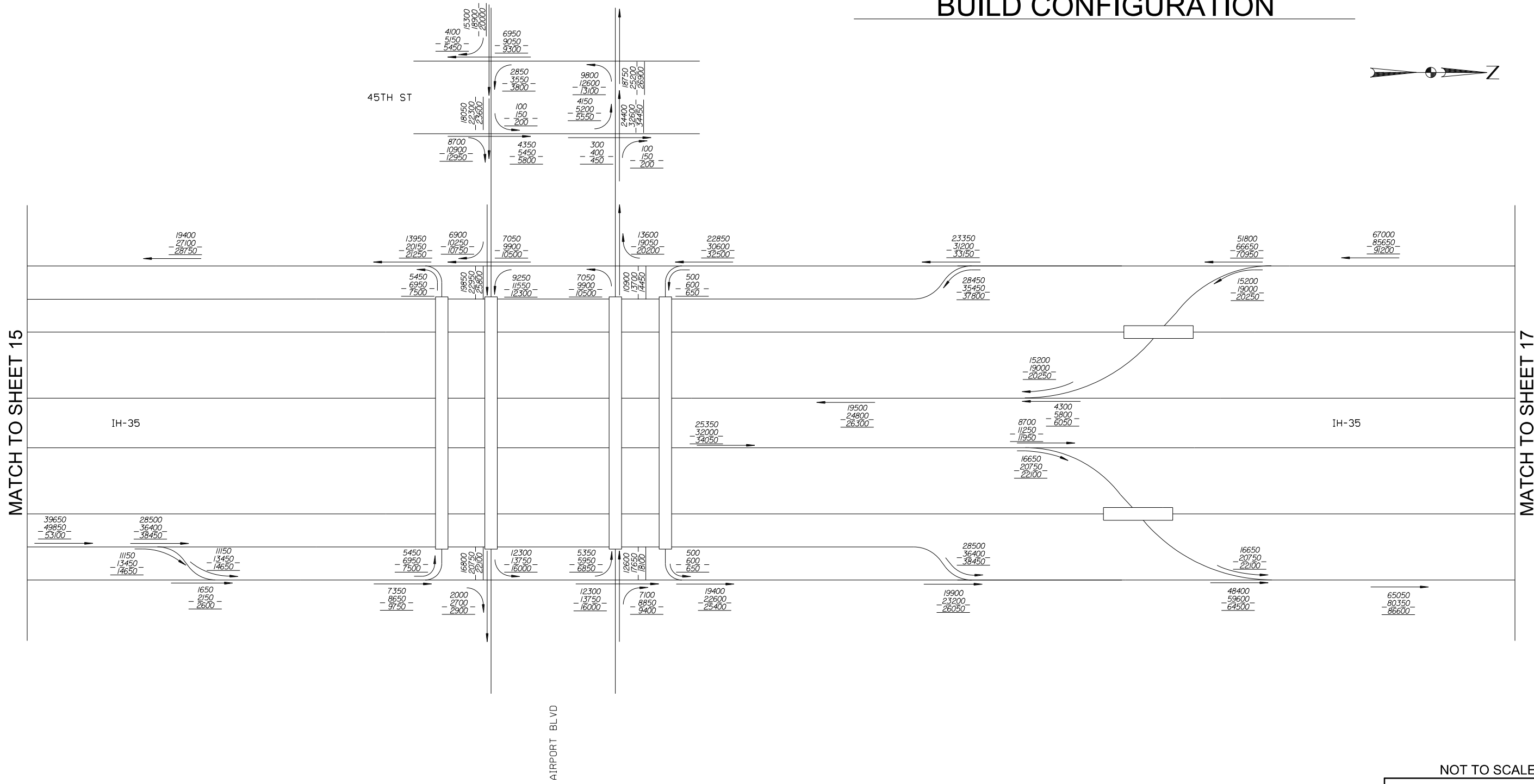
NOT TO SCALE



CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 15 OF 28)

| | | | | |
|----------------|----------------|-------------------|----------|-----------|
| SCALE : N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 15 |


BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000_ - 2050 ADT
 1000_ - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



HDR

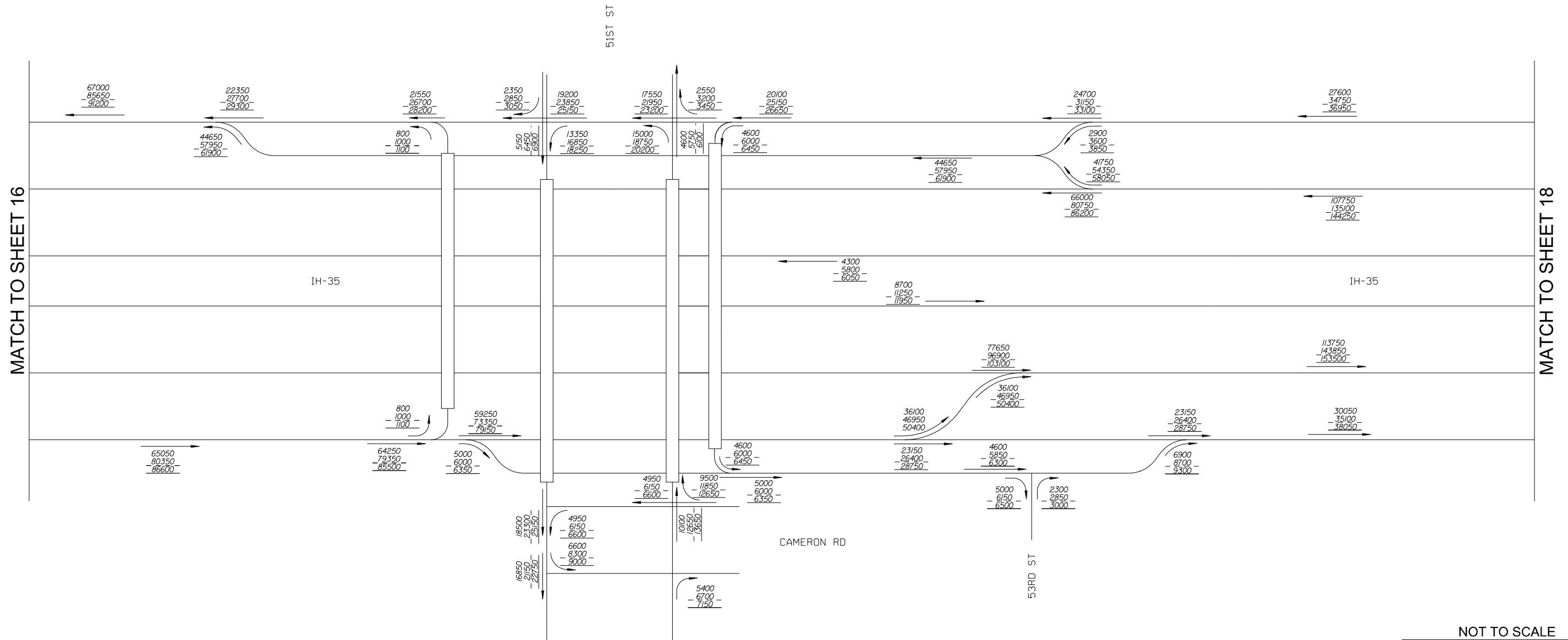
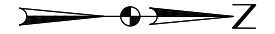


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 16 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 16 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

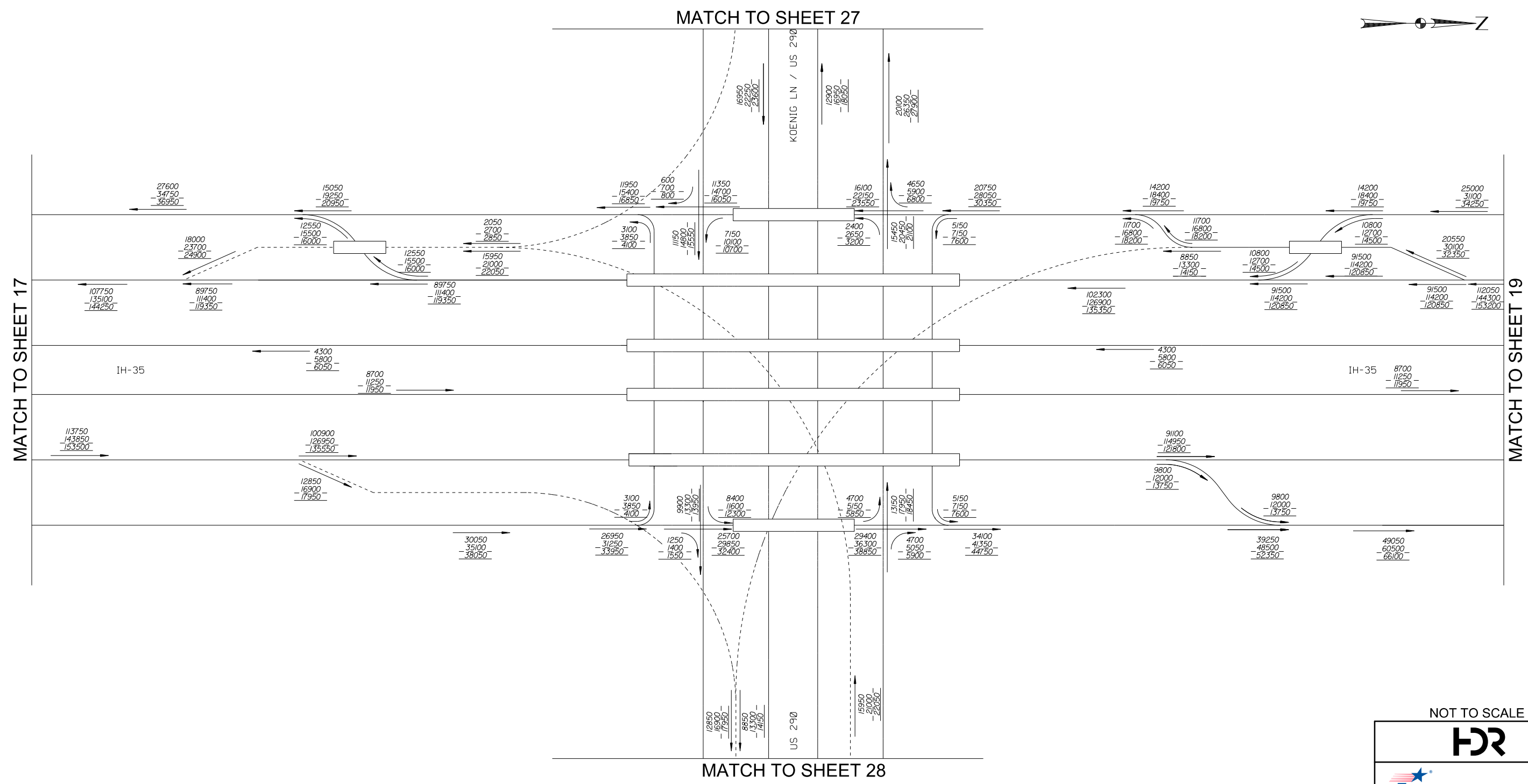
NOT TO SCALE

HR
 Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 17 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 17 |

BUILD CONFIGURATION



2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

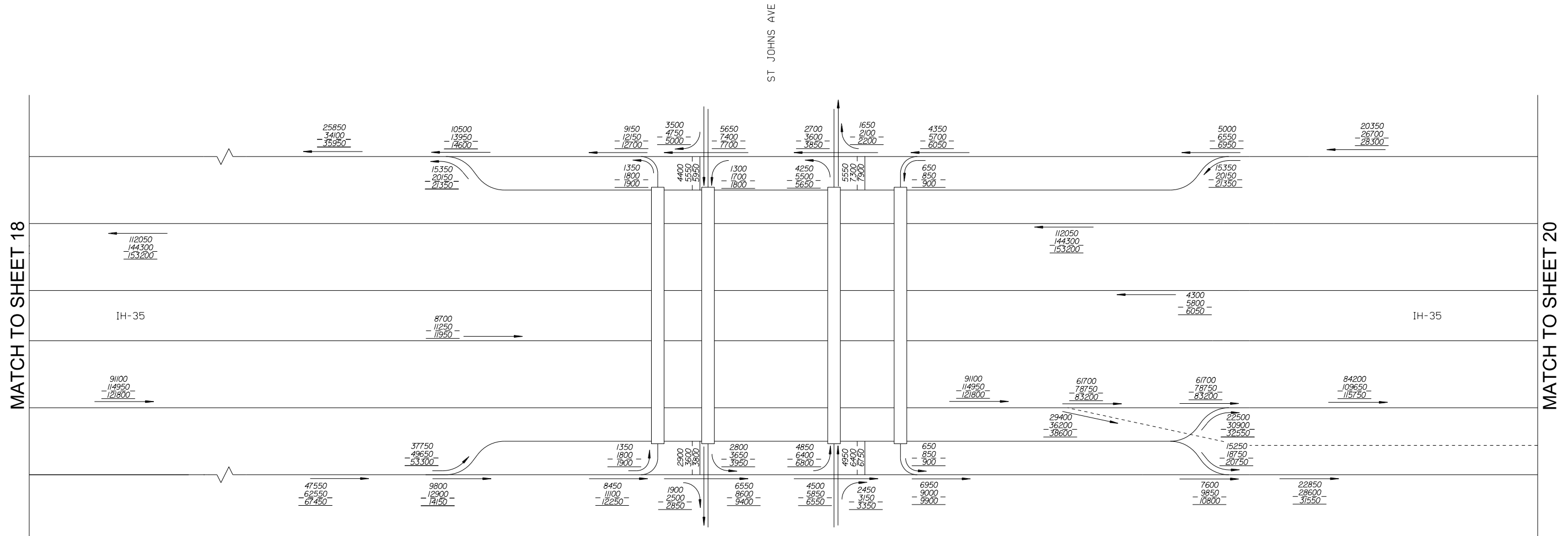
NOT TO SCALE

Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 18 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 18 |


BUILD CONFIGURATION




2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



HDR

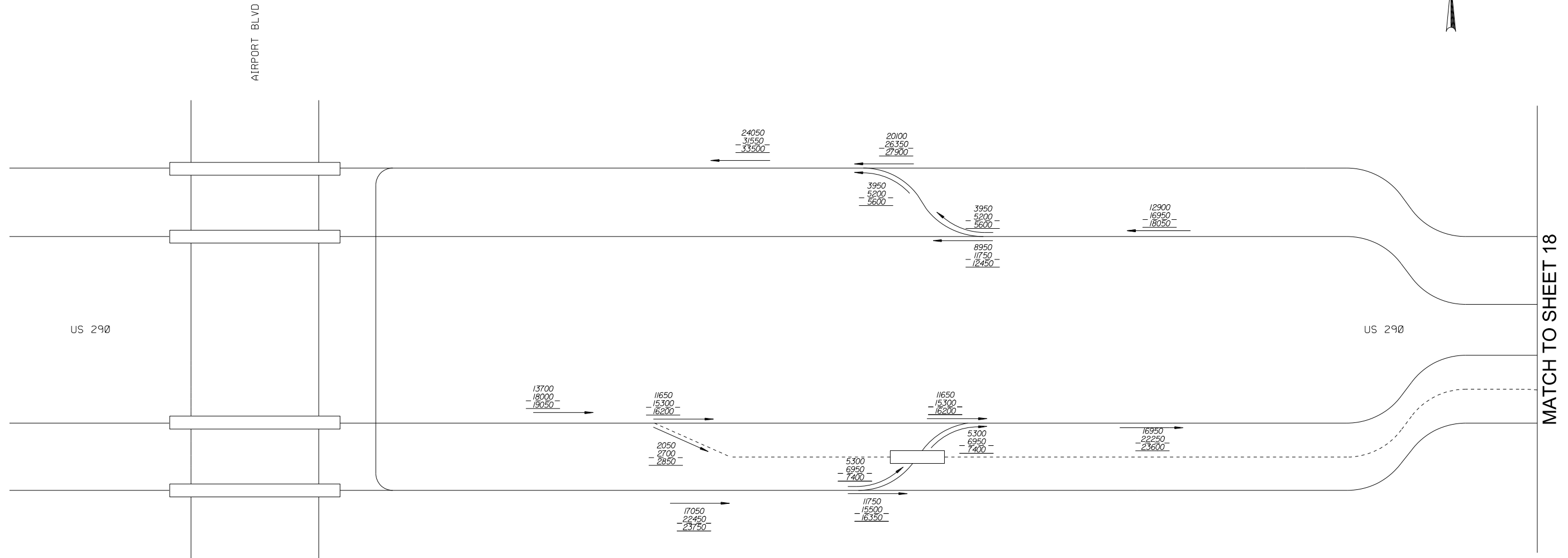


Texas Department of Transportation

CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 19 OF 28)

| | | | |
|---------------|----------------|-------------------|--------------------|
| SCALE: N.T.S. | | PROJECT NO. | |
| DWN: TH | CKD: HH | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY |
| TEXAS | 14 | 6 | TRAVIS |
| CONTROL | SECTION | JOB | HWY. NO. SHEET NO. |
| 5000 | 00 | 106 | IH-35 19 |

BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND

- 1000 - 2030 ADT
- 1000 - 2050 ADT
- 1000 - 2060 ADT

→ TRAVEL DIRECTION

NOT TO SCALE

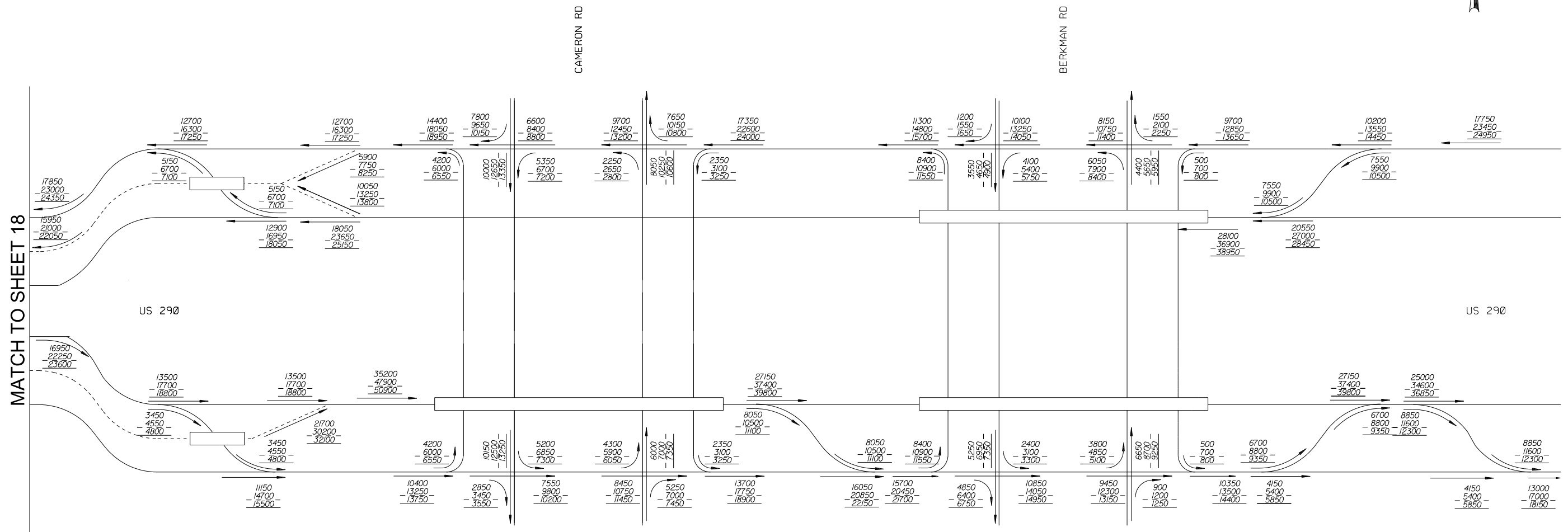


CAPITAL EXPRESS

BUILD CONFIGURATION
ALTERNATIVE 3 MOD
24 HOUR VOLUMES
(SHEET 27 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 27 |

BUILD CONFIGURATION



MATCH TO SHEET 18

2030, 2050, 2060 FORECASTED ULTIMATE BUILD AVERAGE DAILY TRAFFIC VOLUMES AND TURNING MOVEMENTS AT SPECIFIED POINTS ALONG CORRIDOR I-35 FROM MAIN ST TO HESTER'S CROSSING ROAD AND US 290 FROM AIRPORT BLVD TO US 183

LEGEND
 1000 - 2030 ADT
 1000 - 2050 ADT
 1000 - 2060 ADT
 → TRAVEL DIRECTION

NOT TO SCALE



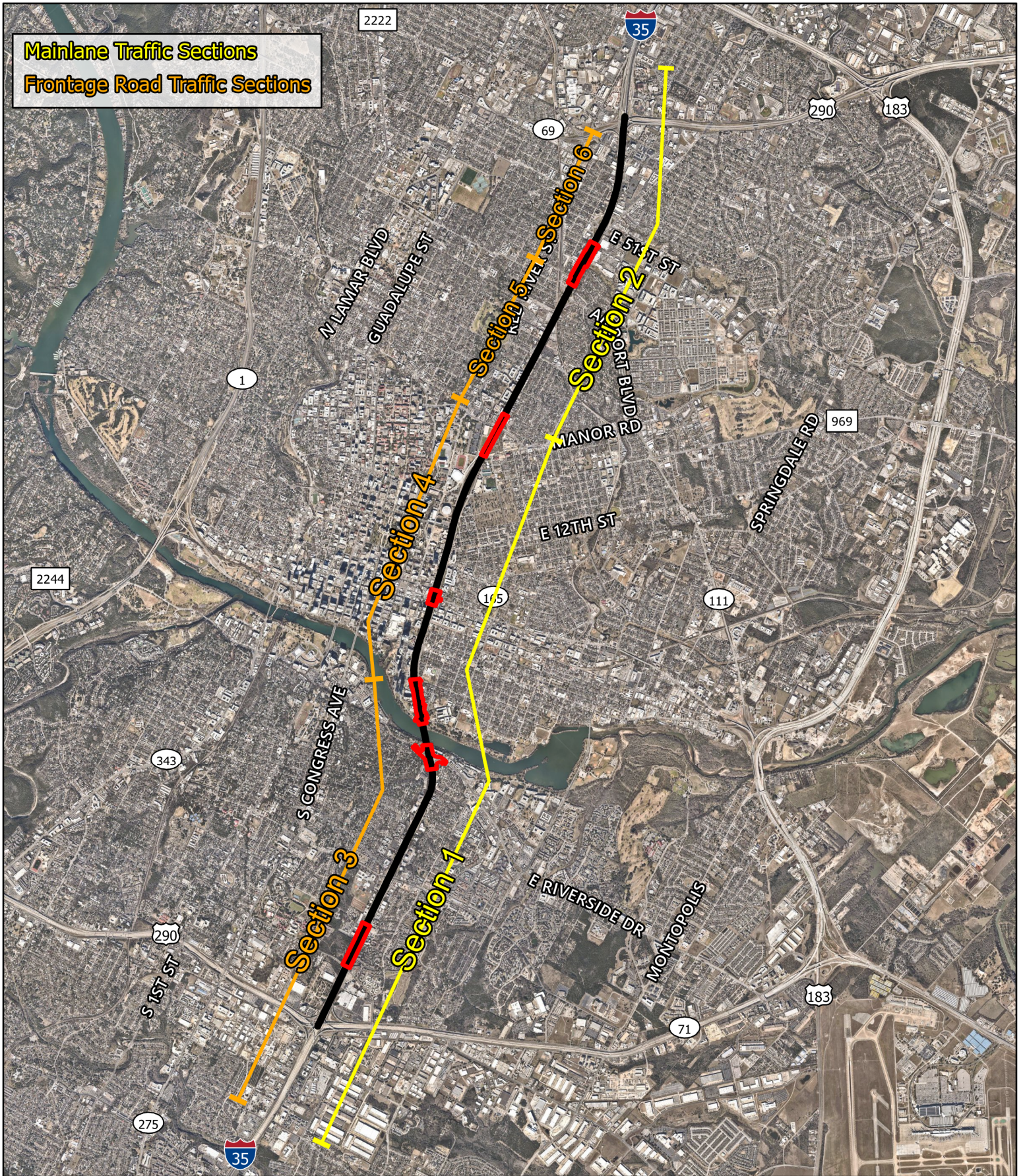
CAPITAL EXPRESS
 BUILD CONFIGURATION
 ALTERNATIVE 3 MOD
 24 HOUR VOLUMES
 (SHEET 28 OF 28)

| | | | | |
|---------------|----------------|-------------------|----------|-----------|
| SCALE: N.T.S. | | PROJECT NO. | | |
| DWN: TH | CKD: HH | | | |
| STATE | STATE DISTRICT | FED. RD. DIV. NO. | COUNTY | |
| TEXAS | 14 | 6 | TRAVIS | |
| CONTROL | SECTION | JOB | HWY. NO. | SHEET NO. |
| 5000 | 00 | 106 | IH-35 | 28 |

APPENDIX C

CO Receptor Locations

Mainlane Traffic Sections
Frontage Road Traffic Sections

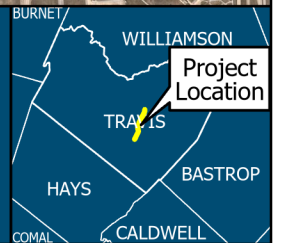
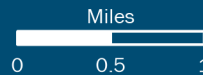


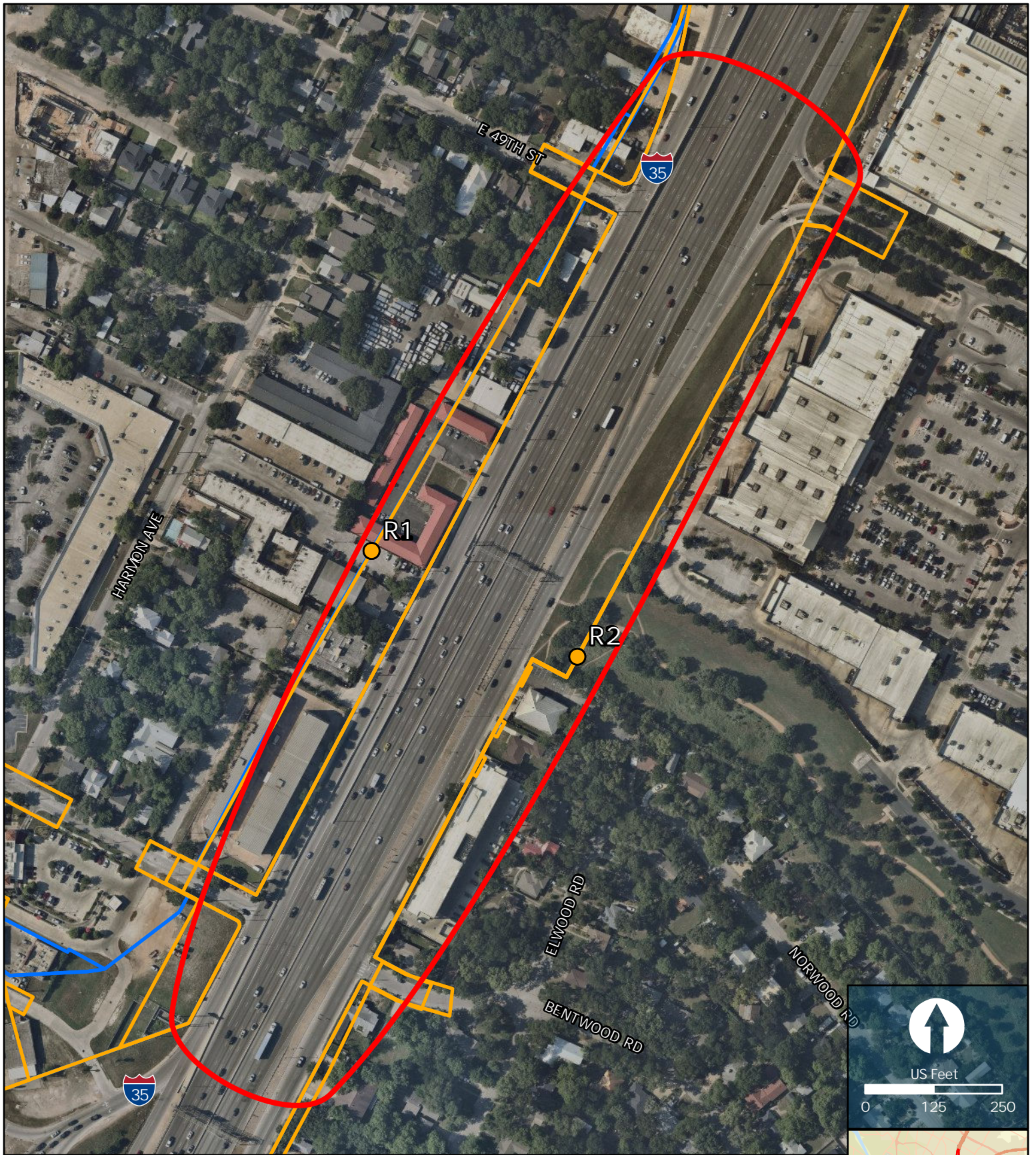
CO Modeling Locations Overview
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

Sources: ESRI Basemaps 2021

 Project Location
 CO Modeling Area





CO Receptors - Segment 1

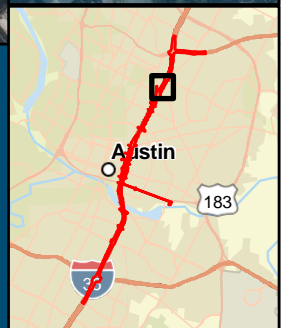
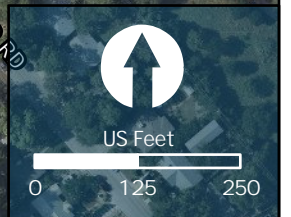
I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

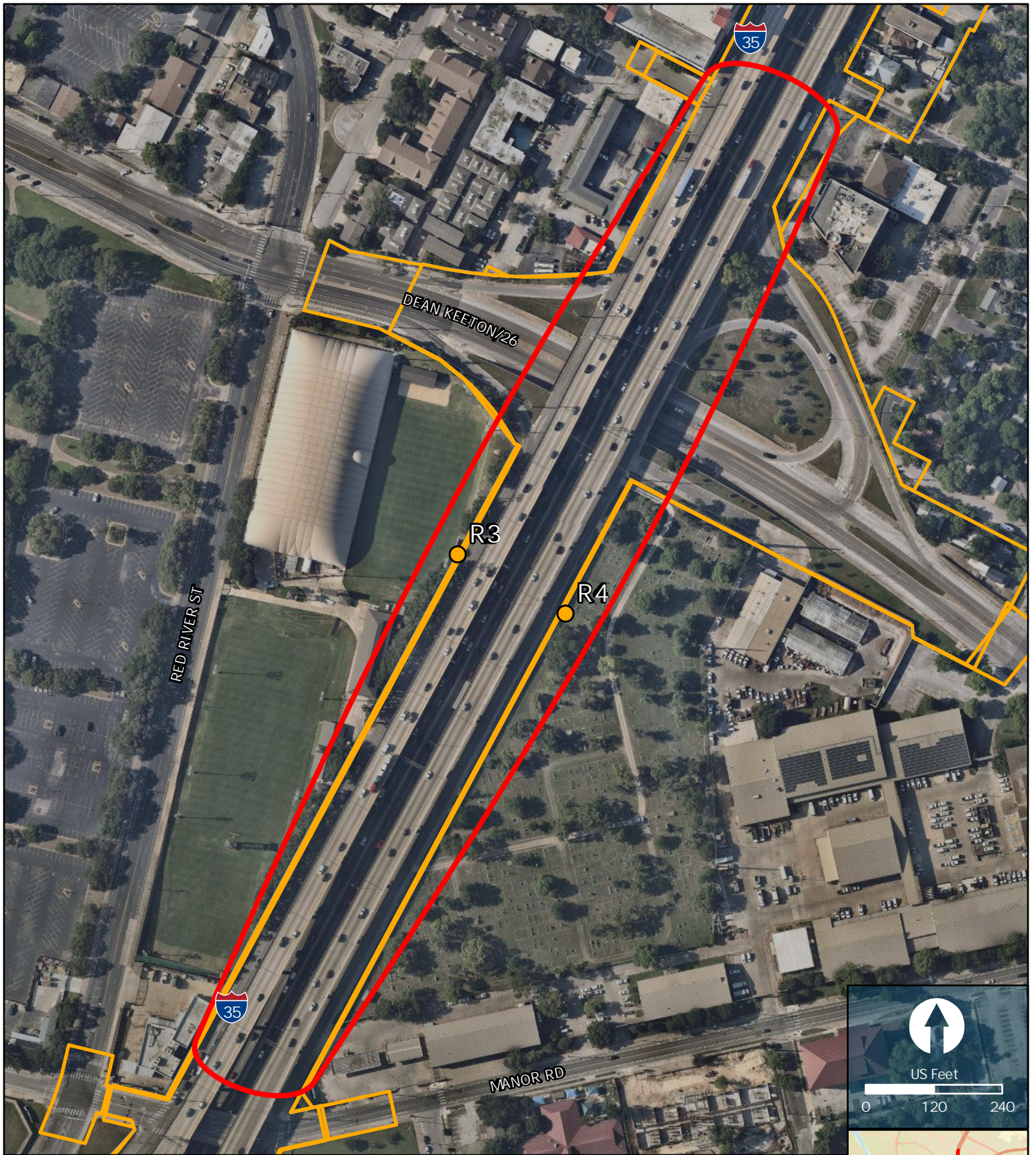
- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod



Sources: Nearmap 2022



CO Receptors - Segment 2

I-35 Capital Express Central

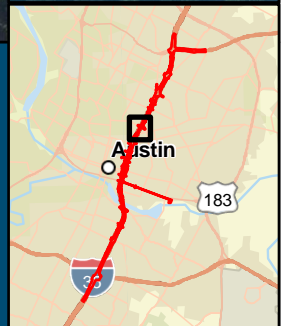
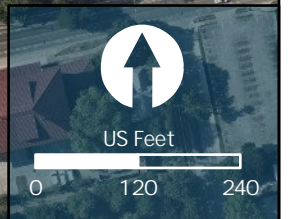
From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

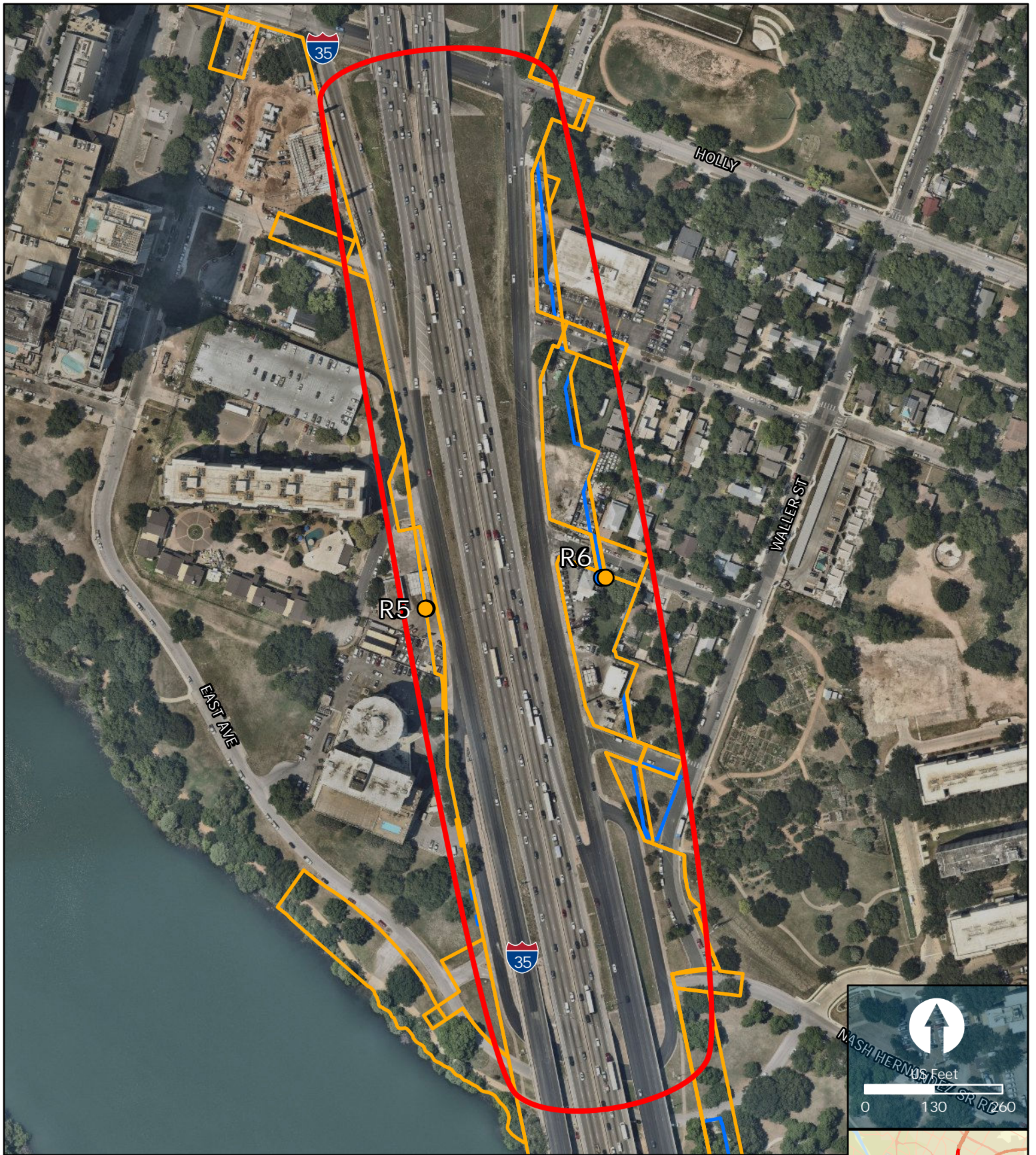
- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod

Sources: Nearmap 2022





CO Receptors - Segment 3

I-35 Capital Express Central

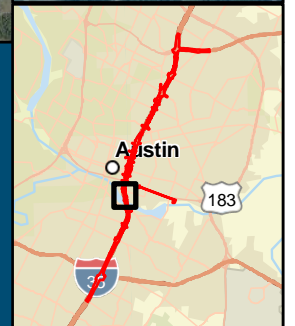
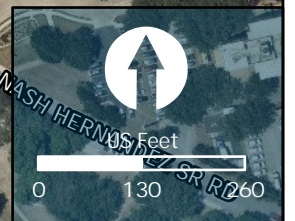
From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

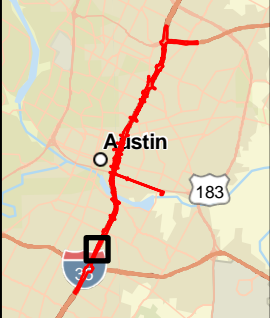
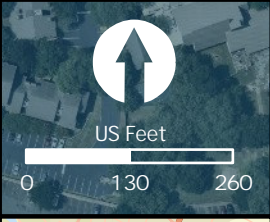
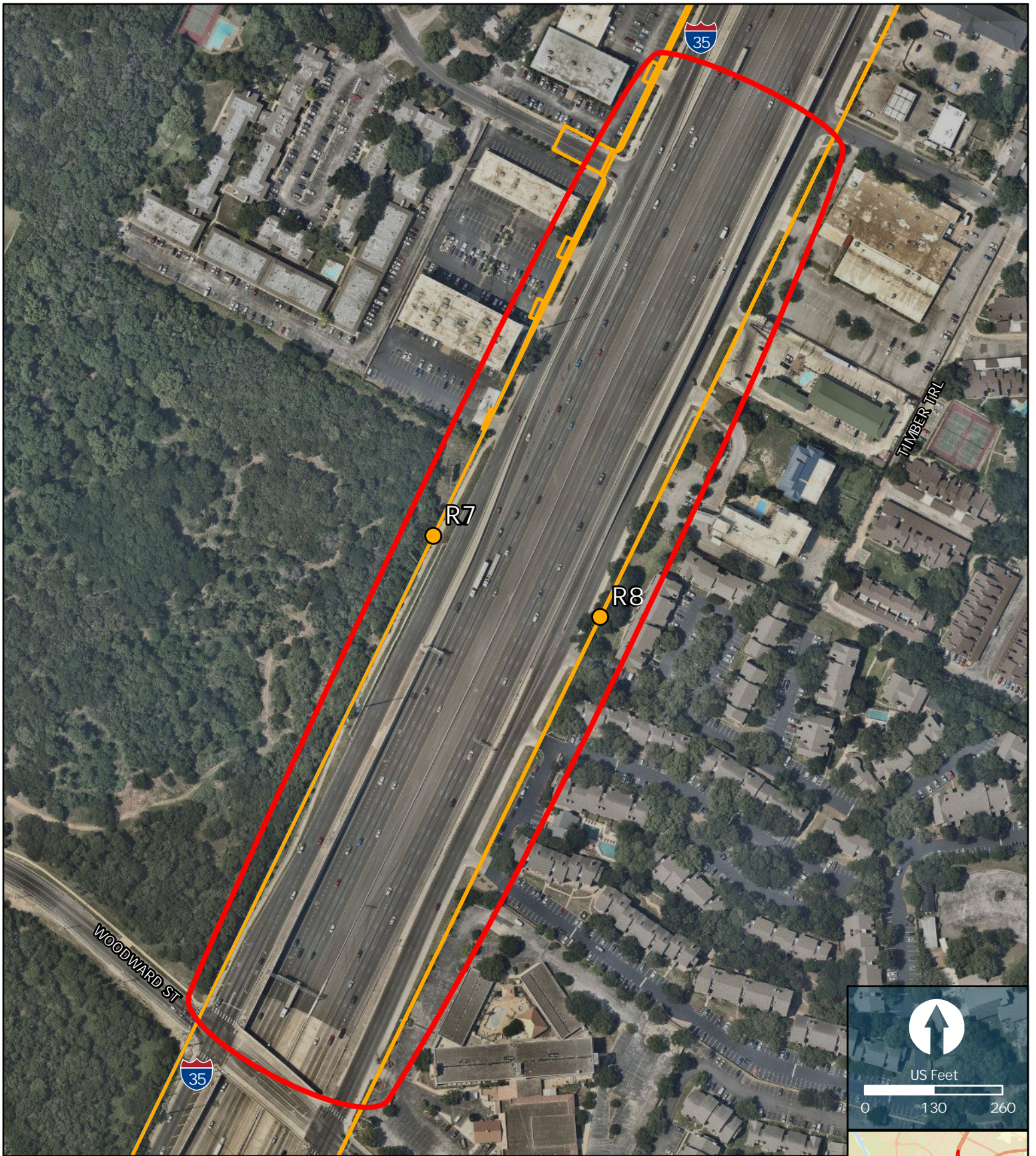
- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod

Sources: Nearmap 2022





CO Receptors - Segment 4

I-35 Capital Express Central

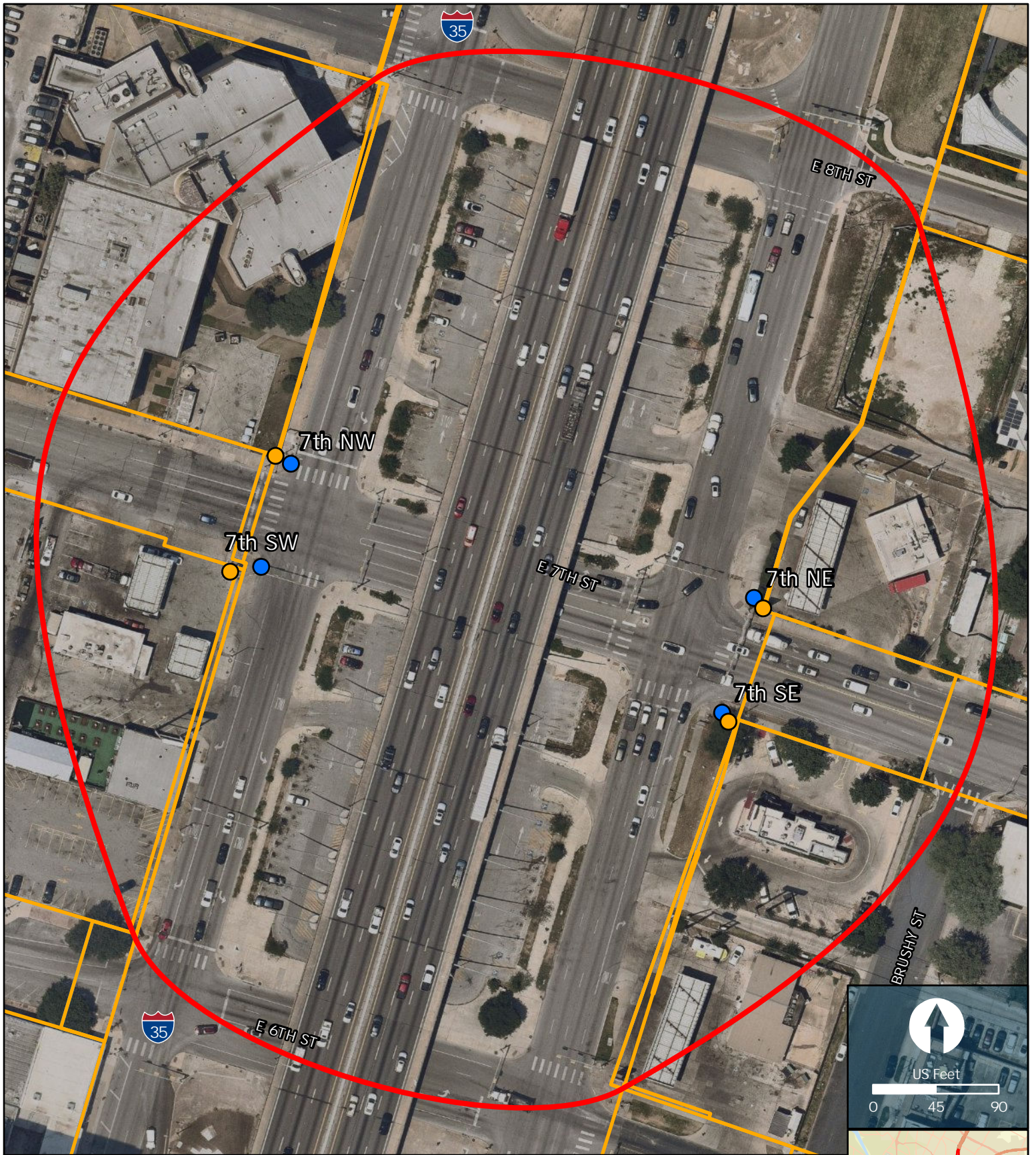
From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod

Sources: Nearmap 2022



CO Receptors - Segment 5

I-35 Capital Express Central

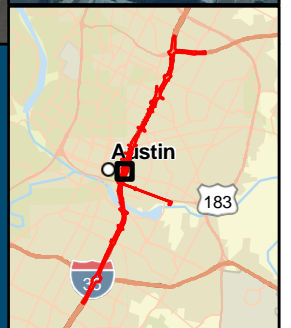
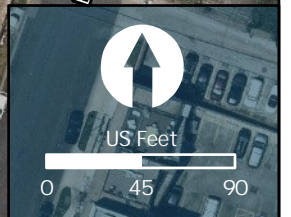
From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

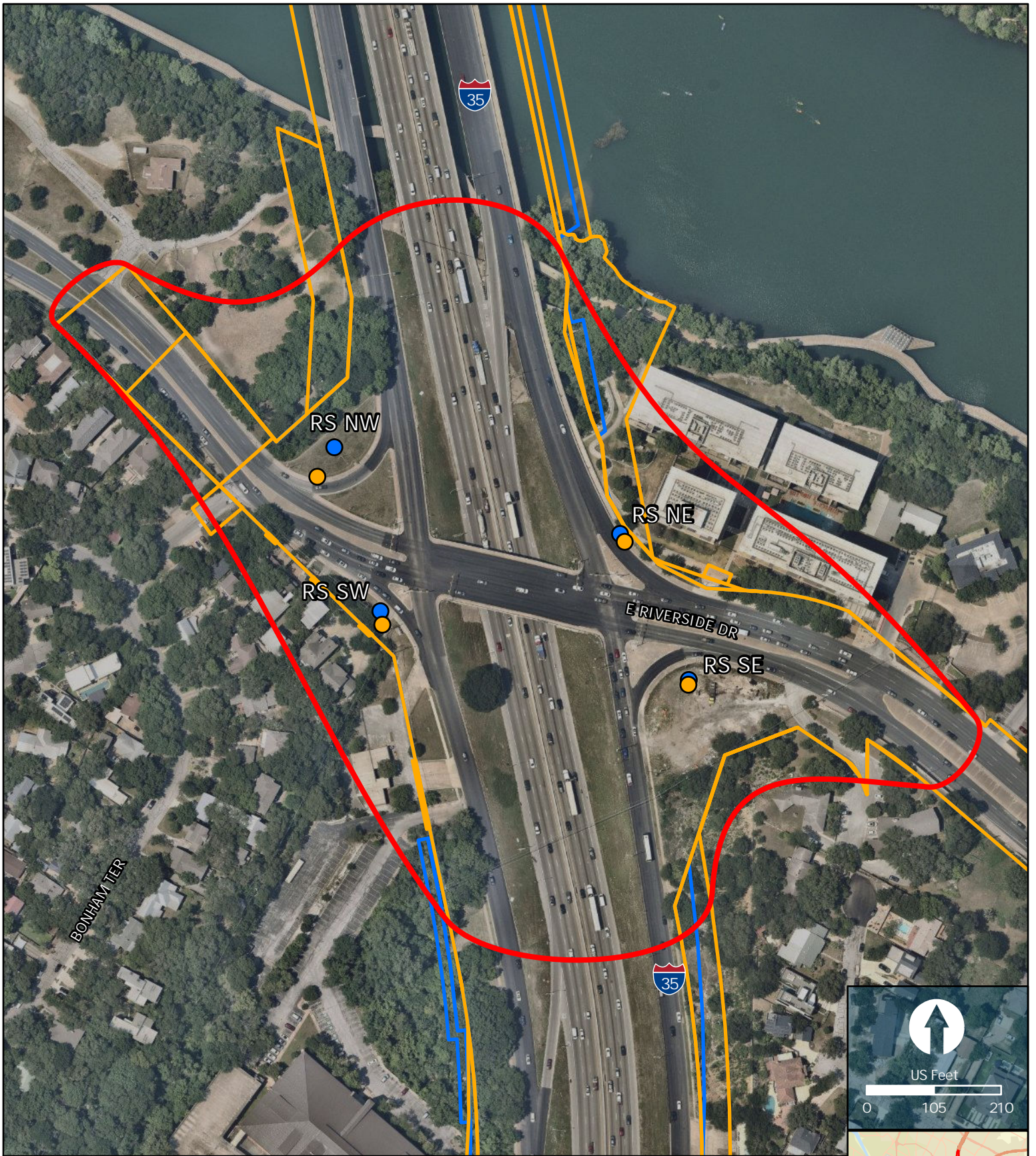
- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod

Sources: Nearmap 2022





CO Receptors - Segment 6

I-35 Capital Express Central

From US 290 East
 To US 290 West/SH 71
 Travis County, TX
 CSJ: 0015-13-388

- Alt 2 Study Area
- Alt 3 Mod Study Area
- CO Modeling Area

Receptor Location

- Alt 2
- Alt 3 Mod

